TECHNICAL REPORT IGE-300

A USER GUIDE FOR DONJON VERSION4

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1 INTRODUCTION

DONJON is a full-core modelization code designed around solution techniques of the neutron diffusion or simplified P_n equation.^[1] The current DONJON package is an evolution version, released as an attempt to introduce the innovative capabilities for the full-core modeling and simulations of different types of nuclear reactors sush as Pressurized Water Reactors (PWRs), legacy CANDU reactors, and Advanced CANDU Reactors (ACRs). The computer code DONJON (Release 4.0) is part of Version4 distribution^[2], built around the GAN generalized driver^[3]. Its execution depends on other computer codes, components of Version4, namely: GANLIB, UTILIB, DRAGON^[4], and TRIVAC^[5] codes. The DRAGON modules are used with DONJON code to define the reactor geometry, to provide the macroscopic cross-section libraries and to perform micro-depletion calculations. The TRIVAC solver modules are used to perform a spatial discretization of the reactor geometry and to provide the numerical solution according to the user-selected numerical procedure^[6-11]. The UTILIB library provides the utility and linear algebra libraries. Finally, the GANLIB computer code provides CLE-2000 capabilities to control data flows and to implement *computational schemes*. GANLIB also provide LCM data structures to exchange information between modules.

The DONJON code is divided into several modules, each module is designed to perform some particular tasks. The transfer of information between the modules is achieved by means of well defined data structure. Several design features, data structure and computing algorithms were recovered, revised and adapted from the previous DONJON version^[12, 13]. One of the main concerns of the DONJON developers is to ensure the code reliability and extensibility.

The DONJON modules are first designed for the reactor full-core modeling in 3-D Cartesian geometry. These modules are built around the reactor fuel lattice specification corresponding to the common design features of CANDU reactors. The modules related to the modeling of reactivity mechanisms, which are normally presented in the reactor core, also constitute an important part of code. The DONJON code can perform several full-core calculations and can be used to determine some important core characteristics, such as the power and normalized flux distributions over the reactor core. All full-core calculations using current version of DONJON correspond to the reactor static conditions.

The modeling of the reactor fuel lattice using DONJON is made in considering that the fuel lattice is composed of a well defined number of fuel channels and bundles. All reactor channels contain the same number of fuel bundles and are identified by their specific names. The fuel bundles have a distinct set of properties that are recovered and interpolated according to the specified global and local parameters. The interpolation of fuel properties with respect to burnup distribution can be performed according to the time-average or instantaneous models^[14]. The time-average calculation is performed in considering the bidirectional refuelling scheme of reactor channels and assuming that all channels have the same bundle-shift.

The modeling of the reactivity mechanisms is based on their specified parameters, which include the devices position, rods insertion level, water filling level, direction of movement, etc. The rod-devices insertion level can be set according to their nominal positions or they can be displaced in and out of core. The devices can also be divided into several groups so that they can be manipulated, displaced or moved simultaneously. The time-dependent behaviour of the moving devices can also be studied and used for the transient simulations or reactor control studies. The reactivity worth of devices can also be studied and predicted using DONJON.

The reactor material properties are essentially recovered from the reactor database, obtained from the lattice calculations using DRAGON code. The two distinct macroscopic cross-section libraries can be constructed using DONJON. The first MACROLIB is constructed only for the material properties which are evolution-independent, such as reflector and devices properties. The second MACROLIB is constructed only for the fuel properties, defined per each fuel bundle over the fuel lattice. The two libraries are next combined and updated, according to the devices insertion level. The produced extended MACROLIB is subsequently used to obtain the numerical solution, using TRIVAC modules.

Finally, it should be noted that the DONJON code development is permanently in progress. The future updates will provide several extended capabilities for the reactor design and calculations; they will

be gradually added to the subsequent DONJON versions.

2 GENERAL SPECIFICATION OF DONJON

2.1 Modules

Reactor calculations using DONJON are performed by means of sequential execution of several userselected modules, according to the user-defined computing scheme. Each module is designed to perform some particular tasks. The detailed description of DONJON modules is given in Section 3 to Section 6. In order to perform the reactor calculations, it is also required to use some DRAGON and TRIVAC modules. For more details on DRAGON modules specification, refer to its user guide^[4]; for more details on TRIVAC modules specification, refer to its user guide^[5]. Because the code execution is controlled by the GAN generalized driver, it is also possible to use its utility modules^[3,4]. A brief description of each module that can be executed using DONJON is given below. A short description of each data structure that can be used in DONJON is given in Section 2.2.

• The following DRAGON modules can be executed using DONJON:

GEO:	module used to create or modify a reactor geometry. The spatial locations of the reactor material mixtures must also be defined using the GEO: module. Only 3-D Cartesian reactor geometries are allowed with DONJON.
MAC:	module used to create or modify a MACROLIB containing the material properties, by directly specifying the group-ordered macroscopic cross-sections for each selected material mixture.
• The following	ng TRIVAC modules can be executed using DONJON:
TRIVAT:	module used to perform a $3-D$ numerical discretization or "tracking" of the reactor geometry.
TRIVAA:	module used to compute the set of system matrices with respect to the previously obtained "tracking" information.
FLUD:	module used to compute the numerical solution to an eigenvalue problem, correspond- ing to a previously obtained set of system matrices.
• The following	ng are short descriptions of utility modules that can be executed using DONJON:
UTL:	module used to perform several utility actions on a data structure.
DELETE:	module used to delete one or many data structures.
GREP:	module used to extract a single value from a data structure.

END: module used to delete all the local linked lists, to close all the remaining local files and to return from a procedure; or to terminate the overall DONJON execution controlled by the GAN generalized driver.

• The following are short descriptions of DONJON modules:

CRE:	module used to create a MACROLIB containing the material properties, by interpolating the nuclear properties from a mono-parameter database, previously generated in the lattice code.		
NCR:	module used to create a MICROLIB or a MACROLIB containing the material properties, by interpolating the nuclear properties from a multi-parameter database, previously generated in the lattice code.		
AFM:	module used to create a MACROLIB containing the material properties, by interpolating the nuclear properties from a multi-parameter feedback model database, previously generated in the lattice code.		
USPLIT:	module used to create an extended reactor material index over the whole mesh-splitted reactor geometry.		
RESINI:	module used to define the fuel lattice, to create the fuel-map geometry and to specify the global and local parameters.		
MACINI:	module used to create an extended MACROLIB, in which the properties are stored per each material region, over the whole mesh-splitted reactor geometry.		
DEVINI:	module used for $3-D$ modeling of rod-type devices in the reactor core.		
DETINI:	module used to read and store detector information.		
LZC:	module used for $3-D$ modeling of liquid zone controllers in the reactor core.		
DSET:	module used to set the new devices parameters, that can be used for the reactivity worth studies.		
MOVDEV:	module used to compute the time-dependent positions of the moving rod-type devices.		
NEWMAC:	module used to create an extended MACROLIB, that will contain the updated material properties, computed with respect to the actual devices positions.		
FLPOW:	module used to compute and print powers and normalized fluxes over the reactor core.		
TAVG:	module used to perform burnups calculation according to the time-average model, compute burnups integration limits, core-average exit burnup, axial power-shapes and channel refuelling rates.		
TINST:	module used to perform burnups calculation according to the time-linear model and compute instantaneous burnups values. This module is specific to Candu reactor refuelling.		
SIM:	module used to perform burnups calculation according to the time-linear model and compute instantaneous burnups values. This module is specific to PWR reactor refuelling.		
DETECT:	module used to compute the mean flux at each detector site and the response of each detector according to different types of interpolation.		
CVR:	module used for the core-voiding simulations.		
HST:	module used to manage a full reactor execution in DONJON using explicit DRAGON calculations for each cell (see Section 3.17). ^[18]		

2.2 Data structures

The transfer of information between the modules is performed by means of well defined data structures, also called objects. The objects can be defined in either create, read-only or modification mode. Each object has its own specific signature that can be easily recognized by a module. A detailed description of DONJON data structures is given in Section 7. For more details on DRAGON and TRIVAC data structures, refer to their guide^[17]. A brief description of all data structures that can be used in DONJON is given below.

GEOMETRY	data structure containing the geometry information. This object has a signature $\tt L_GEOM;$ it is created using DRAGON module <code>GEO:</code> .
MACROLIB	data structure containing the multigroup macroscopic properties; it has a signature L_MACROLIB. This object can be created in several modules, namely: using DRAGON modules MAC: and NCR:; or using DONJON modules CRE:, MACINI:, and NEWMAC:.
СОМРО	data structure containing the mono-parameter database, generated by the lattice code. This object has a signature L_COMPO ; it is created using DRAGON module CPO:.
MULTICOMPO	data structure containing the multi-parameter database, generated by the lattice code. This object has a signature L_MULTICOMPO; it is created using DRAGON module COMPO:.
SAPHYB	data structure containing the multi-parameter database, generated by the lattice code. This object has a signature L_SAPHYB; it is created using the APOLLO2 lattice code or the DRAGON module SAP:.
FMAP	data structure containing the fuel-lattice specification. This object has a signature L_MAP; it is created using DONJON module RESINI:.
MATEX	data structure containing the extended reactor material index. This object has a signature L_MATEX; it is created using DONJON module USPLIT:.
DEVICE	data structure containing the devices specification. This object has a signature L_DEVICE; it is created using DONJON module DEVINI:.
DETECT	data structure containing detector positions and responses. This object has a signature L_DETECT; it is created using DONJON module DETINI:, and can be modified by the modules DETINI: and DETECT: .
TRACK	data structure containing a "tracking" information of the reactor geometry. This object has a signature L_TRACK; it is created using TRIVAC module TRIVAT:.
SYSTEM	data structure containing a set of system matrices. This object has a signature L_SYSTEM; it is created using TRIVAC module TRIVAA:.
FLUX	data structure containing the numerical solution to an eigenvalue problem. This object has a signature L_FLUX; it is created using TRIVAC module FLUD:.
POWER	data structure containing the powers and normalized fluxes over the reactor core. This object has a signature L_POWER; it is created using DONJON module FLPOW:.
HISTORY	This data structure contains the information required to ensure a smooth coupling of DRAGON with DONJON when an history based full reactor calculation is to be performed. It is used only by the HST: module.

2.3 Syntactic rules for input specification

The input data to any module is read in free format using the subroutine **REDGET**. CLE-2000 variables^[21, 22] are also allowed. The user guide for DONJON is written using the following convention:

- the parameters surrounded by single square brackets '[]' denote an optional input;
- the parameters surrounded by double square brackets '[[]]' denote an input which may be repeated as many times as needed;
- the parameters in braces separated by vertical bars '{ | | }' denote a choice where one and *only* one input is mandatory;
- the parameters in **bold face** and in brackets '()' denote an input structure;
- the parameters in italics and in brackets with an index '(data(i), i = 1, n)' denote a set of n inputs;
- the words using the typewriter font KEYWORD are character constants used as keywords;
- the words in italics denote the user-defined variables: they are lower-case and of integer type (when starting from *i* to *n*), or of real type (when starting from *a* to *h* or from *o* to *z*); or they are upper-case and of character type *CHARACTER*.

2.4 General input structure

DONJON is built around the GAN generalized driver^[3, 22]. Accordingly, all the modules that will be used during the current execution must be first identified. It is also necessary to define the format of each object (data structure) that will be processed by these modules. Then, the modules required for the specific DONJON calculation are called successively, information being transferred from one module to the next via the objects. Finally, the execution of DONJON is terminated when it encounters the END: module, even if it is followed by additional data records in the input data stream. The general input data structure therefore follows the calling specifications given below:

Table	1:	Structure	(DONJON)
-------	----	-----------	----------

```
[ MODULE [[ MODNAME ]] ; ]
[ LINKED_LIST [[ STRNAME ]] ; ]
[ XSM_FILE [[ STRNAME ]] ; ]
[ SEQ_BINARY [[ STRNAME ]] ; ]
[ SEQ_ASCII [[ STRNAME ]] ; ]
[[ (module) ; ]]
END: ;
```

where

MODULE keyword used to specify the names of all modules that will be used in the current DONJON execution.

MODNAME character*12 name of a DONJON, or DRAGON, or TRIVAC, or utility module. The list of modules that can be executed using DONJON code is provided in Section 2.1.

LINKED_LIST	keyword used to specify the names of data structure that will be stored as linked lists.
XSM_FILE	keyword used to specify the names of all data structure that will be stored on XSM format files.
SEQ_BINARY	keyword used to specify the names of all data structure that will be stored on sequential binary files.
SEQ_ASCII	keyword used to specify the names of all data structures that will be stored on sequen- tial ASCII files.
STRNAME	character*12 name of a data structure. The list of data structure that can be used in DONJON is presented in Section 2.2.
(module)	input specification for a module that will be executed. For DONJON specific modules, these input structures are described in Section 3 to Section 6 .
END:	keyword to call the normal end-of-execution utility module.
;	keyword to specify the end of record. This keyword is used to delimit the part of the input data stream associated with each module.

Generally, the user has the choice to declare the most of data structure in the format of a linked list to reduce CPU times or as a XSM file to reduce memory resources. In general, the data structure are stored on the sequential ASCII files only for the backup purposes.

The input data normally ends with a call to the END: module. However, the GAN driver will insert automatically the END: module, even if it was not provided, upon reaching an end-of-file in the input stream.

Each (module) calling specification contains a module execution description and its associated input structure. All these modules, except the END: module may be called more than once.

3 GENERAL CORE-DESCRIPTION MODULES

3.1 The RESINI: module

The **RESINI**: module is used for modeling of the reactor fuel lattice in 3-D Cartesian geometry or 3-D Hexagonal geometry. This modeling is based on the following considerations:

• For 3-D Cartesian geometry, the reactor fuel lattice is composed of a well defined number of fuel channels. Each channel is composed of a well defined number of fuel bundles or assembly subdivisions. All channels contain the same number of fuel bundles or assembly subdivisions. Each reactor channel is identified by its specific name which corresponds to its position in the fuel lattice.

In a Candu reactor, the channels are refuelled according to the bidirectional refuelling scheme. The refuelling scheme of a channel corresponds to the number of displaced fuel bundles (bundle-shift) during each channel refuelling. The direction of refuelling corresponds to the direction of coolant flow along the channel.

In a PWR, a basic assembly layout can be projected over the fuel map using a naval-coordinate position system. Assembly refuelling and shuffling will be possible using the ad hoc module SIM: (see Section 3.13).

- For 3-D Hexagonal geometry, the reactor fuel lattice is composed of a well defined number of fuel channels and each channel is composed of a well defined number of fuel bundle. All fuel bundles have the same volume. All channels contain the same number of fuel bundles. Refuelling is not available during the calculation. The lattice indexation is kept to identify the hexagons.
- The fuel regions generally have a different set of global and local parameters. For example, the fuel bundles have a different evolution of the fuel properties according to the given burnup distribution, which is a global parameter. Consequently, the homogenized cell properties will differ from one fuel region to another, i.e., they are not uniform over the fuel lattice. Thus, the realistic modeling of a reactor core requires the fuel properties to be interpolated with respect to global and local parameters, which must be specified in the fuel map.

Note that the above considerations correspond to the typical core modeling of CANDU or PWR reactors. The RESINI: module will create a new FMAP object that will store the information related to the fuel lattice specification and properties (see Section 7.1).

The **RESINI**: module specifications are:

Table 2: Structure RESINI:

{ FLMAP MATEX := RESINI: MATEX :: (descresini1) |
FLMAP := RESINI: FLMAP :: (descresini2) }

where

FLMAPcharacter*12 name of the RESINI object that will contain the fuel-lattice information.
If FLMAP appears on both LHS and RHS, it will be updated; otherwise, it is created.MATEXcharacter*12 name of the MATEX object specified in the modification mode.
MATEX is required only when FLMAP is created.

(descresini1) structure describing the main input data to the RESINI: module. Note that this input data is mandatory and must be specified only when *FLMAP* is created.

(descresini2) structure describing the input data for global and local parameters. This data is permitted to be modified in the subsequent calls to the RESINI: module.

3.1.1 Main input data to the RESINI: module

Note that the input order must be respected.

Table 3: Structure (descresini1)

```
 \begin{bmatrix} \texttt{EDIT } \textit{iprint} \end{bmatrix} \\ \texttt{::: GEO: (descgeo)} \\ \texttt{NXNAME } ( \textit{XNAME(i)}, i = 1, nx ) \\ \texttt{NYNAME } ( \textit{YNAME(i)}, i = 1, ny ) \\ \texttt{NCOMB } \{ \textit{ncomb } \texttt{B-ZONE } (\textit{icz(i)}, i = 1, nch ) | \texttt{ALL} \} \\ \begin{bmatrix} \texttt{SIM } lx \ ly \ (\textit{naval(i)}, i = 1, nch ) \end{bmatrix} \\ \texttt{(descresini2)} \end{cases}
```

where EDIT

keyword used to set *iprint*.

iprint integer index used to control the printing on screen: = 0 for no print; = 1 for minimum printing (default value); larger values produce increasing amounts of output.

- ::: keyword used to indicate the call to an embedded module.
- GEO: keyword used to call the GEO: module. The fuel-map geometry differs from the complete reactor geometry in the sense that it must be defined as a coarse geometry, i.e. without mesh-splitting over the fuel bundles. Consequently, the mesh-spacings over the fuel regions must correspond to the bundle dimensions (e.g. $h_x = width$; $h_y = height$; $h_z = length$ or in 3-D Hexagonal geometry $h_x = side$; $h_z = height$). Note that the total number of non-virtual regions in the embedded geometry must equal to the number of fuel channels times the number of fuel bundles per channel. This means that only the fuel-type mixture indices are to be provided in the data input to the GEO: module for MIX record. Other material regions (e.g. reflector) must be declared as virtual, i.e. with the mixtures indices set to 0.
- (descgeo) structure describing the input data to the GEO: module (see the user guide^[4]). Only 3-D Cartesian or 3-D Hexagonal fuel-map geometry is allowed.
- NXNAME keyword used to specify XNAME. Not used for 3-D Hexagonal geometry.
- XNAME character*2 array of horizontal channel names. A horizontal channel name is identified by the channel column using numerical characters '1', '2', '3', and so on. Note that the total number of X-names must equal to the total number of subdivisions along the X-direction in the fuel-map geometry. All non-fuel regions are to be assigned a single character '-'. This option is not available for 3-D Hexagonal geometry.

nx	integer total number of subdivisions along the X-direction in the fuel-map geometry. Not used for 3-D Hexagonal geometry.	
NYNAME	keyword used to specify $YNAME$. Not used for 3-D Hexagonal geometry.	
YNAME	character*2 array of vertical channel names. A vertical channel name is identified by the channel row using alphabetical letters 'A' (from the top), 'B', 'C', and so on. The total number of Y-names must equal to the total number of subdivisions along the Y-direction in the fuel-map geometry. All non-fuel regions are to be assigned a single character '-'. This option is not available for 3-D Hexagonal geometry.	
ny	integer total number of subdivisions along the Y-direction in the fuel-map geometry. Not used for $3\text{-}D$ Hexagonal geometry.	
NCOMB	keyword used to specify the number of combustion zones.	
ncomb	integer total number of combustion zones. This value must be greater than (or equal to) 1 and less than (or equal to) the total number of reactor channels.	
B-ZONE	keyword used to specify <i>icz</i> .	
icz	integer array of combustion-zone indices, specified for every channel. A reactor channel can belong to only one combustion zone, however a combustion zone can be specified for several channels.	
ALL	keyword used to indicate that the total number of combustion zones equals to the number of reactor channels. In this particular case, each channel will have a unique combustion-zone number. Hence, an explicit specification of the combustion-zone in- dices can be omitted.	
nch	$N_{\rm ch}$: number of fuel channels in the radial plane.	
nb	$N_{\rm b}$: number of fuel bundles or assembly subdivisions in the axial plane.	
SIM	keyword used to specify a basic assembly layout for the SIM: PWR refuelling module (see Section 3.13).	
lx	number of assemblies along the X axis. Typical values are 15 or 17.	
ly	number of assemblies along the Y axis.	
naval	 character*3 identification name corresponding to the basic naval-coordinate position of an assembly. <i>naval</i>(i) is the concatenation of a letter (generally chosen between A and T) and of an integer (generally chosen between 01 and 17). An assembly may occupies four positions in the fuel map in order to be represented by four radial burnups. In this case, the same naval-coordinate value will appear at four different (i) indices. 	

$3.1.2\ {\rm Input}$ of global and local parameters

The information with respect to the fuel burnup is required for the fuel-map MACROLIB construction, using either the CRE:, NCR: or AFM: module. The fuel-region properties related to other local or global parameters can be interpolated only using the NCR: module.

[EDIT iprint]
[BTYPE { TIMAV-BURN | INST-BURN }]
[TIMAV-BVAL (bvalue(i), i = 1, ncomb)]
[INST-BVAL { SAME bvalue | CHAN (bvalue(i), i = 1, nch) | BUND (bvalue(i), i = 1, nch·nb) |
SMOOTH }]
[BUNDLE-POW { SAME pwvalue | CHAN (pwvalue(i), i = 1, nch) | BUND (pwvalue(i), i = 1, nch·nb) }]
[REF-SHIFT { ishift | COMB (ishift(i), i = 1, ncomb) }]
[(ADD-PARAM PNAME PNAME PARKEY PARKEY { GLOBAL | LOCAL }]]
[[SET-PARAM PNAME { pvalue | { [TIMES PNAMEREF] SAME pvalue | CHAN (pvalue(i), i = 1, nch) | BUND (pvalue(i), i = 1, nch·nb) }]]
[[FUEL { WEIGHT | ENRICH | POISON } (fvalue(i), i = 1, nfuel)]]
[CELL (ialch(i), i = 1, nch)]

where

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); $= 2$ to print the channels refuelling schemes (if they are new or modified); $= 3$ initial burnup limits per each channel are also printed (if the axial power-shape has been reinitialized).
ВТҮРЕ	keyword used to specify the type of interpolation with respect to burnup data. This information will be used during the execution of CRE:, NCR: or AFM: module.
TIMAV-BURN	keyword used to indicate the burnups interpolation according to the time-average model. This option is not available in 3 - D Hexagonal geometry.
INST-BURN	keyword used to indicate the burnups interpolation according to the instantaneous model.
TIMAV-BVAL	keyword used to indicate the input of average exit burnup values per each combustion zone. Note that the axial power-shape and the first burnup limits will be reinitialized each time the average exit burnups are modified by the user. These data are required for the time-average calculation (see Section 3.11). This option is not available with $3-D$ Hexagonal geometry.
INST-BVAL	keyword used to specify the instantaneous burnup values for each fuel bundle.
SMOOTH	keyword used to level fuel mixtures burnup. If the burnup is supposed to be the same at each occurence of every fuel mixture (for symetry reasons), SMOOTH will make sure they share the exact same value (the first one in the burnup map). Purpose is only to correct calculation noise in historic calculation.
BUNDLE-POW	keyword used to specify the power values for each fuel bundle. This option is not available in $3\text{-}D$ Hexagonal geometry.
bvalue	real array containing the burnups values, given in $MW \cdot day \ per \ tonne/MW$ of initial heavy elements. The fuel burnup is considered as a global parameter.
pwvalue	real array containing the powers values, given in kW.

REF-SHIFT	keyword used to specify <i>ishift</i> . Note that the axial power-shape and the first burnup limits will be reinitialized each time the channel refuelling schemes are modified by the user. This option is not available in $3-D$ Hexagonal geometry.
COMB	keyword used to indicate the input of bundle-shift numbers per combustion zone.
ishift	integer array (or single value) of the bundle-shift numbers. A single <i>ishift</i> value means that the same bundle-shift will be applied for all combustion zones. Note that the bundle-shift value must be positive, it corresponds to the number of displaced fuel bundles during each channel refuelling.
ADD-PARAM	keyword used to indicate the input of information for a new global or local parameter. For more information about the parameter data organization on FMAP data structure see Section $7.1.5$.
PNAME	keyword used to specify <i>PNAME</i> .
PNAME	<pre>character*12 identification name of a given parameter. This name is user-defined so that it is arbitrary, however it must be unique so that it can be used for the search of parameter information and interpolation purpose. Moreover, it is recommended to use the following pre-defined values: C-BORE Boron concentration</pre>
	T-FUELAveraged fuel temperatureT-SURFSurfacic fuel temperatureT-COOLAveraged coolant temperatureD-COOLAveraged coolant densityCANDU-only parameters:
	T-MODEAveraged moderator temperatureD-MODEAveraged moderator density
PARKEY	keyword used to specify <i>PARKEY</i> .
PARKEY	character*12 corresponding name of a given parameter as it is recorded in the par- ticular multi-parameter compo file. The <i>PARKEY</i> name of a parameter may not be same as its <i>PNAME</i> and can also differ from one multi-compo file to another.
GLOBAL	keyword used to indicate that a given parameter is global, which will have a single and constant parameter's value.
LOCAL	keyword used to indicate that a given parameter is local. In this case, the total number of recorded parameter's values will be set to $N_{\rm ch} \times N_{\rm b}$.
SET-PARAM	keyword used to indicate the input (or modification) of the actual values for a parameter specified using its $PNAME$.
SAME	keyword used to indicate that a core-average value of a local parameter will be pro- vided. If the keyword SAME is specified, then this average value will be set for all fuel bundles for every reactor channel.
CHAN	keyword used to indicate that the values of a local parameter will be provided per each reactor channel. If the keyword CHAN is specified, then the channel-averaged parameter's value will be set for all fuel bundles containing in the same reactor channel.
BUND	keyword used to indicate that the values of a local parameter will be specified per each fuel bundle for every channel.
TIMES	keyword used to indicate that the values of the local parameter $PNAME$ is a translation of the local parameter $PNAMEREF$ via a multiplication of the constant indicated by SAME.

PNAMEREF	character*12 identification name of a given parameter.
pvalue	real array (or a single value) containing the actual parameter's values. Note that these values will not be checked for consistency by the module. It is the user responsibility to provide the valid parameter's values which should be consistent with those recorded in the multicompo database.
FUEL	keyword used to indicate the input of data which will be specified for each fuel type.
WEIGHT	keyword used to indicate the input of fuel weight in a bundle, given in kg .
ENRICH	keyword used to indicate the input of fuel enrichment values, given in $wt\%$.
POISON	keyword used to indicate the input of poison load in a fuel.
fvalue	real value of the fuel-type parameter, specified for each fuel type in the same order as the fuel mixture indices have been recorded in the MATEX object (see Section 3.2.1).
nfuel	integer total number of the fuel types, as been defined in the USPLIT: module.
CELL	keyword used to specify that a patterned age distribution will be input and used to compute instantaneous bundle burnup.
ialch	real array containing the refueling sequence numbers. This channel is refueled the $ialch(i)$ th one. The channels are ordering from the top left to the bottom right of the core. The expression of the resulting bundle burnups are given in Ref. 19.

3.2 The USPLIT: module

The USPLIT: module is used to create a MATEX object that will provide a link between the reactor geometry and material index. The 3-D Cartesian or 3-D Hexagonal reactor geometry, which is previously produced in the GEO: module, is analyzed and the material mixture indices are recomputed in order to provide a unique mixture number for each material sub-volume. Such renumbering permits a complex reactor core modeling. A MATEX object is also used to store some additional information that will be required and updated by other DONJON modules (see Section 7.2).

The USPLIT: module specification is:

Table 5: Structure USPLIT:

GEOM MATEX := USPLIT: { GEOM | GEOMOLD } :: (desclink)

where

GEOM	character*12 name of a GEOMETRY object. This object is defined in creation (appears only on LHS) or modification (appears on both LHS and RHS) mode. An existing geometry previously created in the GEO: module is modified. Only 3-D Cartesian or 3-D Hexagonal reactor geometries are allowed.
MATEX	character*12 name of a MATEX object to be created by the module.
GEOMOLD	character*12 name of a GEOMETRY object previously created in the GEO: module. This object must be specified in read-only mode (appears only on RHS). It is copied into <i>GEOM</i> at the beginning of USPLIT: module. Only 3-D Cartesian or 3-D Hexagonal reactor geometries are allowed.
(desclink)	structure describing the input data to the USPLIT: module.

3.2.1 Input data to the USPLIT: module

Note that the fuel-type and reflector-type mixture indices are need to be specified explicitly and the input order must be respected.

Table 6: Structure (desclink)

[EDIT iprint]
NGRP ngrp
MAXR maxreg
NMIX nmixt
[NREFL nrefl RMIX (mixr(i) , i = 1, nrefl)]
[NFUEL nfuel FMIX (mixf(i) , i = 1, nfuel)]
;

where	
EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); larger values produce increasing amounts of output.
NGRP	keyword used to specify <i>ngrp</i> .
ngrp	integer total number of energy groups. This value must be greater than 0.
MAXR	keyword used to specify <i>maxreg</i> .
maxreg	integer maximum number of mesh-splitted regions in the reactor geometry. In 3-D Hezagonal geometry, it corresponds to the total number of prismatic blocks l_h*l_z .
NMIX	keyword used to extend number of material mixtures in case new fuels are going to be inserted in the fuel map in upcoming fuel cycles. By default, <i>nmixt</i> is set to the maximum mixture index in RHS geometry <i>GEOM</i> or <i>GEOMOLD</i> .
nmixt	the maximum fuel mixture index in the complete life of the reactor. This number must be greater than the maximum mixture index in RHS geometry <i>GEOM</i> or <i>GEOMOLD</i> .
NREFL	keyword used to specify <i>nrefl</i> .
nrefl	integer total number of reflector types. A reactor should have at least one reflector material.
RMIX	keyword used to specify <i>mixr</i> .
mixr	integer array of the reflector-type mixture indices. Each reflector type is assigned a distinct mixture number as previously defined in the GEOMETRY object.
NFUEL	keyword used to specify <i>nfuel</i> .
nfuel	integer total number of fuel types. A reactor should have at least one fuel type.
FMIX	keyword used to specify <i>mixf</i> .
mixf	integer array of the fuel-type mixture indices. Each fuel type is assigned a distinct mixture number as previously defined in the GEOMETRY object.

3.3 The MACINI: module

The MACINI: module is used to construct an extended MACROLIB, in which the properties are stored per each material region over the whole mesh-splitted reactor geometry. This MACROLIB is obtained by combining the material properties which are contained in the two distinct MACROLIB objects:

- The first MACROLIB contains the material properties which are evolution-independent, such as reflector and device properties. It is created using either MAC:, CRE:, NCR: or AFM: module.
- The second is a fuel-map MACROLIB created using either CRE:, NCR: or AFM: module. It must contain the interpolated fuel properties per each fuel bundle.

The resulting MACROLIB will contain the properties that are stored for each reactor material and per each mesh-splitted volume. When the devices are not present in the reactor core, then the resulting MACROLIB can be considered as a complete reactor MACROLIB and it can be directly used for the numerical solving. However, when the devices are inserted into the reactor core, the resulting MACROLIB is not yet complete; it must be subsequently updated with respect to the device properties, using the NEWMAC: module (see Section 3.9).

The MACINI: module specification is:

Table 7: Structure MACINI:

MACRO2 MATEX := MACINI: MATEX MACRO [MACFL] :: [EDIT iprint] ;

where

MACRO2	$\tt character*12$ name of the extended MACROLIB to be created by the module.
MATEX	character*12 name of the MATEX object containing an extended material index over the reactor geometry. <i>MATEX</i> must be specified in the modification mode; it will store the recovered h-factors per each fuel region.
MACRO	character*12 name of a MACROLIB, created using either MAC:, CRE:, NCR: or AFM: module, for the evolution-independent material properties (see structure (desccre1) or refer to the user guide ^[4]).
MACFL	character*12 name of a fuel-map MACROLIB, created using either CRE:, NCR: or AFM: module, for the interpolated fuel properties (see structure (desccre2) or refer to the user guide ^[4]).
EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing; larger values produce increasing amounts of output. The default value is $iprint = 1$.

3.4 The DEVINI: module

The DEVINI: module is used for the modeling of reactivity mecanisms, based on the devices specifications which are read from the input data file. The module will create a new DEVICE object that will store the devices specifications and parameters (see Section 7.3). Note that only the rod-type (i.e. solid) devices are considered using the DEVINI: module; the liquid zone controllers can be added subsequently, using the LZC: module (see Section 3.6). A rod-type device is a reactivity controller rod (or plate), such as: a zone control rod (ZCR), a shutoff rod (SOR), etc. Several devices parameters can be modified using the DSET: module (see Section 3.7).

A device specification includes several controller rod parameters, such as: a rod position, rod insertion level, direction of movement, etc. The devices positions can not overlap in the reactor core; they are referred using 3-D-Cartesian coordinates. The insertion level of rods can be set according to their nominal positions or they can be displaced *in* or *out* of core. The rods can also be divided into the several user-defined groups so that they can be manipulated, displaced or moved simultaneously.

The **DEVINI**: module specification is:

Table 8: Structure DEVINI:

DEVICE MATEX := DEVINI: MATEX :: (descdev)

where

DEVICE	character*12 name of the DEVICE object that will be created by the module; it will contain the devices information.
MATEX	character*12 name of the MATEX object that will be updated by the module. The rod-devices material mixtures are appended to the previous material index and the rod-devices indices are also modified, accordingly.
(descdev)	structure describing the input data to the DEVINI : module.

3.4.1 Input data to the DEVINI: module

The DEVINI: module allows the definition of rod-type devices made of one or many (up to 10) parts, as depicted in Fig. 1.

Table 9: Structure (descdev)

```
[ EDIT iprint ]
NUM-ROD nrod [ { FADE | MOVE } ]
( (dev-rod), i = 1, nrod )
[ CREATE ROD-GR ngrp ( (rod-group), i = 1, ngrp ) ]
;
```



Figure 1: Presentation of fully- and partially-inserted 3-part control rods.

where

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); larger values produce increasing amounts of output.
NUM-ROD	keyword used to specify <i>nrod</i> .
nrod	integer total number of the reactor rod-type devices. This number must be greater than 0.
FADE	fading rod keyword. A fraction of the fully inserted rod vanishes (default option).
MOVE	moving rod keyword. The complete rod is moving (DONJON3-type movement).
CREATE	keyword used to create the rod-groups of devices. The creation of groups is optional.
ROD-GR	keyword used to set <i>ngrp</i> .
ngrp	integer total number of the rod groups to be created. This number must be greater than 0.
(dev-rod)	structure describing the input data for each individual rod.
(rod-group)	structure describing the input data for each group of rods.

3.4.2 Description of dev-rod input structure

A rod position is referred by its 3-D Cartesian coordinates only. Note that the devices positions can not overlap. The input order of data must be respected.

ROD id
ROD-NAME NAME
AXIS { $X Y Z$ }
FROM { $H+ H- $ }
[LEVEL value]
[SPEED speed]
[TIME time]
[[MAXPOS (pos(i), i = 1, 6) DMIX mix1 mix2]]
ENDROD

where

ROD	keyword used to specify the rod <i>id</i> number.
id	integer identification number of the current rod. Each rod-type device must be assigned a unique <i>id</i> number, given in an ascending order ranging from 1 to <i>nrod</i> .
ROD-NAME	keyword used to specify the rod NAME.
NAME	character*12 name of the current rod. In general, this name is composed by the rod specific type (e.g. SOR, ZCR, etc.) followed by its sequential number (e.g. 01, 02, etc.).
AXIS	keyword used to specify the rod movement axis. A rod can be displaced along only one of the axis.
X	keyword used to specify that a rod is displaced along X axis.
Y	keyword used to specify that a rod is displaced along Y axis.
Z	keyword used to specify that a rod is displaced along Z axis.
FROM	keyword used to specify the insertion side of geometry. The rod-devices can be inserted into the reactor core from only one side of geometry. For example, some vertically moving devices can be inserted only from the top, whereas other only from the bottom.
H+	keyword used to specify that a rod will be inserted into reactor core from the highest position (e.g. from the top for vertically moving rod-device).
Н-	keyword used to specify that a rod will be inserted into reactor core from the lowest position (e.g. from the bottom for vertically moving rod-device).
LEVEL	keyword used to specify the actual rod insertion level <i>value</i> . By default, the rod insertion level is left undefined.
value	real positive value of the rod insertion level. This value is used to compute the actual rod position in the reactor core. The rod insertion level is minimal (value = 0.0) when the rod is completely withdrawn, and it is maximal (value = 1.0) when the rod is fully inserted. For the partially inserted rod the insertion level must be: $0.0 < value < 1.0$
SPEED	keyword used to specify <i>speed</i> . By default, the speed is left undefined.
speed	real positive value of the rod movement speed, given in cm/s. This value is needed only for the reactor regulating purpose.

TIME	keyword used to specify <i>time</i> . By default, the insertion time is left undefined.
time	real value of time for the rod insertion (or extraction), given in sec. This value is needed only for the reactor regulating purpose.
MAXPOS	keyword used to specify the full-inserted coordinates of a rod part. The sequence of MAXPOS and DMIX data structures is repeated for each part making the rod.
pos	real array containing 3-D Cartesian coordinates of the full-inserted rod. This is the limiting rod position in the reactor core, which may or may not be the same as the actual rod position. These coordinates must be given in the order: $X-$, $X+$, $Y-$, $Y+$, $Z-$, and $Z+$.
DMIX	keyword used to specify $mix1$ and $mix2$.
mix1	first of two integer rod mixture indices. Index $mix1$ corresponds to the perturbed cross sections.
mix2	second of two integer rod mixture indices. Index $mix2$ corresponds to the reference cross sections. Indices $mix1$ and $mix2$ will be used to compute the incremental cross sections in the NEWMAC: module.
ENDROD	keyword used to end the rod description.

3.4.3 Description of rod-group input structure

The partition of devices into groups is very useful when the same action is to be applied to several rods, e.g. setting of new parameters (using the DSET: module) or rods moving (using the MOVDEV: module).

Table 11: Structure (rod-group)

GROUP-ID igrp { ROD-ID [[id]] | ALL }

where

GROUP-ID	keyword used to set <i>igrp</i> number.
igrp	integer identification number of a group to be created. Each rods group must be assigned a unique identification number, given in ascending order ranging from 1 to $ngrp$.
ROD-ID	keyword used to set the rod <i>id</i> numbers.
id	integer identification numbers of rods which belong to the same group <i>igrp</i> . A particular rod (or several rods) may belong to different groups, but it could not be repeated inside the same group. The total number of rods in any group must be between 1 and <i>nrod</i> .
ALL	keyword used to specify that all rods will belong to the same group <i>igrp</i> .

3.5 The DETINI: module

The DETINI: module is used to read and store detector information. A detector is represented by a 2-D or 3-D Cartesian/Hexagonal geometry.

The DETINI: module specification is:

Table 12: Structure DETINI:

DETECT := DETINI: [DETECT] :: (descdet)

where

DETECT	character*12 name of the DETECT object that will be created by the module; it will
	contain the detector informations. If DETECT appear on RHS, it is updated, otherwise,
	it is created.

(descdev) structure describing the input data to the DETINI: module.

3.5.1 Input data to the DETINI: module

Note that the input order must be respected.

Table 13: Structure (descinidet)

```
[ EDIT iprt ] [ HEXZ ] NGRP ngrp
[[ TYPE NAMTYP
INFO ndetect nrep { SPECTRAL ( spec(i), i=1,ngrp ) | DEFAULT }
[ INVCONST ( tinv(i), i=1,nrep-2 ) ] [ FRACTION ( fract(i), i=1,nrep-1 ) ]
( (descdet), i=1,ndetect ) ]];
```

where EDIT

keyword used to set *iprt*.

- iprt index used to control the printing in module INIDET:. =1,2 for no print(default value); =3 for printing the contents of the output DETECT.
- HEXZ keyword to specify that only hexagonal detectors will be defined. If this keyword is absent, Cartesian detectors will be defined.

NGRP keyword used to set ngrp.

ngrp number of energy groups in the calculation. It must be equal to the number set in the MACD: module or by the COMPO files.

TYPE	keyword to specify the detector type.
NAMTYP	character*12 name of the detector type. To correspond to the actual detector response model encoded, the type of detector must be in this list:
	• PLATN_REGUL
	• PLATN_SAU
	• VANAD_REGUL
	• CHION_SAU
	• CHION_REGUL
	For other type names, only a fixed normalisation can be performed.
INFO	keyword to specify the information associated with the detector type.
ndetect	number of detectors of the specified type.
nrep	number of detector response components for the specified type. It must be greater or equal to 2, corresponding to a response in fraction and the reference flux value.
SPECTRAL	keyword to specify the energy spectral of a detector type.
spec	array containing the energy spectral of a detector type.
DEFAULT	keyword to specify the energy spectral will be initialized as 1.0 for the highest energy group and 0.0 for other groups.
INVCONST	keyword to specify the inverse time constants of the detector type model. This option is only valid for platinum, $(NAMTYP(1:5) = 'PLATN')$, detector type.
tinv	array containing the inverse time constants of the detector model.
FRACTION	keyword to specify the fractions corresponding to each delayed or prompt reponse of the detector type model. This option is only valid for platinum, $(NAMTYP(1:5) = PLATN')$, detector type.
frac	array containing the detector type model fractions.
$(\mathrm{descdet})$	structure describing the format used to read detector information.

3.5.2 Description of the detector data

Note that the information input order must be respected.

Table 14: Structure (descdet)

```
NAME NAMDET [ NHEX nhex HEX ( ihex(i), i=1,nhex ) ] POSITION ( pos(i), i=1,6 ) RESP ( rep(i), i=1,nrep ) ENDN
```

where	
NAME	keyword to specify the detector name.
NAMDET	<pre>character*12 name of the detector. The different names in alphabetical order must fit their usual numbering in the core.(Ex: PLATN01, CHION01C)</pre>
NHEX	keyword to set the number of hexagons where the detector is placed.
nhex	number of hexagons.
HEX	keyword to set the hexagon numbers corresponding to the detector position.
ihex	array containing the hexagon numbers where the detector is present, as ordered in the geometry definition.
POSITION	keyword to specify the detector coordinates.
pos	array containing the positions of the specified detector. The positions must be read as $X-X+Y-Y+Z-Z+$. For 2-D geometry, Z coordinates must be 0.0 and a value greater than 1.0. For hexagonal geometry, only Z coordinates are used in 3-D representation.
RESP	keyword to specify the detector initial responses.
rep	array containing the initial responses of the detector. To use the current detector models in DONJON, responses are given as
	• For vanadium detectors: current response, last response.
	• For platinum detectors: current response, reference flux, last detector slow responses.
	• For ion chamber detectors: current logarithmic response, current log rate response, reference flux.
ENDN	keyword to specify the end of the detector informations.

3.6 The LZC: module

The LZC: module is used for the modeling of liquid zone controllers, which are normally presented in the CANDU6-type reactor core. The liquid zone controllers specifications are read from the input data file. Note that this modeling can be made after the rod-type devices have been previously defined using the DEVINI: module (see Section 3.4). In this case, the previously created DEVICE object will be updated by the LZC: module; it will store the additional and separate information with respect to the liquid controllers (see Section 7.3).

The liquid zone controller specification includes several device parameters, such as: the whole device position, water filling level, direction of filling, etc. Note that a liquid zone controller is normally composed of two parts: one part is empty and the second part is full-filled. The water level can be adjusted according to the control reactivity requirements. The controllers positions are referred using 3-D-Cartesian coordinates. Several devices parameters can be modified using the DSET: module (see Section 3.7). The liquid controllers can also be divided into the several user-defined groups so that they can be manipulated simultaneously.

The LZC: module specification is:

Table 15: Structure LZC:

DEVICE MATEX := LZC: [DEVICE] MATEX :: (desclzc)

where

DEVICE	character*12 name of the DEVICE object. Note, if the rod-type devices are not present in the reactor core, then <i>DEVICE</i> object must appear only on the LHS (i.e. in create mode), it will contain the information only with respect to the liquid zone controllers. However, if the rod-type devices are present in the reactor core, then they must be specified first (i.e. before the liquid controllers) using the DEVINI : module (see Section 3.4). In the last case, the <i>DEVICE</i> object must also appear on the RHS (i.e. in modification mode), it will contain the additional and separate information with respect to the liquid zone controllers.
MATEX	character*12 name of the MATEX object that will be updated by the module. The lzc-devices material mixtures are appended to the previous material index and the lzc-devices indices are also modified, accordingly.
(desclzc)	structure describing the input data to the LZC: module.

3.6.1 Input data to the LZC: module

Note that the input order must be respected.

```
[ EDIT iprint ]
NUM-LZC nlzc
((dev-lzc), i = 1, nlzc)
[ CREATE LZC-GR ngrp ((lzc-group), i = 1, ngrp) ]
;
```

where

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); larger values produce increasing amounts of output.
NUM-LZC	keyword used to specify <i>nlzc</i> .
nlzc	integer total number of liquid zone controllers. This number must be greater than 0.
CREATE	keyword used to create the lzc-groups of devices. The creation of groups is optional.
LZC-GR	keyword used to set <i>ngrp</i> .
ngrp	integer total number of the lzc groups to be created. This number must be greater than 0.
(dev-lzc)	structure describing the input data for each individual liquid controller.
(lzc-group)	structure describing the input data for each group of liquid controllers.

3.6.2 Description of dev-lzc input structure

Note that the devices positions can not overlap in the reactor core. The input order of data must be respected.

Table 17: Structure (dev-lzc)

LZC id
MAXPOS ($pos(i)$, $i = 1, 6$)
MAX-FULL fmax
AXIS $\{ X \mid Y \mid Z \}$
LEVEL value
[RATE rate]
[TIME time]
EMPTY-MIX ($mixE(n), n = 1, 2$
FULL-MIX ($mixF(n), n = 1, 2$)

)

where	
LZC	keyword used to specify the liquid controller <i>id</i> number.
id	integer identification number of the current liquid controller. Each controller must be assigned a unique id number, given in an ascending order ranging from 1 to $nlzc$.
MAXPOS	keyword used to specify the entire position of a liquid zone controller, including its empty and full parts.
pos	real array containing 3-D Cartesian coordinates of the liquid zone controller position in the reactor core. These coordinates must be given in the order: X– X+ Y– Y+ Z– Z+
MAX-FULL	keyword used to specify <i>fmax</i> .
fmax	real value of the limiting coordinate along the controller filling axis, which corresponds to the maximum full-filling level for the current liquid controller.
AXIS	keyword used to specify the controller filling axis. A liquid controller can be filled along only one (vertical) axis.
Х	keyword used to specify that a liquid controller is filled along X axis.
Y	keyword used to specify that a liquid controller is filled along Y axis.
Z	keyword used to specify that a liquid controller is filled along Z axis.
LEVEL	keyword used to specify the actual filling level.
value	real positive value of the water level. This value is minimal (value = 0.0) when the controller is empty, and it is maximal (value = 1.0) when the controller is full-filled. For the partially filled controller the water level must be: $0.0 < value < 1.0$
RATE	keyword used to specify <i>rate</i> .
rate	real positive value of the water filling rate, given in m^3/s . This value is needed only for the reactor regulating purpose.
TIME	keyword used to specify <i>time</i> .
time	real value of the filling time, given in sec. This value is needed only for the reactor regulating purpose.
EMPTY-MIX	keyword used to specify $mixE$.
mixE	two integer mixture indices, specified for the empty-part of liquid controller. The first and the second mixture indices correspond to the perturbed and the reference cross sections, respectively. These indices will be used to compute the incremental cross sections in the NEWMAC: module.
FULL-MIX	keyword used to specify $mixF$.
mixF	two integer mixture indices, specified for the full-part of liquid controller. The first and the second mixture indices correspond to the perturbed and the reference cross sections, respectively. These indices will be used to compute the incremental cross sections in the NEWMAC: module.

3.6.3 Description of lzc-group input structure

The partition of lzc-devices into groups is similar to that of rod-devices.

Table 18: Structure (lzc-group)

GROUP-ID igrp { LZC-ID [[id]] ALL }	

where

GROUP-ID	keyword used to set <i>igrp</i> number.
igrp	integer identification number of a group to be created. Each controllers group must be assigned a unique identification number, given in ascending order ranging from 1 to $ngrp$.
LZC-ID	keyword used to set the controllers <i>id</i> numbers.
id	integer identification numbers of the liquid controllers which belong to the same group $igrp$. A particular controller (or several devices) may belong to different groups, but it could not be repeated inside the same group. The total number of liquid controllers in any group must be between 1 and $nlzc$.
ALL	keyword used to specify that all liquid controllers will belong to the same group $igrp$.

3.7 The DSET: module

The DSET: module is used to set or to update some of the devices parameters. The new parameters can be applied for the rod-type devices and/or for the liquid zone controllers, such as: the new insertion level for the rods or water filling level for the lzc-type devices, etc. It is possible to apply the new parameters to the individual user-selected devices as well as to the user-selected groups of devices. If the device (rod-insertion or lzc-filling) level is selected for the modification, then a new device position is recomputed accordingly. The DSET: module can be used to perform the device reactivity studies and also to predict the reactivity worth of the rod-devices.

The DSET: module specification is:

Table 19: Structure DSET:

DEVICE := DSET: DEVICE :: (descdset)

where

DEVICE character*12 name of the DEVICE object that will be updated by the module.

(descdset) structure describing the input data to the DSET: module.

3.7.1 Input data to the DSET: module

It is possible to set or to modify the parameters for several individual devices and/or for several groups of devices simultaneously.

Table 20: Structure (descdset)

EDIT <i>iprint</i>
[[{ ROD <i>irod</i> ROD-GROUP <i>irgrp</i> LZC <i>ilzc</i> LZC-GROUP <i>ilgrp</i> }
[LEVEL value] [SPEED speed] [TIME time]
END]]
;

where	
EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing; larger values produce increasing amounts of output.
ROD	keyword used to specify the rod <i>irod</i> number.
irod	integer identification number of a rod to be modified. Each rod-type device has a

	unique <i>irod</i> number, ranging from 1 to <i>nrod</i> , as been defined in the DEVINI: module (see Section $3.4.2$).
ROD-GROUP	keyword used to specify the rod-group <i>irgrp</i> number.
irgrp	integer identification number of a rod-group of devices that will be modifed with the same parameters. Each rod-group has a unique <i>irgrp</i> number, ranging from 1 to <i>ngrp</i> , as been defined in the DEVINI: module (see Section 3.4.3).
LZC	keyword used to specify the liquid controller $ilzc$ number.
ilzc	integer identification number of a liquid controller to be modified. Each lzc-type device has a unique <i>ilzc</i> number, ranging from 1 to <i>nlzc</i> , as been defined in the LZC: module (see Section $3.6.2$).
LZC-GROUP	keyword used to specify the lzc-group <i>ilgrp</i> number.
ilgrp	integer identification number of a lzc-group of devices that will be modifed with the same parameters. Each lzc-group has a unique <i>ilgrp</i> number, ranging from 1 to <i>ngrp</i> , as been defined in the LZC: module (see Section $3.6.3$).
LEVEL	keyword used to specify a new level <i>value</i> .
value	real positive value of the new device level. For the rod-type devices this value must correspond to the new rod insertion level (see Section 3.4.3). For the lzc-type devices this value must correspond to the new water filling level (see Section 3.6.2). In any case, the new level value must be: $0.0 \leq value \leq 1.0$
SPEED	keyword used to specify a new value for <i>speed</i> .
speed	real positive value of the device speed. For the rod-type devices this value must correspond to the speed of rod movement (insertion or extraction), given in cm/s. For the lzc-type devices this value must correspond to the water filling rate, given in m^3/s . The value of <i>speed</i> is required only for the reactor regulating purpose.
TIME	keyword used to specify a new value for <i>time</i> .
time	real value of time either for the rod insertion (or extraction) or for the liquid controller filling, given in sec. The value of <i>time</i> is required only for the reactor regulating purpose.
END	keyword used to indicate the end of input of the new parameters for the current device or group of devices.
3.8 The MOVDEV: module

The MOVDEV: module can be used for the transient simulations and reactor control studies, which are related to the time-dependent rod-devices displacement in the reactor core. The rods can be inserted into or extracted from the reactor core, at constant or at variable speed of movement. The rod positions are recomputed at every given time step of movement. The new rod positions can be computed in several ways, based on either: current time increment and movement speed; relative change in rod positions; or current rod insertion level. The MOVDEV: module allows the rod-devices to be displaced individually or simultaneously in groups.

The MOVDEV: module specification is:

Table 21: Structure MOVDEV:

DEVICE := MOVDEV: DEVICE :: (descrove)

where

DEVICE character*12 name of the DEVICE object that will be modified by the module. The rods positions are updated according to the current time step of movement.

(describing the input data to the MOVDEV: module.

3.8.1 Input data to the MOVDEV: module

It is possible to move several individual rods and/or several groups of rods simultaneously. A user must be aware that a particular device will not be displaced more than once during the same time step. Note that the input order of data to the module must be respected.

Table 22: Structure (descmove)

```
[ EDIT iprint ]
DELT delt
[[ { ROD id | GROUP igrp }
{ INSR | EXTR }
{ LEVEL value | DELH delh | SPEED speed } ]]
.
```

where

EDIT keyword used to set *iprint*.

iprint integer index used to control the printing on screen: = 0 for no print; = 1 for minimum printing (default value); larger values produce increasing amounts of output.

rod has a [: module
rod has a [: module
rod has a [: module
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erted into
acted from
value will on level is nal (<i>value</i> rtion level
the period ment axis,
The rod he devices

3.9 The NEWMAC: module

The NEWMAC: module is used to create a complete MACROLIB with respect to the devices parameters. The resulting MACROLIB will contain the exact properties for every material region, over the whole mesh-splitted reactor geometry. The material properties of each region are recomputed with respect to the actual position of each rod-type and if present lzc-type device. The computing algorithm is based on the determination of the volumic fraction occupied by each device; the incremental cross sections are then adjusted, accordingly. Note that the NEWMAC: module must be executed each time the devices positions are modified from the previously computed ones.

The NEWMAC: module specification is:

Table 23: Structure NEWMAC:

MACRO3 MATEX := NEWMAC: MATEX MACRO2 DEVICE :: [EDIT iprint] [XFAC xfac];

MACRO3	character*12 name of the MACROLIB to be created by the module. It will contain the updated properties of each material region with respect to the current position of each device.
MATEX	character*12 name of the MATEX object, containing the complete reactor material index including devices. <i>MATEX</i> must be specified in the modification mode; it will store the updated h-factors, computed per each fuel region with respect to the devices positions.
MACRO2	<pre>character*12 name of the read-only extended MACROLIB, previously created by the MACINI: module.</pre>
DEVICE	$\verb+character*12 name of the read-only \ \verb+Device object containing the devices information and parameters.$
EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing; larger values produce increasing amounts of output. The default value is $iprint = 1$.
XFAC	keyword used to specify the number of cells on which incremental cross sections were computed in the supercell code.
xfac	corrective factor for delta sigmas (real number). For DRAGON code, $xfac$ is generally set to 2.0 and, for MULTICELL code, set to 1.0. The default value is 2.0.

3.10 The FLPOW: module

The FLPOW: module is used to compute and print the flux and power distributions over the reactor core. It also computes and prints some additional information, for example: the fluxes ratios with respect to the thermal energy-group fluxes; the mean power density; the power- and flux-form factors; etc. The computed fluxes and powers are printed either on files or on the screen. Note that the calculation using the FLPOW: module can be performed once the numerical solution has been previously established using the FLUD: or KINSOL: module.

According to the user-selected module specification, the average fluxes and powers can be computed per each fuel region over the fuel lattice and/or per each material region over the whole reactor geometry. In either case, all fluxes are normalized to the given total reactor power corresponding to the reactor nominal conditions at core equilibrium. If the reactor is perturbed from its initial state, then a new total reactor power can be recomputed and, accordingly, the flux and power distributions will be updated using the previously computed normalization factor.

The FLPOW: module will create a new POWER object that will store the information related to the reactor fluxes and powers (see Section 7.5). In addition, the POWER object will store several parameters that can be used as power and criticity constraints for the optimization and fuel management purposes, namely: the maximum channel and bundle powers; the channel and bundle power-form factors; the effective multiplication factor (recovered from the FLUX or KINET data structure).

The FLPOW: module specifications are:

Table 24: Structure FLPOW:

```
{
   POWER [ NRMFLUX ] [ FMAP ]
      := FLPOW: [ POWOLD ] FMAP { FLUX | KINET } TRACK MATEX
      :: (descflpow)
   POWER := FLPOW: [ POWOLD ] { FLUX | KINET } TRACK MACRO
      :: (descflpow)
}
```

POWER	character*12 name of the POWER object that will be created by the module. It will contain the information related to the reactor fluxes and powers.
NRMFLUX	character*12 name of the FLUX object, in creation mode. According to the chosen option, this object contains either the fluxes normalized to the given total reactor power or the fluxes per bundle. Is it useful if you want to compute the detectors readings with the DETECT: module.
POWOLD	character*12 name of the read-only POWER object. It must contain the previously computed flux normalization factor, which corresponds to the reactor nominal or equilibrium conditions.
FMAP	character*12 name of the FMAP object containing the fuel lattice specification. When $FMAP$ is specified on the RHS, the fluxes and powers calculations are performed over

	the fuel lattice as well as over the whole reactor geometry. If <i>FMAP</i> is specified on the LHS, its records 'BUND-PW' and 'FLUX-AV' will be set according to the information present in <i>POWER</i> .
FLUX	character*12 name of the FLUX object, previously created by the FLUD: module. The numerical flux solution contained in <i>FLUX</i> is recovered and all flux are normalized to the given total reactor power.
KINET	<code>character*12</code> name of the KINET object, previously created by the <code>KINSOL:</code> module. The numerical flux solution contained in $KINET$ is recovered.
TRACK	<code>character*12</code> name of the TRACK object, created by the <code>TRIVAT</code> : module. The information stored in $TRACK$ is recovered and used for the average flux calculation.
MATEX	character*12 name of the MATEX object, containing the reactor material index and the h-factors that will be recovered and used for the power calculation.
MACRO	$\tt character*12$ name of the MACROLIB object, containing the h-factors that will be recovered and used for the power calculation.
(descflpow)	structure describing the input data to the \texttt{FLPOW} : module .

3.10.1 Input data to the FLPOW: module

Note that the fuel-lattice power distribution can be printed only on the screen.

Table 25: Structure (descfipow)

```
[ EDIT iprint ]
[ { PTOT power | P-NEW } ]
[ FSTH fsth ] [ INIT ]
[ { NORM | BUND } ]
[ PRINT { MAP | DISTR [ FLUX ] [ RATIO ] [ POWER ] | ALL } ]
;
```

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum editing (default value); $= 2$ only channel powers in radial plane are printed; $= 3$ only bundle powers per each radial plane are printed; $= 10$ only bundle powers per each channel are printed. Any combination of the values 2, 3 and 10 is possible, for example 5 = 2+3. Note that any other value of <i>iprint</i> behaves as the first lower possible value, for example 7 gives the same output as 5. Moreover channel and bundle powers can be printed only if the <i>FMAP</i> object was provided in the calling specification.
PTOT	keyword used to specify the input of <i>power</i> . By default, a power is recovered from the $KINET$ object.

power	real total reactor power, given in MW. This value must correspond to the reactor nominal conditions.
FSTH	keyword to specify the thermal to fission power ratio.
fsth	thermal to fission power ratio. By default this value is not used, and the total power is the one given after the PTOT keyword.
INIT	keyword used to save the actual power distribution in the BUND-PW-INI record of the fuel map object $FMAP$. It is used by the AFM: module to apply power feedback during a fast transient using the initial power distribution instead of the actual power.
P-NEW	keyword used to indicate that a new total reactor power is to be recomputed, based on the previously calculated flux normalization factor. The flux and power distributions over the reactor core are updated, accordingly. Note that this option is valid only if a read-only <i>POWOLD</i> object is provided.
PRINT	keyword used to indicate the printing on files. Note that all produced files will have the same extension ".res".
MAP	keyword used to specify the printing of the average fluxes and flux ratios per fuel bundle. The normalized bundle fluxes are computed and printed for each reactor channel and per each energy group. The flux ratios are computed with respect to the thermal energy-group fluxes; they are printed on the same file.
DISTR	keyword used to indicate the printing of data computed over the whole reactor geom- etry.
FLUX	keyword used to specify the printing of flux distribution. The normalized fluxes are printed in separated files, one file per energy group; the number of produced files will then equal to the total number of energy groups. The flux values are printed for each mesh-splitted volume, in X, Y and Z planes; the virtual regions will have the fluxes values set to 0.
RATIO	keyword used to specify the printing of flux-ratio distribution. The flux ratios are com- puted with respect to the thermal energy-group fluxes per each mesh-splitted volume. They are printed in separated files; the number of produced files will equal to the total number of energy groups less one.
POWER	keyword used to specify the printing of power distribution. The power values are printed for each mesh-splitted volume, in X, Y, and Z planes; the non-fuel regions will have the power values set to 0.
ALL	keyword used to indicate the printing of all available information, i.e. without particular selection of data.
NORM	keyword to specify that the output flux object will contain a value per mesh-splitted element, normalized to the given power, as required by the DETECT: module. This is the default option.
BUND	keyword to specify that the output flux object will contain a value per bundle, nor- malized to the given power.

3.11 The TAVG: module

The TAVG: module is used to compute the burnup integration limits for each fuel bundle, the axial power-shape over the fuel lattice, the channel refuelling rates and the reactor core-average exit burnup. All calculations using the TAVG: module are performed according to the time-average model for the equilibrium-core conditions. The computing algorithm is based on bidirectional refuelling schemes of channels and average exit burnups specified over the fuel lattice, which should be recorded in the fuel map using the RESINI: module.

Note that the complete time-average calculation is a complex and iterative procedure, requiring of several full-core calculations (external iterations) to be performed. The main steps of the time-average calculation using DONJON are briefly described at the end of this section. The TAVG: module can also be used to compute the instantaneous fuel burnups according to the channel patterned-age-model, for the fuel management and optimization purposes.

The TAVG: module specification is:

Table 26: Structure TAVG:

FMAP := TAVG: FMAP POWER :: (desctavg)

where

FMAP	character*12 name of a FMAP object, that will be updated by the TAVG: module. The $FMAP$ object must contain the average exit burnups and refuelling schemes of channels.
POWER	character*12 name of a POWER object containing the channel and bundle powers, previously computed by the FLPOW: module. The channel and bundle powers are used by the TAVG: module to compute the normalized axial power-shape over each channel.
(desctavg $)$	structure describing the input data to the TAVG: module.

3.11.1 Input data to the TAVG: module

Note that the input order must be respected.

Table 27: Structure (desctavg)

```
[ EDIT iprint ]
[ AX-SHAPE [ RELAX relval ] ]
[ B-EXIT ]
;
```

where	
EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); $= 2$ only the burnup limits over each channel are printed; $= 3$ only the axial power-shape values over each channel are printed; $= 4$ only the channel refuelling rates are printed; for larger values of <i>iprint</i> everything will be printed.
AX-SHAPE	keyword used to indicate the calculation of the new axial power-shape and correspond- ing burnups limits over each reactor channel.
RELAX	keyword used to set the relaxation parameter <i>relval</i> .
relval	real value of the relaxation parameter, generally used to control the axial-shape conver- gence over the external time-average iterations. The optimal value, which corresponds to the minimal total number of such iterations, can be found by performing several runs at different <i>relval</i> . The default value of the relaxation parameter is set to 0.5
B-EXIT	keyword used to indicate the calculation of the core-average exit burnup and the chan- nel refuelling rates.

3.11.2 Time-average calculation using DONJON

When the average exit burnups are provided for each channel, the exact burnup integration limits for each fuel bundle are unknown and need to be determined. The burnups integration limits are function of the normalized axial power-shape, which in turn depends on the flux solution over the fuel lattice. Moreover, the flux solution depends on the fuel-map macrolib (i.e. fuel properties), which in turn depends on the burnups integration limits for each fuel bundle. Consequently, the time-average calculation is an iterative procedure that consists to repeat all the steps required for the axial power-shape computation. This repetition is to be made until the relative error between the two (successives) axial power-shape calculations becomes as small as required for the precision.

The axial power-shape computing scheme is composed of several steps, each step is performed using an appropriate DONJON or TRIVAC module:

- 1. An initial axial power-shape is set as a flat distribution over the fuel lattice and the first burnup integration limits are calculated approximately, using the **RESINI**: module.
- 2. A time-average integration is performed and a new fuel-map MACROLIB is created, using either NCR:, CRE: or AFM: module.
- 3. An extended MACROLIB over the whole reactor geometry is created, using the MACINI: module.
- 4. If the devices are inserted into the reactor core, then the previously created MACROLIB is to be updated for the devices properties using the NEWMAC: module.
- 5. The complete MACROLIB is subsequently used by the TRIVAA: module in order to create a matrix SYSTEM.
- 6. The full-core numerical solution (i.e. fluxes and effective multiplication factor) is computed, using the FLUD: module.
- 7. The channel and bundle powers are next calculated, using the FLPOW: module.
- 8. Finally, the new axial power-shape and burnup limits are computed, using the TAVG: module.

Note that the steps from 2 to 8 are to be repeated until the required precision for the axial power-shape convergence is satisfied.

3.12 The TINST: module

The TINST: module is used to compute the instantaneous burnup for each fuel bundle. You can also use TINST: to refuel your reactor, according to a refueling-scheme. The scheme can be either specified with RESINI:, or directly in TINST:.

The **TINST**: module specification is:

Table 28: Structure TINST:

```
{ FMAP := TINST: FMAP [ POWER ] |
MICLIB3 FMAP := TINST: FMAP MICLIB2 MICLIB }
:: (desctinst)
```

where

FMAP	<code>character*12</code> name of a <code>FMAP</code> object, that will be updated by the <code>TINST:</code> module. The $FMAP$ object must contain the instantaneous burnups for each fuel bundle and the weight of each fuel mixture.
POWER	character*12 name of a POWER object containing the channel and bundle powers, previously computed by the FLPOW: module. The channel and bundle powers are used by the TINST: module to compute the new burn-up of each bundle. If bundle-powers are previously specified with the module RESINI:, you can refuel your core without a <i>POWER</i> object.
MICLIB3	character*12 name of a LIBRARY object, that will be created by the TINST: module. This MICROLIB contains the fuel properties after refueling when keyword MICRO is used in (desctinst).
MICLIB2	<code>character*12</code> name of a LIBRARY object, that will be read by the <code>TINST:</code> module. This must be a fuel-map $LIBRARY$ created either created by the NCR: or the EVO: module.
MICLIB	character*12 name of a LIBRARY object, that will be read by the TINST: module. This MICROLIB contains the new fuel properties, that should be used for the refueling.
$({ m desctinst})$	structure describing the input data to the TINST : module.

3.12.1 Input data to the <code>TINST:</code> module

Note that the input order must be respected.

[EDIT iprint]
[BURN-STEP rburn TIME rtime { DAY HOUR MINUTE SECOND }]
[[REFUEL [MICRO] CHAN NAMCHA nsh]]
[[NEWFUEL CHAN NAMCHA nsh { SOME (imix(i), i=1,ABS(nsh)) ALL imix]]
[[SHUFF CHAN NMCHA1 TO { NMCHA2 POOL }]]
;

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); $= 2$ only the burnup limits over each channel are printed; $= 3$ only the axial power-shape values over each channel are printed; $= 4$ only the channel refueling rates are printed; for larger values of <i>iprint</i> everything will be printed.
BURN-STEP	keyword used to indicate an increase of core average burn-up.
rburn	keyword used to indicate in MWd/t the average increase of burn-up in the core.
TIME	keyword used to indicate the time of combustion at the power specified in $POW\!ER$ structure.
rtime	keyword used to set the time combustion value in DAY or HOUR or MINUTE or SECOND.
DAY	keyword used to specify that <i>rtime</i> is a number of days.
HOUR	keyword used to specify that <i>rtime</i> is a number of hours.
MINUTE	keyword used to specify that <i>rtime</i> is a number of minutes.
SECOND	keyword used to specify that <i>rtime</i> is a number of seconds.
REFUEL	key word to specify a channel refueling.
MICRO	keyword used to perform a microscopic refueling. In this case, three libraries have to be provided when TINST : is called.
CHAN	key word to specify the refueled channel information.
NAMCHA	channel name as defined by NXNAME and NYNAME. NAMCHA is a character ^{*4} variable, constructed as $WRITE(NAMCHA, '(A1, A3)')NYNAME(1:1), NXNAME(1:2).$
nsh	refueling scheme. The absolute value of nsh is the number of fuel bundles inserted in the channel NAMCHA. The sign of nsh define the refueling direction: positive direction is from the first to the nk -th bundle and negative is from the nk -th to the first bundle.
NEWFUEL	key word to specify that a channel will be refueled with a different type of fuel.
SOME	key word to specify that the <i>nsh</i> values of fuel types can be different.
<i>imix</i> (i)	index number of a fuel type with respect to the values defined in module NCR:, CRE: or AFM:.

ALL	key word to specify that the <i>nsh</i> values of fuel types will be identical to <i>imix</i> .
SHUFF	key word to specify that a specified channel will move into an other one or discharge into the pool.
CHAN	key word to specify the moved channel name.
NMCHA1	channel name as defined by $N\!XN\!AM\!E$ and $NY\!N\!AM\!E.$ It is constructed as $N\!AM\!C\!H\!A.$
ТО	key word to specify the bundle destination.
NMCHA2	channel name as defined by $N\!XN\!AM\!E$ and $NY\!N\!AM\!E.$ It is constructed as $N\!AM\!C\!H\!A.$
POOL	key word to specify that the channel referenced by <i>NMCHA1</i> is discharged into the pool.

3.13 The SIM: module

The SIM: module can perform a sequence of operations related to fuel management in PWRs:

- simulate a refuelling and shuffling scheme and update the burnup distribution accordingly. The refuelling scheme is specified directly in SIM:.
- increase the burnup using the power available in the *POWER* object and compute the final instantaneous burnup of each assembly subdivision
- modify a local parameter such as the Boron concentration in the coolant.

The SIM: module specification is:

Table 30: Structure SIM:

FMAP := SIM: FMAP [POWER]
:: (descsim)

where

FMAP	character*12 name of a FMAP object, that will be updated by the SIM: module. The $FMAP$ object must contain the instantaneous burnups for each assembly subdivision, a basic naval-coordinate assembly layout and the weight of each assembly subdivision.
POWER	character*12 name of a POWER object containing the channel and powers of the assembly subdivisions, previously computed by the FLPOW: module. The channel and powers of the assembly subdivisions are used by the SIM: module to compute the new burn-up of each assembly subdivision. If the powers of the assembly subdivisions are previously specified with the module RESINI:, you can burn your core without a <i>POWER</i> object.
(descsim $)$	structure describing the input data to the SIM: module.

3.13.1 Input data to the SIM: module

Note that the input order must be respected.

Table 31: Structure (descsim)

```
 \begin{bmatrix} \text{EDIT } iprint \end{bmatrix} \\ \begin{bmatrix} \text{CYCLE } hcnew [ FROM hcold [ BURN { indcycle | burncycle } ] ] \\ & [ { MAP } (hx(i), i=1, lx ) \\ & (hy(j), (hcase(i,j), i=1, lx ), j=1, ly ) | \\ & \text{QMAP } (hx(i), i=lx/2+1, lx ) \\ & (hy(j), (hcase(i,j), i=lx/2+1, lx ), j=ly/2+1, ly ) } ] \\ \end{bmatrix}
```

continued on next page

Structure (descsim)

[SPEC [[[[asmb1]] { SET AVGB avburn | SET FUEL ifuel | FROM hcold2 AT asmb2 [BURN { indcycle | burncycle }] }]]] [DIST-AX [[[[asmb1]] { SET (axn(i), i=1,nb) | FROM hcold2 AT asmb2 [BURN { indcycle | burncycle }] }]]] [BURN-STEP rburn | TIME rtime { DAY | HOUR | MINUTE | SECOND }] ENDCYCLE] [[COMPARE hc1 [BURN { indcycle1 | burncycle1 }] hc2 [BURN { indcycle2 | burncycle2 }] { DIST-BURN >> epsburn << | DIST-POWR >> epspowr << }]] [[SET-PARAM PNAME pvalue]] ;

where

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing (default value); for larger values of <i>iprint</i> everything will be printed.
CYCLE	keyword defining operations based on the actual fuel cycle.
hcnew	character*12 identification name of the specific fuel cycle.
FROM	keyword defining the previous fuel cycle in case that some information needs to be transmitted to the actual fuel cycle.
hcold	character*12 identification name of the previous fuel cycle.
BURN	keyword defining the burnup at which the assembly is recycled in the previous fuel cycle. By default, the last burnup step is used.
indcycle	integer index of the burnup step in the previous fuel cycle.
burncycle	real value of the burnup in the previous fuel cycle.
MAP	keyword defining the assembly layout in naval-coordinate positions in the actual fuel cycle. Here, lx and ly values are those defined in the fuel map (see Section 3.1.2).
QMAP	keyword defining the assembly layout in naval-coordinate positions using quarter-core symmetry conditions. Here, the lower-right quarter is defined. The full map is recon- structed through rotations around the center.
hx	ordered list of available character*1 prefixes for the X-oriented naval-coordinate positions. Values are generally chosen between A and T.
hy	ordered list of available character*2 suffixes for the Y-oriented naval-coordinate positions. Values are generally chosen between 01 and 17 .
hcase	character*4 identification value for the (i,j) position. Accepted values are:
	• , - or - - for a position outside the core,
	• NEW for a new assembly (at zero burnup) selected according to the fuel map

specified in Sect. 3.1,

	• SPC for an assembly described later in the dataset using a SPEC specification,
	• or a naval-coordinate position referring to the position of an assembly in cycle <i>hcold</i> that is recycled in the current cycle.
SPEC	keyword defining specifications related to all assemblies previously identified with the SPC keyword. If QMAP keyword has been used with SPC values, the 4 equivalent assemblies must be specified (i.e. not only the lower-right quarter assembly).
asmb1	character*3 naval-coordinate position of an assembly identified with a SPC keyword. Up to 30 coordinates can be set aside if many assemblies have the same specification.
SET	keyword indicating that a user-defined value will be assigned to the assembly.
AVGB	keyword indicating that an averaged burnup will be assigned to the assembly.
avburn	real value of the average burnup in MWd/t.
FUEL	keyword indicating that a new fuel assembly will be used.
fuel	integer index of the fuel type corresponding to the new fuel assembly. Fuel type indices are those used in the RESINI: PLANE descriptions of Sect. 3.1.
FROM	keyword indicating that a value recovered from another assembly will be assigned to the current assembly.
hcold2	character*12 identification name of a previous fuel cycle.
AT	keyword indicating that the naval-coordinate position of the other assembly will be given.
asmb2	$\verb+character*3 naval-coordinate position of the other assembly in cycle $hcold2$.$
DIST-AX	keyword used to impose an axial burnup distribution to the assembly. The burnup distribution is recovered from an existing assembly or is set to user-suppled values.
axn	real values of the axial burnup distribution.
BURN-STEP	keyword used to indicate an increase of core average burn-up.
rburn	keyword used to indicate in $\rm MWd/t$ the average increase of burn-up in the core.
TIME	keyword used to indicate the time of combustion at the power specified in $POW\!ER$ structure.
rtime	keyword used to set the time combustion value in \mathtt{DAY} or \mathtt{HOUR} or \mathtt{MINUTE} or $\mathtt{SECOND}.$
DAY	keyword used to specify that <i>rtime</i> is a number of days.
HOUR	keyword used to specify that <i>rtime</i> is a number of hours.
MINUTE	keyword used to specify that <i>rtime</i> is a number of minutes.
SECOND	keyword used to specify that <i>rtime</i> is a number of seconds.
ENDCYCLE	keyword indicating the end of data specific to the actual fuel cycle.
COMPARE	keyword for obtaining a CLE-2000 variable that is a measure of the discrepancy between two cycles.
hc1	character*12 identification name of the first fuel cycle to compare.
hc2	character*12 identification name of the second fuel cycle to compare.

DIST-BURN	keyword used to recover the discrepancy on burnup distribution in a CLE-2000 variable.
epsburn	character*12 CLE-2000 variable name in which the extracted burnup discrepancy (expressed in MW-day/tonne) will be placed.
DIST-POWR	keyword used to recover the relative error on power distribution in a CLE-2000 variable.
epspowr	$\tt character*12$ CLE-2000 variable name in which the extracted power relative error will be placed.
SET-PARAM	keyword used to indicate the input (or modification) of the actual values for a parameter specified using its $PNAME$.
PNAME	keyword used to specify <i>PNAME</i> .
PNAME	character*12 name of a parameter.
pvalue	single real value containing the actual parameter's values. Note that this value will not be checked for consistency by the module. It is the user responsibility to provide the valid parameter's value which should be consistent with those recorded in the multicompo or Saphyb database.

3.14 The XENON: module

The XENON: module is used to correct the Xenon distribution coming from an interpolation calculation. This module computes the new densities according to the bundle flux, and the equation providing the balance concentration of Xenon-135:

$$N_{X_{eq}} = \frac{(Y_I + Y_X)\Sigma_f \phi}{\lambda_X + \sigma_X \phi} \tag{3.1}$$

where

- Y_I is the fission yield of I135
- Y_X is the fission yield of Xe135
- σ_X is the capture cross section of Xe135
- λ_X is the decay constant of Xe135
- Σ_f is the total fission cross section
- ϕ is the bundle flux

The XENON: module specification is:

Table 32: Structure XENON:

MICROLIB := XENON: MICROLIB [POWER]
:: (descrenon)

where

MICROLIB	character*12 name of a LIBRARY object, that will be updated by the XENON: module. The Xenon should be extracted in this library for the use of this module.
POWER	character*12 name of a POWER object containing the bundle fluxes, previously computed by the FLPOW: module. The fluxes should be normalized to the reactor power.
(descxenon)	structure describing the input data to the XENON: module.

3.14.1 Input data to the XENON: module

Note that the input order must be respected.

Table 33: Structure (descxenon)

Structure (descxenon)

[INIT];

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen.
INIT	keyword used to indicate the initialization of the library for a recursive calculation using the $XENON$: module. The Xenon concentration is set to zero for all the bundles.

3.15 The DETECT: module

The DETECT: module is used to compute the mean flux at each detector site and the response of each detector.

The ${\tt DETECT}\colon$ module specifications are:

Table 34: Structure DETECT:

DETEC := DETECT: DETEC FLUX TRACK GEOM :: (descdetect) ;

where

DETEC	$\tt character*12$ name of the <code>DETECT</code> containing the detector positions and responses.
FLUX	character*12 name of the FLUX containing the flux solution computed by the FLUD: or FLPOW: modules. To obtain a correct result, the best is to use a normalized flux, coming from the FLPOW: module. In this case, the fluxes are normalized to the reactor power.
TRACK	character*12 name of the TRACK containing the TRIVAC tracking.
GEOM	<pre>character*12 name of the GEOMETRY containing the mesh-splitting geometry created by the USPLIT: or GEO: modules.</pre>
$(ext{descdetect})$	structure containing the data to module DETECT:.

3.15.1 Input data to the DETECT: module

Note that the fuel-lattice power distribution can be printed only on the screen.

Table 35: Structure (descdetect)

[EDIT *iprt*] TIME *dt* REF *kc* [NORM *vnorm*] [SIMEX { SPLINE | PARAB }] ;

where

EDIT key word used to set *iprt*.

iprt index used to control the printing in module DETECT:. =0 for no print; =1 for minimum printing(default value); =4 for printing each detector name; =5 for finite element numbers and total number of finite elements for each detector.

TIME	key word used to set dt .
dt	time step between two calls to the DETECT: module.
REF	key word used to set kc .
kc	index used to control the type of calculation, $=0$ for reference calculation; $=1$ normal calculation. The reference responses are used to obtain detector current responses in full power fractions.
NORM	key word used to set <i>vnorm</i> .
vnorm	value used to normalized responses of all the detectors present in DETECT.
SIMEX	key word used to specify that a polynomial interpolation of detector fluxes according to HQSIMEX method. This interpolation will be applied only for vanadium detectors, under $NAMTYP$ of value VANAD_REGUL.
SPLINE	key word to specify that the flux at detector site will be computed with a spline method.
PARAB	key word to specify that the flux at detector site will be computed with a parabolic method.

3.16 The CVR: module

The CVR: module is used to update the fuel-type index and the coolant densities throughout the reactor core as required for the voiding simulations. A particular core-voiding pattern is either selected from the several pre-defined patterns or directly defined by the user in an arbitrary fashion. In the last case, the user may specify the individual voided channels by indicating their identification names. The CVR: module will create a new (perturbed) FMAP object, in which the fuel-type mixtures indices are modified according to the specified core-voiding pattern. The information with respect to the relative coolant densities is required only for the subsequent interpolation of fuel properties using the NCR: module. These data will also be reordered by the CVR: module according to the specified voiding pattern and recorded as local parameter in the perturbed fuel-map object (see Section 3.1.2).

The CVR: module specification is:

Table 36: Structure CVR:

FMAPV := CVR: FMAP :: (descrcvr)	

where

FMAP	<pre>character*12 name of a read-only FMAP object, created in the RESINI: module. This object must contain the non-perturbed fuel-cell properties.</pre>
FMAPV	character*12 name of a new FMAP object, that will contain the modified fuel-type indices and reordered coolant densities according to the specified core-voiding pattern.
$({ m descrcvr})$	structure describing the input data to the CVR: module.

3.16.1 Input data to the CVR: module

Note that the input order must be respected.

Table 37: St	ucture (descrcvr)	
--------------	-------------------	--

```
\begin{array}{l} \mbox{EDIT iprint} \\ (\mbox{ MIX-FUEL } mixF(i) \mbox{ MIX-VOID } mixV(i) \ , i = 1, \ nfuel \ ) \\ [\mbox{ DENS-COOL } PNAME \ \mbox{ SET } dcoolV \ ] \\ \mbox{VOID-PATTERN } \left\{ \mbox{ FULL } | \mbox{ HALF } | \mbox{ QUARTER } | \mbox{ CHECKER-1/2 } | \mbox{ CHECKER-1/4 } | \\ \mbox{ CHAN-VOID } nvoid \ ( \ YNAME(i) \ XNAME(i) \ , i = 1, \ nvoid \ ) \end{array} \right\} ;
```

where

EDIT keyword used to set *iprint*.

iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing; $= 2$ modified fuel indices and coolant densities are printed per bundle over each channel; $= 3$ modified fuel indices are printed per each radial plane; for larger values of <i>iprint</i> everything will be printed.	
MIX-FUEL	keyword used to specify $mixF$.	
mixF	integer fuel-type mixture number of the non-perturbed fuel cell. This number must be specified for each fuel type as been recorded in the MATEX object (see Section 3.2.1).	
MIX-VOID	keyword used to specify $mixV$.	
mixV	integer new mixture number assigned to the voided fuel cell. Note that this number must be specified for each fuel type and it must be different from any other reactor material mixtures.	
DENS-COOL	keyword used to specify $PNAME$. This information is required only for the interpolation of fuel properties using the NCR: module.	
PNAME	character*12 user-defined identification name of local parameter associated with the relative coolant density. The recommended name is D-COOL. This parameter name and the unperturbed densities values should be previously recorded in the $FMAP$ object (see Section 3.1.2). The same $PNAME$ will be set for the coolant density in the perturbed $FMAPV$, but the actual values of coolant densities throughout the core will be reordered by the CVR: module according to the specified voiding pattern.	
SET	keyword used to specify the value $dcoolV$.	
dcoolV	real value of the relative coolant density (with respect to the nominal or unperturbed conditions) associated with the voided reactor channels. In general, this value equals to 0.0 for the complete voiding of a channel and to 1.0 for an unperturbed channel. Intermediate values of $dcoolV$ will then correspond to the partially voided channels. It is supposed that all voided channels will have the same $dcoolV$ value.	
VOID-PATTERN	keyword used to specify the core voiding pattern, which will be used for a particular voiding simulation.	
FULL	keyword used to specify the full-core voiding pattern. According to this pattern, the fuel mixtures will be modified for all reactor channels.	
HALF	keyword used to specify the half-core voiding pattern. According to this pattern, the fuel mixtures will be modified only for the upper-half of reactor channels.	
QUARTER	keyword used to specify the quarter-core voiding pattern. According to this pattern, the fuel mixtures will be modified only for the upper-left quarter of reactor channels.	
CHECKER	keyword used to specify the checkerboard-full voiding pattern. According to this pattern, the fuel mixtures will be modified for all reactor channels in which the direction of coolant flow is positive.	
CHECKER-1/2	keyword used to specify the checkerboard-half voiding pattern. According to this pattern, the fuel mixtures will be modified only for the upper-half of reactor channels in which the direction of coolant flow is positive.	
CHECKER-1/4	keyword used to specify the checkerboard-quarter voiding pattern. According to this pattern, the fuel mixtures will be modified only for the upper-left quarter of reactor channels in which the direction of coolant flow is positive.	

CHAN-VOID	keyword used to specify the user-defined voiding pattern. Each voided channel must be identified by its $YNAME$ name followed by its $XNAME$.
nvoid	integer total number of the voided channels. This number must be greater than 0 and less than (or equal to) the total number of reactor channels.
YNAME	character*2 vertical name of the voided channel. A vertical channel name is identified by the channel row using an alphabetical letter ('A', 'B', 'C', etc). The total number of the specified Y-names must equal to the total number of voided channels <i>nvoid</i> .
XNAME	character*2 horizontal name of the voided channel. A horizontal channel name is identified by the channel column using a numerical character ('1', '2', '3', etc.). The total number of the specified X-names must equal to the total number of voided channels <i>nvoid</i> .

3.17 The HST: module

The HST: module has been designed to manage a full reactor execution in DONJON using explicit DRAGON calculations for each cell.^[18] This module saves in an HISTORY data structure the information available in BURNUP data structures generated by DRAGON. It can also read MAP data structure generated by DONJON to prepare the HISTORY data structure for a new series of cell calculations in DRAGON. The HISTORY data structure can also be used to update the MAP data structure. Finally, the module HST: can be used to create an initial BURNUP data structure that can be used to evolve the cell another time step in DRAGON.

The HST: module can be used to create or update an HISTORY data structure. The possible options are:

Table 38: Updating an HISTORY structure using a MAP structure

```
HISTORY := HST: [HISTORY] MAP [:: [(hstdim)] [GET (hstpar)]]
```

Table 39: Updating an HISTORY structure using a BURNUP structure

```
HISTORY := HST: [ HISTORY ] [ BURNUP ] [ :: [ (hstdim) ]
[ GET (hstpar) ] [ CELLID icha ibun [ idfuel ] [ GET (hstpar) ] ] ]
```

It can also be used to create a BURNUP data structure from the information available on an HISTORY data structure:

Table 40: Updating a BURNUP structure using an HISTORY structure

```
BURNUP := HST: HISTORY [ :: [ (hstdim) ]
      [ PUT (hstpar) ]
      CELLID icha ibun
      [ PUT { BREFL (hstbrn) (hstpar) AREFL (hstbrn) (hstpar) | [ AREFL ] (hstbrn) (hstpar)
}]]
```

It can also be used to update a MAP data structure from the information available on an HISTORY data structure:

Table 41: Updating an HISTORY structure using a MAP structure

MAP := HST: MAP HISTORY

HISTORY	character*12 name of an HISTORY data structure.
BURNUP	character*12 name of a BURNUP data structure.
MAP	character*12 name of a MAP data structure.
(hstdim)	structure containing the dimensions for the HISTORY data structure.
CELLID	keyword to identify the cell for which history information is to be processed.
icha	channel number for which history information is to be processed.
ibun	bundle number for which history information is to be processed.
idfuel	fuel type number associated with this cell. One can associate to each fuel cell a different fuel type. By default a single fuel type is defined and it fills every fuel cell. Only the initial properties of each fuel type are saved. These properties are used for refueling.
GET	keyword to specify that the values of the parameters selected in (brnpar) will be read from the input stream or CLE-2000 local variables and stored on the HISTORY data structure.
PUT	keyword to specify that the values of the parameters selected in (brnpar) will be read from the HISTORY data structure and transferred to local CLE-2000 variables.
BREFL	to specify that the information to extract from the HISTORY data structure is related to the properties of the cell before refueling takes place.
AREFL	to specify that the information to extract from the HISTORY data base is related to the properties of the cell after refueling took place.
$({ m hstbrn})$	structure containing the burnup options.
(hstpar)	structure containing the local parameters options.

The (hstdim) input structure is required for general dimensioning purpose. It is generally used only when creating the HISTORY data structure. However, the number of global and local parameters used in a HISTORY data structure can be increased at all time. The number of channels, bundles and the refueling scheme must be defined at the creation of the HISTORY data structure. This information can be provided manually or extracted from a MAP data structure. The general form of the (hstdim) input structure follows:

Table 42: Structure (hstdim)

[EDIT iprint]	
[DIMENSIONS [GLOBAL nglo] [LOCAL nloc] [BUNDLES nbun bunl] [CHANNELS ncha]]

where	
EDIT	keyword used to modify the print level <i>iprint</i> .
iprint	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required.
DIMENSIONS	keyword used to indicate that the general dimensioning of the HISTORY data struc- ture will be modified.

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GLOBAL	keyword used to modify the number of global parameters on the HISTORY data structure.
nglo	the number of global parameters. Note that the history module will use the maximum value between the current $nglob$ and the value, if any, defined on the HISTORY data structure.
LOCAL	keyword used to modify the number of local parameters on the HISTORY data structure.
nloc	the number of local parameters. Note that the history module will use the maximum value between the current $nloc$ and the value, if any, defined on the HISTORY data structure.
BUNBLES	keyword used to specify the number of bundles per channels for the reactor model considered in the HISTORY data structure.
nbun	the number of bundles per channels for the reactor model. Note that if <i>nbun</i> is different from the value already defined on the HISTORY data structure or the MAP data structure, the execution will be aborted.
bunl	bundle length in cm. This information is required to compute initial fuel weight.
CHANNELS	keyword used to specify the number of fuel channels for the reactor model considered in the HISTORY data structure.
ncha	the number of fuel channels for the reactor model. Note that if <i>ncha</i> is different from the value already defined on the HISTORY data structure or the MAP data structure, the execution will be aborted.

The (hstbrn) serves a unique purpose, mainly to extract from the HISTORY file the information required to process a burnup evaluation in DRAGON using the EVO: module. The information must be stored inside CLE-2000 variables. The general form of this output structure is:

Table 43: Structure (hstbrn)

where

BURN keyword to indicate that burnup information follows.

the burnup period (in days) that will be transferred to a real CLE-2000 variable. period

the power density (in kW/kg) that will be transferred to a real CLE-2000 variable. power

The (hstpar) serves two purposes. First, it is used to define the names of the local and global parameters that may be used in our calculations as well as the values of these local parameters. In can also be used to extract from a HISTORY data structure the values of these parameters. The general form of this structure is:

[[NAMPAR valpar]]

where

NAMPAR name of a local or global parameter to process. The parameters specified before the keyword *CELLID* is read will be considered global otherwise they will be considered local.

valpar

real value for the local or global parameter to process. In the case where the GET option is activated, the history module will extract this parameter from the input data stream. In the case where the PUT option is activated, the history module will try to transfer this information into a real CLE-2000 variable.

3.17.1 Example

The history interface between the codes DRAGON and DONJON has been written as a new module in order to facilitate the access to the GANLIB utilities that manage the required hierarchical data structures. The resulting HST: module can be called both by DRAGON and DONJON.

The reactor model we will consider as an example is a 3–D model with an x = 3, y = 3 and z = 3mesh. Here we will assume that the x - y plane describes fuel channels. The z plane will be associated with the so-called fuel bundles. This choice is somewhat arbitrary, however it is useful if the refueling takes place in a specific direction as in a CANDU reactor. Here, a 2-bundle shift fueling strategy will be considered. To each fresh fuel cell introduced in the core the HST: module will associate a unique cell number between 1 and Nc, the maximum number of cells in the reactor. Most of the information associated with the fresh fuel cells will be extracted from a DRAGON BURNUP file or defined using variable local parameters. Each fresh fuel cell inserted in the core will also be associated with a specific fuel type. Each fuel type is defined as a unique initial fuel composition. The fuel management for the reactor, including burnup and refueling will be performed by the DONJON code. Here the HST: will interact with this code via the MAP data structure. Typically, each cell in the reactor will be burned inside DRAGON using the power provided in the AX-SHAPE record and the depletion time provided in the BURNUP-BEG record stored in the MAP structure. When refueling takes place some of the fuel cells will be extracted, other will be displaced from one position to another and finally new fresh fuel cells inserted. The fresh fuel cells properties will be extracted from the fuel types properties available on the HISTORY data structure.

In a coupled DRAGON/DONJON execution, the HST: module will be called at various points and for various reasons. The first call to HST: can be performed using:

MODULE HST: ; *----* Map data structure for initialization: MAPO * History data structure : History *----SEQ_ASCII MAPO ; XSM_FILE History ; XSM_FILE Reseau ; *----* Reactor parameters

```
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```

```
* ncha = nunber of channels = 9
* nbun = nunber of bundles = 3
* nevo = nunber of evolution = 3
* nglo = nunber of global parameters = 1
* nloc = nunber of local parameters = 2
* bunl = bundle length in cm = 49.53 cm
*----
INTEGER ncha nbun nevo nglo nloc :=
93312;
REAL bunl := 49.53 ;
*----
* Initialize History using MAPO
*----
Reseau := MAPO ;
History := HST: Reseau ::
DIMENSIONS GLOBAL <<nglo>> LOCAL <<nloc>>
BUNDLES <<nbun>> <<bunl>>
CHANNELS <<ncha>> ;
```

Here, the HISTORY data structure will be stored in the XSM file History. One global and two local parameters are considered. No information about the name or the value of the global and local parameters will be available. This initialization procedure stores information only on the main level of the HISTORY data structure if the MAP data structure is not available. In this case the HISTORY is updated using a MAP data structure (in sequential ASCII file MAPO). The number of channels and bundles per channel are stored and compared with the same information in the MAP structure. For each bundle in the MAP, cell type and fuel type directories are constructed. The bundle powers and burnups available in MAP are used to generate the power rates in kW/kg and the depletion time in days required to reach the specified burnups. These values are stored in the HISTORY in the PARAMBURNTAR record. The fuel mass is mandatory for such calculation, thus the fuel weight is recovered from the MAP. If the HISTORY is in modification mode, the fuel weight is computed using the bundle lenght and the initial fuel density. Now, let us assume that a DRAGON calculation was performed for the cell located in bundle j = 1 of channel i = 1. We will also assume that these cells contain a single type of fuel. Here the moderator temperature TMod is a global parameter while the fuel (TComb) and coolant (TCalo) temperatures are considered local parameters. We assume that after the cell flux calculation a BURNUP data structure was generated using the following instructions:

```
*----
* Procedures for cell calculation: CellCalc
*----
PROCEDURE CellCalc ;
*----
* Global parameter: Tmod for moderator temperature
* Local parameters: TComb for fuel temperature
* TCalo for coolant temperature
*----
REAL TMod := 345.66;
REAL TComb TCalo := 941.29 560.66 ;
*----
* Initial burnup options for cell calculation
*----
REAL Power DeltaT := 31.9713 5.0 ;
*----
* Local data structures
```

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```
LINKED_LIST Burnup Edition ;
*----
* Execution control parameters
* icha = channel number = 1
* ibun = bundle number = 1
*----
INTEGER icha ibun := 1 1 ;
*----
* Perform cell calculation
*----
Burnup Edition := CellCalc Burnup ::
<<TComb>> <<TCalo>> <<TMod>>
<<Power>> <<DeltaT>> ;
```

Then, assuming that the history structure HistXSM was created using the options above, we can use

```
* ----
* Update history structure
*----
History := HST: History Burnup ::
GET TMod <<TMod>>
CELLID <<icha>> <<ibun>>
GET TComb <<TComb>> TCalo <<TCalo>> ;
```

where no idfuel is given (see Table 39), thus we have used the default value for idfuel= 1 to store in HISTORY the general information associated with fuel channel 1 and bundle 1. Here, the initial properties associated with fuel type 1 will be generated from the initial isotope densities in the BURNUP. For the CELLID, here icha= 1 and ibun= 1, the burnup information, isotope densities, depletion parameters and initial fuel density are stored in a /celldir/ directory. Moreover the power rate 31.9713 kW/kg and the depletion time 5.0 days are kept in the PARAMBURNTAR record.

A HISTORY data structure that contains the initial cell information can be updated using a MAP data structure:

```
*----
* Map data structure for refueling: MAP1
*----
SEQ_ASCII MAP1 ;
*----
* Refuel
*----
Reseau := MAP1 ;
History := HST: History Reseau ;
```

Here, new burnup power ratings will be stored in the HISTORY data structure reflecting the power distribution in the DONJON calculation. The refueling information available in the MAP structure will also be used to redistribute the fuel in the HISTORY structure at various cell location.

Finally the last option is to recover this information in DRAGON to perform a new series of cell calculations:

```
*----
* Local parameters
* Initial burnup options for cell calculation
* *A is after refueling
* *B is before refueling
*----
```

```
REAL TCombA TCaloA TCombB TCaloB ;
REAL PowerA DeltaTA PowerB DeltaTB ;
Burnup := HST: History ::
PUT TMod >>TMod<<
CELLID <<icha>> <<ibun>>
PUT BREFL BURN >>DeltaTB<< >>PowerB<<
TComb >>TCombB<< TCalo >>TCaloB<<
AREFL BURN >>DeltaTA<< >>PowerA<<
TComb >>TCombA<< TCalo >>TCaloA<< ;</pre>
IF DeltaTB 0.0 > THEN
*----
* Burn before refueling
*----
Burnup Edition := CellCalc Burnup ::
<<TCombB>> <<TCaloB>> <<TMod>>
<<PowerB>> <<DeltaTB>> ;
Edition := DELETE: Edition ;
ENDIF ;
*----
* Burn after refueling
*----
Burnup Edition := CellCalc Burnup ::
<<TCombA>> <<TCaloA>> <<TMod>>
<<PowerA>> <<DeltaTA>> ;
*----
* Update History
*----
History := HST: History Burnup ::
CELLID <<icha>> <<ibun>> ;
```

Note that here, there are two sets of local parameters that can be extracted from the history data structure, namely the before (BREFL) and the after (AREFL) refueling information. In the case of fresh fuel (single fuel description or a refueled bundle) extracting the before information is not required. However, if one uses the general procedure described above to extract the before and after information, one will be able to identify the new fuel bundles as well as the bundle that have not been moved in the core by the fact that $\Delta t = 0$ for burnup before refueling. For bundles that have been displaced in the core during refueling then $\Delta t > 0$.

4 CROSS-SECTION INTERPOLATION MODULES

4.1 The CRE: module

The CRE: module is used for the recovering and interpolation of nuclear properties from one or many COMPO objects, originated from the transport calculations using lattice code DRAGON. A resulting MACROLIB will be created (or updated) by the CRE: module, it will contain the nuclear properties of some selected reactor materials.

Two types of MACROLIB can be constructed using the CRE: module:

- A MACROLIB that will be constructed for the few reactor materials, namely for the devices and/or reflector properties. It can also be created for the few fuel regions defined in the reactor core. This MACROLIB is permitted to be updated for the new properties in the subsequent calls to the CRE: module.
- A fuel-map MACROLIB that will be constructed over the fuel lattice only. This MACROLIB will contain a set of interpolated fuel properties with respect to the burnup distribution over the fuel lattice and according to the interpolation option defined in the FMAP object. The total number of mixtures in the resulting MACROLIB will equal to the total number of fuel bundles.

Note that the CRE: module can be used only with the mono-parameter COMPO objects and the nuclear properties can be interpolated only with respect to the burnup data. In case of the MACROLIB construction from a multi-parameter database, the NCR: module should be used instead. In this case, the interpolation of nuclear properties can be made with respect to global and local parameters, if they were previously specified in the fuel-map (see Section 3.1.2).

The CRE: module specifications are:

Table 45: Structure CRE:

{ MACRO := CRE: [MACRO] [[CPO]] :: (desccre1) | MACFL := CRE: [[CPO]] FMAP :: (desccre2) }

MACRO	character*12 name of the MACROLIB object to be created or updated for the few reactor material properties. Note that if $MACRO$ appears on the RHS, the information previously stored in $MACRO$ is kept.
СРО	$\tt character*12$ name of the COMPO object containing the mono-parameter database from transport calculations.
MACFL	$\tt character*12$ name of the fuel-map MACROLIB that will be created only for the fuel properties over the fuel lattice.
FMAP	$\tt character*12$ name of the <code>FMAP</code> object containing the fuel-map specification and burnup informations.
$(ext{desccre1})$	structure describing the input data to the CRE: module when the FMAP object is not specified.

(desccre2) structure describing the input data to the CRE: module for the fuel-map MACROLIB construction.

4.1.1 Input data for the CRE: module

Table 46: Structure (desccre1)

[EDIT iprint] [NMIX nmix] READ [[COMPO CPO (descdata1)]] :

Table 47: Structure (desccre2)

[EDIT *iprint*] READ [[TABLE CPO (descdata2)]]

where

;

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing of information on screen: $= 0$ for no print; = 1 for minimum printing; larger values will produce increasing amounts of output.
NMIX	keyword used to define the number of material mixtures $nmix$. This data must be given only if $MACRO$ is created and the FMAP object is not specified.
nmix	integer maximum number of reactor material mixtures, as defined in the reactor geometry.
READ	keyword used to read the MACROLIB specification from the input data file.
СОМРО	keyword used to indicate a simple MACROLIB creation, i.e. according to the first calling specification when FMAP object is not specified.
TABLE	keyword used to indicate a fuel-map ${\tt MACROLIB}$ creation, i.e. according to the second calling specification with ${\tt FMAP}$ object specified.
СРО	$\tt character*12$ name of the selected COMPO object. This name must appear in the calling specification to the CRE: module.
(descdata1)	structure containing the interpolation specification if \texttt{COMPO} is the selected option.
(descdata2)	structure containing the interpolation specification if TABLE is the selected option.

```
[[ MIX mix NAMDIR [ DERIV ] [ UPS ]
    [ { I-BURNUP burn | T-BURNUP burn0 burn1 } ]
    [ MICR0 { [[ HISO { conc | * } ]] | ALL } ]
ENDMIX ]]
```

Table 49: Structure (descdata2)

```
[[ MIX mix NAMDIR [ DERIV ] [ UPS ]
   [ { TIMAV-BURN | INST-BURN | AVG-EX-BURN ivarty } ]
   [ MICRO { [[ HISO { conc | * } ]] | ALL } ]
ENDMIX ]]
```

where

MIX	keyword used to set the material mixture <i>mix</i> .
mix	integer identifier for the material mixture that will be included in the MACROLIB. The maximum number of identifiers permitted is <i>nmix</i> and the maximum value that <i>mix</i> may have is <i>nmix</i> . Note that if TABLE is the selected option, then <i>mix</i> identifies the fuel type as defined in the reactor geometry.
NAMDIR	<code>character*12</code> directory name in the CPO object from which the nuclear properties for material mixture mix are to be recovered.
DERIV	keyword used to compute the derivative of the MACROLIB information with respect to $burn$ or $burn1$ value. By default, the MACROLIB information is not differentiated.
UPS	keyword used to compute properties with no up-scattering contribution.
TIMAV-BURN	keyword used to compute time-averaged cross-section information. This option is available only if TABLE is the selected option. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the $FMAP$ object.
INST-BURN	keyword used to compute cross-section information at specific bundle burnups. This option is available <i>only if</i> TABLE is the selected option. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the $FMAP$ object.
AVG-EX-BURN	keyword used to compute the derivatives of cross-section information relative to the exit burnup of a single combustion zone. The derivatives are computed using Eq. (3.3) of Ref. 15, written as
	$\frac{\partial \bar{\Sigma}_x}{\partial B_j^{\rm e}} = \frac{1}{B_j^{\rm e} \left(B_{j,k}^{\rm eoc} - B_{j,k}^{\rm boc}\right)} \left[-\int_{B_{j,k}^{\rm boc}}^{B_{j,k}^{\rm eoc}} dB \Sigma_x(B) + B_{j,k}^{\rm eoc} \Sigma_x(B_{j,k}^{\rm eoc}) - B_{j,k}^{\rm boc} \Sigma_x(B_{j,k}^{\rm boc}) \right]$
	where B^{boc} B^{eoc} and B^{e} are the beginning of cycle burnup of bundle $\{i, k\}$ end of

where $B_{j,k}^{\text{boc}}$, $B_{j,k}^{\text{eoc}}$, and B_j^{e} are the beginning of cycle burnup of bundle $\{j, k\}$, end of cycle burnup of bundle $\{j, k\}$ and exit burnup of channel j. This option is available only if TABLE is the selected option.

ivarty	index of the combustion zone for differentiation of cross-section information.
I-BURNUP	keyword used to perform a single interpolation and to set the burnup interpolation value <i>burn</i> .
burn	real interpolation value of the burnup, given in MW·day per tonne of initial heavy elements.
T-BURNUP	keyword used to perform a time-average MACROLIB evaluation between the burnup values $burn0$ and $burn1$.
burn0	real initial value of the burnup, given in MW·day per tonne of initial heavy elements.
burn1	real final value of the burnup, given in MW-day per tonne of initial heavy elements.
MICRO	keyword used to set the number densities of the extracted isotopes present in the COMPO linked list or XSM file. By default, the extracted isotopes are not added to the resulting MACROLIB.
HISO	character*12 name of an extracted isotope.
conc	user-defined real number density of the extracted isotope, given in 10^{24} particles per cm ³ .
*	keyword used to indicate that the number density for the isotope $HISO$ will be recovered from the COMPO object.
ALL	keyword used to indicate that all the number densities are to be recovered from the COMPO object.
ENDMIX	keyword used to indicate the end of data specification for the material mixture mix .

4.2 The NCR: module

This component of DONJON is dedicated to the interpolation of MICROLIB and MACROLIB data from a MULTICOMPO object, the reactor database produced by COMPO:. A set of *global* and/or *local parameters* are defined for each material mixture and used as multi-dimensional interpolation variables.

The calling specifications are:

Table 50: Structure (NCR:)

MLIB := NCR: [{ MLIB | MLIB2 }] CPONAM1 [[CPONAM2]] [MAPFL] :: (ncr_data)

where

MLIB	character*12 name of a MICROLIB (type L_LIBRARY) or MACROLIB (type L_MACROLIB) containing the interpolated data. If this object also appears on the RHS, it is open in modification mode and updated. A MACROLIB object cannot be specified on the RHS.
MLIB2	$\verb character*12 name of an optional \verb MICROLIB object whose content is copied on $MLIB$.$
CPONAM1	$\tt character*12$ name of the LCM object containing the MULTICOMPO data structure (L_MULTICOMPO signature).
CPONAM2	character*12 name of an additional LCM object containing an auxiliary MULTICOMPO data structure (L_MULTICOMPO signature). This object is optional.
MAPFL	character*12 name of the MAP object containing fuel regions description, global and local parameter information (burnup, fuel/coolant temperatures, coolant density, etc). Keyword TABLE is expected in (ncr_data).
ncr_data	input data structure containing interpolation information (see Section $4.2.1$).

4.2.1 Interpolation data input for module NCR:

Table 51: Structure (ncr_data)

[EDIT iprint]	
[ALLX nbfuel] [RES]	
$[\{ MACRO MICRO \}] [\{ LINEAR CUBIC \}] [LEAK b2]$	
[NMIX nmixt]	
{ [[COMPO CPONAM NAMDIR (descintf)]]	
[[TABLE CPONAM NAMDIR [namburn] (descintf)]] }
;	

where

EDIT keyword used to set *iprint*.

iprint	index used to control the printing in module NCR:. =0 for no print; =1 for minimum printing (default value).
ALLX	keyword used to register the region number of each isotope before merging. This option is useful if the same keyword has been specified in EDI: and COMPO: before.
nbfuel	number of fuel rings used for micro-depletion calculations.
RES	keyword indicating that the interpolation is done only for the microscopic cross sections and not for the isotopic densities. In this case, a RHS MICROLIB must be defined and the number densities are recovered from it. This option is useful for micro-depletion applications. Important note: It is possible to force interpolation of some isotopic densities with RES option if these isotopes are explicitly specified with a "*" flag after MICRO keyword in <i>descintf</i> input data structure (see Section 4.2.2).
MACRO	keyword indicating that $MLIB$ is a MACROLIB (default option).
MICRO	keyword indicating that <i>MLIB</i> is a MICROLIB. Object <i>MLIB</i> contains an embedded MACROLIB, but the CPU time required to obtain it is longer.
LINEAR	keyword indicating that interpolation of the MULTICOMPO uses linear Lagrange polynomials.
CUBIC	keyword indicating that interpolation of the MULTICOMPO uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16 (default option).
LEAK	keyword used to introduce leakage in the embedded MACROLIB. This option should only be used for non-regression tests.
b2	the imposed buckling corresponding to the leakage.
NMIX	keyword used to define the maximum number of material mixtures. This information is required only if $MLIB$ is created.
nmixt	the maximum number of mixtures (a mixture is characterized by a distinct set of macroscopic cross sections) the MACROLIB may contain. The default value is $nmixt = 0$ or the value recovered from <i>MLIB</i> if it appears on the RHS.
СОМРО	keyword used to set $CPONAM$ and to define each global and local parameter.
TABLE	keyword used to set <i>CPONAM</i> and to recover some global and local parameter from a MAP object named <i>MAPFL</i> .
CPONAM	character*12 name of the LCM object containing the MULTICOMPO data structure where the interpolation is performed. This name must be set in the RHS of the (NCR:) data structure.
NAMDIR	access the MULTICOMPO structure of <i>CPONAM</i> from the sub-directory named <i>NAMDIR</i> . This value must be set equal to 'default' if not previously defined by a STEP UP keyword in module COMPO.
namburn	name of the parameter for burnup (or irradiation) in the sub-directory named NAMDIR. This value is defined if option TABLE is set and if burnup (or irradiation) is to be considered as parameter.
descintf	input data structure containing interpolation information relative to the MULTICOMPO data structure named $CPONAM$ (see Section 4.2.2).
4.2.2 Defining local and global parameters

If a MAP object is defined on the RHS of structure (ncr_data), and if the TABLE keyword is set, some information required to set the interpolation points is found in this object. In this case, the NCR: operator search the MULTICOMPO object for global or local parameters having an arbitrary name specified in the MAP object or set directly in this module. Note that any parameter's value set directly in this module prevails on a value stored in the MAP object.

Each instance of descintf is a data structure specified as

Table 52: Structure (descintf)

```
[[ MIX imix [ { FROM imixold | USE } ]
    [ { TIMAV-BURN | INST-BURN | AVG-EX-BURN ivarty } ]
    [[ { SET | DELTA | ADD } ] [ { LINEAR | CUBIC } ] PARKEY { val1 | MAP } [ { val2 | MAP } ]
    [REF [[ PARKEY { valref | SAMEASREF } ]] ENDREF ] ]]
    [MICRO { ALL | ONLY } [[ HISO { conc | * } ]]
ENDMIX ]]
```

where

MIX	keyword used to set $imix.$ Discontinuity factor information present in the Multicompo is interpolated as mixture 1 values.	
imix	index of the mixture that is to be created in the MICROLIB and MACROLIB.	
FROM	keyword used to set the index of the mixture in the MULTICOMPO object.	
imixold	index of the mixture that is recovered in the MULTICOMPO object. By default, $imixold = 1$.	
USE	keyword used to set the index of the mixture in the MULTICOMPO object equal to $imix$.	
TIMAV-BURN	keyword used to compute time-averaged cross-section information. This option is available only if a $MAPFL$ object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the $MAPFL$ object.	
INST-BURN	keyword used to compute cross-section information at specific bundle burnups. This option is available <i>only if</i> a <i>MAPFL</i> object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the <i>MAPFL</i> object.	
AVG-EX-BURN	keyword used to compute the derivatives of cross-section information relative to the exit burnup of a single combustion zone. The derivatives are computed using Eq. (3.3) of Ref. 15, written as	
	$\frac{\partial \bar{\Sigma}_x}{\partial B_j^{\rm e}} = \frac{1}{B_j^{\rm e} \left(B_{j,k}^{\rm eoc} - B_{j,k}^{\rm boc}\right)} \left[-\int_{B_{j,k}^{\rm boc}}^{B_{j,k}^{\rm eoc}} dB \Sigma_x(B) + B_{j,k}^{\rm eoc} \Sigma_x(B_{j,k}^{\rm eoc}) - B_{j,k}^{\rm boc} \Sigma_x(B_{j,k}^{\rm boc}) \right]$	
	where $B_{j,k}^{\text{boc}}$, $B_{j,k}^{\text{eoc}}$, and B_j^{e} are the beginning of cycle burnup of bundle $\{j, k\}$, end of cycle burnup of bundle $\{j, k\}$ and exit burnup of channel j . This option is available only if a MAPFL object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the MAPFL object.	

ivarty

index of the combustion zone for differentiation of cross-section information.

SET	keyword used to indicate a simple interpolation at val1 or an averaging between val1 and val2. The result $\sigma_{\rm ref}$ is also used as the reference value when the ADD is used. Note: see at the ending note of this section for a detailed description and examples.
DELTA	keyword used to indicate a delta-sigma calculation between val2 and val1 (i.e., $\Delta \sigma_{ref} = \sigma_{val2} - \sigma_{val1}$ is computed). Note: see at the ending note of this section for a detailed description and examples.
ADD	keyword used to indicate a delta-sigma calculation between val2 and val1 is added to the reference value (i.e., $\Delta \sigma = \sigma_{val2} - \sigma_{val1}$ is used as contribution, $\sigma_{ref} + \Delta \sigma$ or $\Delta \sigma_{ref} + \Delta \sigma$ is returned). Note: see at the ending note of this section for a detailed description and examples.
LINEAR	keyword indicating that interpolation of the MULTICOMPO for parameter <i>PARKEY</i> uses linear Lagrange polynomials. It is possible to set different interpolation modes to different parameters. By default, the interpolation mode is set in Sect. 4.2.1.
CUBIC	keyword indicating that interpolation of the MULTICOMPO for parameter <i>PARKEY</i> uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16. By default, the interpolation mode is set in Sect. 4.2.1.
PARKEY	${\tt character*12}$ user-defined keyword associated to a global or local parameter to be set.
val1	value of a global or local parameter used to interpolate. <i>val1</i> is the initial value of this parameter in case an average is required. <i>val1</i> can be an integer, real or string value.
val2	value of the final global or local parameter. By default, a simple interpolation is performed, so that $val2=val1$. $val2$ is always a real value with $val2\geq val1$.
МАР	keyword used to indicate that the value of parameter val1 or the second value for the $\Delta \sigma$ calculation is recovered from MAPFL, i.e. the MAP object containing fuel regions description.
REF	keyword only available together with the ADD option. It is used to set all the other variable values when a Δ contribution is performed for one variable.
valref	value of the reference parameter, when it is directly given by the user. Note that there is no default value.
SAMEASREF	keyword used to specify that the reference value will be the same as in the refence case, i.e. for the $\sigma_{\rm ref}$ computation.
ENDREF	keyword only available together with the ADD option. It is used to specify that all the other variable values which are required are given.
MICRO	keyword used to set the number densities of some isotopes present in the MULTICOMPO object. The data statement "MICRO ALL" is used by default.
ALL	keyword to indicate that all the isotopes present in the MULTICOMPO object will be used in the MICROLIB and MACROLIB objects. Concentrations of these isotopes will be recovered from the MULTICOMPO object or set using the "HISO conc" data statement.
ONLY	keyword to indicate that only the isotopes set using the "HISO conc" data statement will be used in the MICROLIB and MACROLIB objects.
HISO	character*8 name of an isotope.
conc	user-defined value of the number density (in 10^{24} particles per cm ³) of the isotope.

*	the value of the number density for isotope $H\!I\!SO$ is recovered from the <code>MULTICOMPO</code> object.
ENDMIX	end of specification keyword for the material mixture.

4.2.3 Interpolation in the parameter grid

The following example corresponds to a delta-sigma computation in mixture 1 corresponding to a perturbation. Note that in this case, the MACROLIB object may content negative cross-section.

```
MACROLIB := NCR: CPO ::
EDIT 40 NMIX 1 MACRO COMPO CPO default
MIX 1 !(* delta sigma contribution *)
SET 'CELL' '3D'
DELTA 'PITCH' 0.0 1.0
ENDMIX
```

```
;
```

When the number of parameters used for the interpolation is increased, all the lattice computations corresponding to all the combinations of parameters may not be done for computation time reasons. In this case, some approximations may be required. The choice for the SET, DELTA and ADD is then dependent of the structure of the database (i.e. how the database grid of possibilities is filled). When a MAP object containing fuel regions description is used, the problem become even more complex, because values have to be automatically changed for all bundles. In order to clarify all the different possibilities and limitations dependently of the database structure, we will use a 3 parameter case. The parameters are referenced by 'A', 'B' and 'C'. But before we explain the different cases, we want to remind that the interpolation factors are computed on each axis seperatly.

The first case corresponds to a complete grid, represented by a gray paralepiped on Fig. 2 and 3. The figure 2 shows that the interpolated value in point V can be obtained directly without MAP object. For time-average (TA) computation, lets assume that the parameter 'B' represents the burnup (and keep this convention for other database structure also). In this case the figure 3 shows also that the direct interpolation can be done to compute an average value between the points V' and V. Note that the TA burnups are stored in the MAP object, and are then recovered automatically.

The second case corresponds to a partial grid where all the lattice computations have been performed for several pairs of parameters, which are represented as the gray rectangles on Fig. 4 and 5. If we use the notations of Fig. 4 and 5, the best estimate interpolated values, f, we can get are given by:

 $f = f(V) \approx f(V_B) + (f(V_{BA}) - f(V_B)) + (f(V_{BC}) - f(V_B)) = f(V_{BC}) + (f(V_{BA}) - f(V_B)) = f(V_{BA}) + (f(V_{BC}) - f(V_B))$ for instataneous

 $f = f(V', V) \approx f(V'_B, V_B) + (f(V'_{BA}, V_{BA}) - f(V'_B, V_B)) + (f(V'_{BC}, V_{BC}) - f(V'_B, V_B)) = f(V'_{BC}, V_{BC}) + (f(V'_{BA}, V_{BA}) - f(V'_B, V_B)) = f(V'_{BA}, V_{BA}) + (f(V'_{BC}, V_{BC}) - f(V'_B, V_B)) \text{ for TA}$ where f(.,.) represents the average value between two points.

where f(.,.) represents the average value between two points.

The third case corresponds to a minimal grid, where the lattice computations have been performed only for one parameter variation at a time. In this case, the grid is represented by the thick gray lines on the axis on Fig. 6 and 7. If we use the notations of Fig. 6 and 7, the best estimate interpolated values, f, we can get are given by:

$$f = f(V) \approx f(V_0) + (f(V_A) - f(V_0)) + (f(V_B) - f(V_0)) + (f(V_C) - f(V_0)) = f(V_B) + (f(V_A) - f(V_0)) + (f(V_C) - f(V_0))$$
 for instataneous

 $f = f(V', V) \approx f(V'_B, V_B) + (f(V_A) - f(V_0)) + (f(V_C) - f(V_0))$ for TA

Note that the reference point (V_0 in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 8 can also been used. In this case, we even have two choices for the Δf computation on axis 'A'.

The last case is in fact a mix of cases 2 and 3. The gray rectangle and the gray line on Fig. 9 and 10 represent where all the lattice computations have been performed. With the notations used on those

figures, one can write that the best estimate interpolated values, f, we can get are given by:

 $\begin{aligned} f &= f(V) \approx f(V_B) + (f(V_{BC}) - f(V_B)) + (f(V_A) - f(V_0)) = f(V_{BC}) + (f(V_A) - f(V_0)) \text{ for instataneous} \\ f &= f(V', V) \approx f(V'_B, V_B) + (f(V'_{BC}, V_{BC}) - f(V'_B, V_B)) + (f(V_A) - f(V_0)) = f(V'_{BC}, V_{BC}) + (f(V_A) - f(V_0)) \\ f(V_0)) \text{ for TA} \end{aligned}$

Note once again that the reference point (V_0 in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 11 can also been used.

The input files will actually reflect the previous equations. However, they are different if the parameters are stored in a MAP object, *MAPFL*, or provided directly by the user. For the case of one point interpolation (i.e. instantaneous), the input files will be:

case	all parameters explicitly set	all parameters in MAP
GRID (Fig. 2)	<pre>MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc>> ENDMIX;</vc></vb></va></pre>	MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 ENDMIX ;
PLANE (Fig. 4)	<pre>MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vco>> ADD 'C' <<vco>> <<vc>> REF 'A' <<vao>> 'B' <<vb>> ENDREF !or 'B' SAMEASREF ENDREF ENDMIX;</vb></vao></vc></vco></vco></vb></va></pre>	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'C' <<vco>> ADD 'C' <<vco>> MAP REF 'A' <<vao>> 'B' SAMEASREF ENDREF !or SET 'A' <<vao>> !or ADD 'A' <<vao>> !or REF 'C' <<vco>> !or REF 'C' <<vco>> !or 'B' SAMEASREF ENDREF ENDMIX ;</vco></vco></vao></vao></vao></vco></vco></pre>
AXE (Fig. 6)	<pre>MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va0>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> B' <<vb0>> ENDREF ADD 'C' <<vc0>> REF 'A' <<va0>> B' <<vb0>> ENDREF ADD 'C' <<vc0>> REF 'A' <<va0>> B' <<vb0>> ENDREF ENDMIX;</vb0></va0></vc0></vb0></va0></vc0></vb0></vc0></va></va0></vc0></vb></va0></pre>	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;</vb0></va0></vc0></vb0></vc0></va0></vc0></va0></pre>

case	all parameters explicitly set	all parameters in MAP
PLANE +		
AXE (Fig. 9)	<pre>MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va0>> SET 'B' <<vb>> SET 'C' <<vc>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX;</vb0></vc0></va></va0></vc></vb></va0></pre>	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX;</vb0></vc0></va0></va0></pre>

Table 53: NCR inputs for instantaneous cases

For the TA, the burnup variable has no other choice than to be stored in the MAP object, MAPFL. Then the input files will be:

case	only the burnup in MAP	all parameters in MAP
GRID (Fig. 3)	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vc>> ENDMIX;</vc></va></pre>	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 ENDMIX;</pre>
PLANE (Fig. 5)	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vco>> ADD 'C' <<vco>> <<vc>> REF 'A' <<vao>> 'B' SAMEASREF ENDREF ENDMIX;</vao></vc></vco></vco></va></pre>	<pre>MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'C' <<vco>> ADD 'C' <<vco>> MAP REF 'A' <<vao>> 'B' SAMEASREF ENDREF !or SET 'A' <<vao>> !or ADD 'A' <<vao>> !or REF 'C' <<vco>> !or REF 'C' <<vco>> !or 'B' SAMEASREF ENDREF ENDMIX ;</vco></vco></vao></vao></vao></vco></vco></pre>

-

case	only the burnup in MAP	all param. in MAP
AXE (Fig.		
7)	MACROLTB := NCB: CPO FMAP ::	MACROLTE := NCE: CPO FMAP ::
	NMIX 1 MACRO	NMIX 1 MACRO
	TABLE CPO default 'B'	TABLE CPO default 'B'
	MIX 1	MIX 1
	SET 'A' < <va0>></va0>	SET 'A' < <va0>></va0>
	SET 'C' < <vc0>></vc0>	SET 'C' < <vc0>></vc0>
	ADD 'A' < <va0>> <<va>></va></va0>	ADD 'A' < <va0>> MAP</va0>
	REF 'C' < <vc0>></vc0>	REF 'C' < <vc0>></vc0>
	'B' < <vb0>> ENDREF</vb0>	'B' < <vb0>> ENDREF</vb0>
	ADD 'C' < <vc0>> <<vc>>></vc></vc0>	ADD 'C' < <vco>> MAP</vco>
	REF 'A' < <va0>></va0>	REF 'A' < <va0>></va0>
	'B' < <vb0>> ENDREF</vb0>	'B' < <vb0>> ENDREF</vb0>
	ENDMIX	ENDMIX
	;	;
PLANE +		
AXE (Fig.	MACROLIB := NCR: CPO FMAP ::	MACROLIB := NCR: CPO FMAP ::
10)	NMIX 1 MACRO	NMIX 1 MACRO
	TABLE CPO default 'B'	TABLE CPO default 'B'
	MIX 1	MIX 1
	SET 'A' < <va0>></va0>	SET 'A' < <va0>></va0>
	SET 'C' < <vc>></vc>	ADD 'A' < <va0>> MAP</va0>
	ADD 'A' < <va0>> <<va>></va></va0>	REF 'C' < <vc0>></vc0>
	REF 'C' < <vc0>></vc0>	'B' < <vb0>> ENDREF</vb0>
	'B' < <vb0>> ENDREF</vb0>	ENDMIX
	ENDMIX	•
	•	

Table 54: NCR inputs for TA cases

The following pictures correspond to the previous different examples:



Figure 2: Complete grid, one point case



Figure 3: Complete grid, TA case



Figure 4: Partial grid, complete planes, one point case



Figure 5: Partial grid, complete planes, TA case



Figure 6: Partial grid, complete axis, one point case



Figure 7: Partial grid, complete axis, TA case





configuration, one point case

Figure 8: Partial grid, complete axis with another Figure 10: Partial grid, one complete plane and one complete axis, TA case



Figure 9: Partial grid, one complete plane and one complete axis, one point case



Figure 11: Partial grid, one complete plane and one complete axis with another configuration, one point case

4.3 The SCR: module

This component of DONJON is dedicated to the interpolation of MACROLIB data from a SAPHYB object, the reactor database produced by module SAP: in DRAGON or by module SAPHYB: in APOLLO2.^[24] A set of global parameters are defined for each material mixture and used as multi-dimensional interpolation variables.

The calling specifications are:

Table 55: Structure (SCR:)

MLIB := SCR: [{ MLIB | MLIB2 }] SAPNAM1 [[SAPNAM2]] [MAPFL] :: (scr_data)

where

MLIB	character*12 name of a MICROLIB (type L_LIBRARY) or MACROLIB (type L_MACROLIB) containing the interpolated data. If this object also appears on the RHS, it is open in modification mode and updated. A MACROLIB object cannot be specified on the RHS.
MLIB2	$\verb+character*12 name of an optional \verb+MICROLIB+ object whose content is copied on $MLIB$.$
SAPNAM1	<code>character*12</code> name of the LCM object containing the <code>SAPHYB</code> data structure (<code>L_SAPHYB</code> signature).
SAPNAM2	$\label{eq:character*12} \begin{array}{l} \text{character*12} \text{ name of an additional LCM object containing an auxiliary SAPHYB data structure (L_SAPHYB signature). This object is optional. \end{array}$
MAPFL	character*12 name of the MAP object containing fuel regions description, global parameter information (burnup, fuel/coolant temperatures, coolant density, etc). Keyword TABLE is expected in (scr_data).
scr_data	input data structure containing interpolation information (see Section $4.3.1$).

Note: SAPHYB files generated by APOLLO2 don't have a signature. If such a SAPHYB is given as input to module SCR:, a signature must be included before using it. The following instruction can do the job:

Saphyb := UTL: Saphyb :: CREA SIGNATURE 3 = 'L_SA' 'PHYB' ' ;

4.3.1 Interpolation data input for module SCR:

Table 56: Structure (scr_data)

```
[ EDIT iprint ]
[ MEMORY ]
[ RES ]
[ { MACRO | MICRO } ] [ { LINEAR | CUBIC } ] [ LEAK b2 ] [ EQUI TEXT4 ]
[ NMIX nmixt ]
{ [[ SAPHYB SAPNAM (descints) ]] | [[ TABLE SAPNAM [ namburn ] (descints) ]] }
[ (descdepl) ]
;
```

where	
EDIT	keyword used to set <i>iprint</i> .
iprint	index used to control the printing in module SCR:. =0 for no print; =1 for minimum printing (default value).
MEMORY	keyword activating a copy of the Saphyb into memory before performing interpolation. In some cases, this operation may reduce CPU resources in SCR:.
RES	keyword indicating that the interpolation is done only for the microscopic cross sections and not for the isotopic densities. In this case, a RHS MICROLIB must be defined and the number densities are recovered from it. This option is useful for micro-depletion applications. Important note: It is possible to force interpolation of some isotopic densities with RES option if these isotopes are explicitely specified with a "*" flag after MICRO keyword in <i>descints</i> input data structure (see Section 4.3.2).
MACRO	keyword indicating that $MLIB$ is a MACROLIB (default option).
MICRO	keyword indicating that <i>MLIB</i> is a MICROLIB. Object <i>MLIB</i> contains an embedded MACROLIB, but the CPU time required to obtain it is longer.
LINEAR	keyword indicating that interpolation of the SAPHYB uses linear Lagrange polynomials.
CUBIC	keyword indicating that interpolation of the SAPHYB uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16 (default option).
LEAK	keyword used to introduce leakage in the embedded MACROLIB. This option should only be used for non-regression tests.
b2	the imposed buckling corresponding to the leakage.
EQUI	keyword used to select a SPH factor set in the Saphyb. By default, the cross sections and diffusion coefficients are not SPH-corrected.
TEXT4	character*4 user-defined keyword of the SPH factor set selected in the Saphyb. These sets are stored as local parameter information in the Saphyb.
NMIX	keyword used to define the maximum number of material mixtures. This information is required only if $MLIB$ is created.
nmixt	the maximum number of mixtures (a mixture is characterized by a distinct set of macroscopic cross sections) the MACROLIB may contain. The default value is $nmixt = 0$ or the value recovered from <i>MLIB</i> if it appears on the RHS.
SAPHYB	keyword used to set $SAPNAM$ and to define each global parameter.
TABLE	keyword used to set $SAPNAM$ and to recover some global parameter from a MAP object named $MAPFL$.
SAPNAM	character*12 name of the LCM object containing the SAPHYB data structure where the interpolation is performed. This name must be set in the RHS of the (SCR:) data structure.
namburn	name of the parameter for burnup (or irradiation). This value is defined if option TABLE is set <i>and</i> if burnup (or irradiation) is to be considered as parameter.
descints	input data structure containing interpolation information relative to the SAPHYB data structure named $SAPNAM$ (see Section 4.3.2).

(descdepl) input structure describing the depletion chain (see Section 4.3.3). This input structure requires option MICRO. By default, the depletion chain data is not written in the output MICROLIB.

4.3.2 Defining global parameters

If a MAP object is defined on the RHS of structure (scr_data), and if the TABLE keyword is set, some information required to set the interpolation points is found in this object. In this case, the SCR: operator search the SAPHYB object for global parameters having an arbitrary name specified in the MAP object or set directly in this module. Note that any parameter's value set directly in this module prevails on a value stored in the MAP object.

Each instance of descints is a data structure specified as

Table 57: Structure (descints)

```
[[ MIX imix [ { FROM imixold | USE } ]
    [ { TIMAV-BURN | INST-BURN | AVG-EX-BURN ivarty } ]
    [[ { SET | DELTA | ADD } } [ { LINEAR | CUBIC } ] PARKEY { val1 | MAP } [ { val2 | MAP } ]
    [ REF [[ PARKEY { valref | SAMEASREF } ]] ENDREF ] ]]
    [ MICRO { ALL | ONLY } [[ HISO { conc | * } ]]
ENDMIX ]]
```

where

MIX	keyword used to set $imix.$ Discontinuity factor information present in the Saphyb is interpolated as mixture 1 values.	
imix	index of the mixture that is to be created in the MICROLIB and MACROLIB.	
FROM	keyword used to set the index of the mixture in the SAPHYB object.	
imixold	index of the mixture that is recovered in the SAPHYB object. By default, $imixold = 1$.	
USE	keyword used to set the index of the mixture in the SAPHYB object equal to <i>imix</i> .	
TIMAV-BURN	keyword used to compute time-averaged cross-section information. This option is available only if a MAPFL object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the MAPFL object.	
INST-BURN	keyword used to compute cross-section information at specific bundle burnups. This option is available <i>only if</i> a <i>MAPFL</i> object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the <i>MAPFL</i> object.	
AVG-EX-BURN	keyword used to compute the derivatives of cross-section information relative to the exit burnup of a single combustion zone. The derivatives are computed using Eq. (3.3) of Ref. 15, written as	
	$\frac{\partial \bar{\Sigma}_x}{\partial B_j^{\rm e}} = \frac{1}{B_j^{\rm e} \left(B_{j,k}^{\rm eoc} - B_{j,k}^{\rm boc}\right)} \left[-\int_{B_{j,k}^{\rm boc}}^{B_{j,k}^{\rm eoc}} dB \Sigma_x(B) + B_{j,k}^{\rm eoc} \Sigma_x(B_{j,k}^{\rm eoc}) - B_{j,k}^{\rm boc} \Sigma_x(B_{j,k}^{\rm boc}) \right]$	

where $B_{j,k}^{\text{boc}}$, $B_{j,k}^{\text{eoc}}$, and B_j^{e} are the beginning of cycle burnup of bundle $\{j,k\}$, end of cycle burnup of bundle $\{j,k\}$ and exit burnup of channel j. This option is available

	only if a $MAPFL$ object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the $MAPFL$ object.
ivarty	index of the combustion zone for differentiation of cross-section information.
SET	keyword used to indicate a simple interpolation at val1 or an averaging between val1 and val2. The result σ_{ref} is also used as the reference value when the ADD is used. Note: see at the ending note of this section for a detailed description and examples.
DELTA	keyword used to indicate a delta-sigma calculation between val2 and val1 (i.e., $\Delta \sigma_{\rm ref} = \sigma_{\rm val2} - \sigma_{\rm val1}$ is computed). Note: see at the ending note of this section for a detailed description and examples.
ADD	keyword used to indicate a delta-sigma calculation between val2 and val1 is added to the reference value (i.e., $\Delta \sigma = \sigma_{\text{val2}} - \sigma_{\text{val1}}$ is used as contribution, $\sigma_{\text{ref}} + \Delta \sigma$ or $\Delta \sigma_{\text{ref}} + \Delta \sigma$ is returned). Note: see at the ending note of this section for a detailed description and examples.
LINEAR	keyword indicating that interpolation of the SAPHYB for parameter <i>PARKEY</i> uses linear Lagrange polynomials. It is possible to set different interpolation modes to different parameters. By default, the interpolation mode is set in Sect. 4.3.1.
CUBIC	keyword indicating that interpolation of the SAPHYB for parameter <i>PARKEY</i> uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16. By default, the interpolation mode is set in Sect. 4.3.1.
PARKEY	character*12 user-defined keyword associated to a global parameter to be set.
val1	value of a global parameter used to interpolate. <i>val1</i> is the initial value of this parameter in case an average is required. <i>val1</i> can be an integer, real or string value.
val2	value of the final global parameter. By default, a simple interpolation is performed, so that $val2=val1$. $val2$ is always a real value with $val2\geq val1$.
MAP	keyword used to indicate that the value of parameter val1 or the second value for the $\Delta\sigma$ calculation is recovered from MAPFL, i.e. the MAP object containing fuel regions description.
REF	keyword only available together with the ADD option. It is used to set all the other variable values when a Δ contribution is performed for one variable.
valref	value of the reference parameter, when it is directly given by the user. Note that there is no default value.
SAMEASREF	keyword used to specify that the reference value will be the same as in the reference case, i.e. for the σ_{ref} computation.
ENDREF	keyword only available together with the ADD option. It is used to specify that all the other variable values which are required are given.
MICRO	keyword used to set the number densities of some isotopes present in the SAPHYB object. The data statement "MICRO ALL" is used by default.
ALL	keyword to indicate that all the isotopes present in the SAPHYB object will be used in the MICROLIB and MACROLIB objects. Concentrations of these isotopes will be recovered from the SAPHYB object or set using the "HISO conc" data statement.
ONLY	keyword to indicate that only the isotopes set using the "HISO conc" data statement will be used in the MICROLIB and MACROLIB objects.

IGE-300	79
HISO	character*8 name of an isotope.
conc	user-defined value of the number density (in 10^{24} particles per cm ³) of the isotope.
*	the value of the number density for isotope $H\!ISO$ is recovered from the SAPHYB object
ENDMIX	end of specification keyword for the material mixture.

4.3.3 Depletion data structure

Part of the depletion data used in the isotopic depletion calculation (the fission yields and the radioactive decay constants) is recovered from the Saphyb file. Remaining depletion data is recovered from the input data structure (descdepl). This data describes the heredity of the radioactive decay and the neutron activation chain.

Table 58: Structure (descdepl)

```
CHAIN
  [[ NAMDPL [ izae ]
    [[ reaction [ energy ] ]]
    [{ STABLE | FROM [[ { DECAY | reaction } [[ yield NAMPAR ]] ]] } ]]
ENDCHAIN
```

with:

CHAIN	keyword f	to specify the	beginning	of the	depletion	chain.
-------	-----------	----------------	-----------	--------	-----------	--------

- NAMDPL character*12 name of an isotope (or isomer) of the depletion chain that appears as a particularized isotope of the Saphyb.
- izae optional six digit integer representing the isotope. The first two digits represent the atomic number of the isotope; the next three indicate its mass number and the last digit indicates the excitation level of the nucleus (0 for a nucleus in its ground state, 1 for an isomer in its first exited state, etc.). For example, ²³⁸U in its ground state will be represented by izae=922380.
- reactioncharacter*6 identification of a neutron-induced reaction that takes place either for production of this isotope, its depletion, or for producing energy. Example of reactions are following:
 - NG indicates that a radiative capture reaction takes place either for production of this isotope, its depletion or for producing energy.
 - indicates that the following reaction is taking place: N2N

$$n + {}^A X_Z \to 2n + {}^{A-1} X_Z$$

N3N indicates that the following reaction is taking place:

$$n + X_Z \rightarrow 3n + X_Z$$

	N4N	indicates that the following reaction is taking place:	
		$n + {}^A X_Z \to 4n + {}^{A-3} X_Z$	
	NP	indicates that the following reaction is taking place:	
		$n + {}^A X_Z \to p + {}^A Y_{Z-1}$	
	NA	indicates that the following reaction is taking place:	
		$n + {}^A X_Z \to {}^4 \operatorname{He}_2 + {}^{A-3} X_{Z-2}$	
	NFTOT	indicates that a fission is taking place.	
energy	energy (in MeV) recoverable per neutron-induced reaction of type reaction. If the energy associated to radiative capture is not explicitly given, it should be added to the energy released per fission. By default, $energy=0.0$ MeV.		
STABLE	non depleting isotope. Such an isotope may produces energy by neutron-induced reactions (such as radiative capture).		
FROM	indicates that this isotope is produced from decay or neutron-induced reactions.		
DECAY	indicates that a decay reaction takes place for its production.		
yield	branching ratio or production yield expressed in fraction.		
NAMPAR	character*12 name of the a parent isotope (or isomer) that appears as a particularized isotope of the Saphyb.		
ENDCHAIN	keyword to specify the end of the depletion chain.		

4.3.4 Interpolation in the parameter grid

The following example corresponds to a delta-sigma computation in mixture 1 corresponding to a perturbation. Note that in this case, the MACROLIB object may content negative cross-section.

```
MACROLIB := SCR: SAP ::
EDIT 40 NMIX 1 SAPHYB SAP
MIX 1 !(* delta sigma contribution *)
SET 'CELL' '3D'
DELTA 'PITCH' 0.0 1.0
ENDMIX
;
```

When the number of parameters used for the interpolation is increased, all the lattice computations corresponding to all the combinations of parameters may not be done for computation time reasons. In this case, some approximations may be required. The choice for the SET, DELTA and ADD is then dependent of the structure of the database (i.e. how the database grid of possibilities is filled). When a MAP object containing fuel regions description is used, the problem become even more complex, because values have to be automatically changed for all bundles. In order to clarify all the different possibilities and limitations dependently of the database structure, we will use a 3 parameter case. The parameters are referenced by 'A', 'B' and 'C'. But before we explain the different cases, we want to remind that the interpolation factors are computed on each axis seperatly.

The first case corresponds to a complete grid, represented by a gray paralepiped on Fig. 2 and 3. The figure 2 shows that the interpolated value in point V can be obtained directly without MAP object. For time-average (TA) computation, lets assume that the parameter 'B' represents the burnup (and keep this convention for other database structure also). In this case the figure 3 shows also that the direct interpolation can be done to compute an average value between the points V' and V. Note that the TA burnups are stored in the MAP object, and are then recovered automatically.

The second case corresponds to a partial grid where all the lattice computations have been performed for several pairs of parameters, which are represented as the gray rectangles on Fig. 4 and 5. If we use the notations of Fig. 4 and 5, the best estimate interpolated values, f, we can get are given by:

 $f = f(V) \approx f(V_B) + (f(V_{BA}) - f(V_B)) + (f(V_{BC}) - f(V_B)) = f(V_{BC}) + (f(V_{BA}) - f(V_B)) = f(V_{BA}) + (f(V_{BC}) - f(V_B))$ for instataneous

 $f = f(V', V) \approx f(V'_B, V_B) + (f(V'_{BA}, V_{BA}) - f(V'_B, V_B)) + (f(V'_{BC}, V_{BC}) - f(V'_B, V_B)) = f(V'_{BC}, V_{BC}) + (f(V'_{BA}, V_{BA}) - f(V'_B, V_B)) = f(V'_{BA}, V_{BA}) + (f(V'_{BC}, V_{BC}) - f(V'_B, V_B))$ for TA

where f(.,.) represents the average value between two points.

The third case corresponds to a minimal grid, where the lattice computations have been performed only for one parameter variation at a time. In this case, the grid is represented by the thick gray lines on the axis on Fig. 6 and 7. If we use the notations of Fig. 6 and 7, the best estimate interpolated values, f, we can get are given by:

 $f = f(V) \approx f(V_0) + (f(V_A) - f(V_0)) + (f(V_B) - f(V_0)) + (f(V_C) - f(V_0)) = f(V_B) + (f(V_A) - f(V_0)) + (f(V_C) - f(V_0))$ for instataneous

 $f = f(V', V) \approx f(V'_B, V_B) + (f(V_A) - f(V_0)) + (f(V_C) - f(V_0))$ for TA

Note that the reference point (V_0 in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 8 can also been used. In this case, we even have two choices for the Δf computation on axis 'A'.

The last case is in fact a mix of cases 2 and 3. The gray rectangle and the gray line on Fig. 9 and 10 represent where all the lattice computations have been performed. With the notations used on those figures, one can write that the best estimate interpolated values, f, we can get are given by:

 $\begin{aligned} f &= f(V) \approx f(V_B) + (f(V_{BC}) - f(V_B)) + (f(V_A) - f(V_0)) = f(V_{BC}) + (f(V_A) - f(V_0)) \text{ for instataneous} \\ f &= f(V', V) \approx f(V'_B, V_B) + (f(V'_{BC}, V_{BC}) - f(V'_B, V_B)) + (f(V_A) - f(V_0)) = f(V'_{BC}, V_{BC}) + (f(V_A) - f(V_0)) \\ f(V_0)) \text{ for TA} \end{aligned}$

Note once again that the reference point (V_0 in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 11 can also been used.

The input files will actually reflect the previous equations. However, they are different if the parameters are stored in a MAP object, *MAPFL*, or provided directly by the user. For the case of one point interpolation (i.e. instantaneous), the input files will be:

case	all parameters explicitly set	all parameters in MAP
GRID (Fig. 2)	<pre>MACROLIB := SCR: SAP :: NMIX 1 SAPHYB SAP MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc>> ENDMIX;</vc></vb></va></pre>	MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 ENDMIX ;
PLANE (Fig. 4)	<pre>MACROLIB := SCR: SAP :: NMIX 1 SAPHYB SAP MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' <<vb>> ENDREF !or 'B' SAMEASREF ENDREF ENDMIX;</vb></va0></vc></vc0></vc0></vb></va></pre>	<pre>MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'C' <<vco>> ADD 'C' <<vco>> MAP REF 'A' <<vao>> 'B' SAMEASREF ENDREF !or SET 'A' <<vao>> !or ADD 'A' <<vao>> !or ADD 'A' <<vao>> !or REF 'C' <<vco>> !or B' SAMEASREF ENDREF ENDMIX;</vco></vao></vao></vao></vao></vco></vco></pre>
AXE (Fig. 6)	<pre>MACROLIB := SCR: SAP :: NMIX 1 SAPHYB SAP MIX 1 SET 'A' <<va0>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> B' <<vb0>> ENDREF ADD 'C' <<vc0>> REF 'A' <<va0>> B' <<vb0>> ENDREF ADD 'C' <<vc0>> REF 'A' <<va0>> B' <<vb0>> ENDREF ENDMIX;</vb0></va0></vc0></vb0></va0></vc0></vb0></vc0></va></va0></vc0></vb></va0></pre>	<pre>MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;</vb0></va0></vc0></vb0></va0></vc0></vb0></vc0></va0></vc0></va0></pre>

case	all parameters explicitly set	all parameters in MAP
PLANE +		
AXE (Fig. 9)	<pre>MACROLIB := SCR: SAP :: NMIX SAPHYB SAP MIX 1 SET 'A' <<va0>> SET 'B' <<vb>> SET 'C' <<vc>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX ;</vb0></vc0></va></va0></vc></vb></va0></pre>	<pre>MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX;</vb0></vc0></va0></va0></pre>

Table 59: SCR inputs for instantaneous cases

For the TA, the burnup variable has no other choice than to be stored in the MAP object, MAPFL. Then the input files will be:

case	only the burnup in MAP	all parameters in MAP
GRID		
(Fig. 3)	<pre>MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vc>> ENDMIX;</vc></va></pre>	MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 ENDMIX ;
PLANE		
(Fig. 5)	<pre>MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vco>> ADD 'C' <<vco>> <<vc>> REF 'A' <<vao>> 'B' SAMEASREF ENDREF ENDMIX;</vao></vc></vco></vco></va></pre>	<pre>MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'C' <<vco>> ADD 'C' <<vco>> MAP REF 'A' <<vao>> 'B' SAMEASREF ENDREF !or SET 'A' <<vao>> !or ADD 'A' <<vao>> !or ADD 'A' <<vao>> !or REF 'C' <<vco>> !or 'B' SAMEASREF ENDREF ENDMIX ;</vco></vao></vao></vao></vao></vco></vco></pre>

-

case	only the burnup in MAP	all param. in MAP
AXE (Fig.		
7)	MACROLIB := SCR: SAP FMAP ::	MACROLIB := SCR: SAP FMAP ::
	NMIX 1	NMIX 1
	TABLE SAP 'B'	TABLE SAP 'B'
	MIX 1	MIX 1
	SET 'A' < <va0>></va0>	SET 'A' < <va0>></va0>
	SET 'C' < <vc0>></vc0>	SET 'C' < <vc0>></vc0>
	ADD 'A' < <va0>> <<va>></va></va0>	ADD 'A' < <va0>> MAP</va0>
	REF 'C' < <vc0>></vc0>	REF 'C' < <vco>></vco>
	'B' < <vb0>> ENDREF</vb0>	'B' < <vb0>> ENDREF</vb0>
	ADD 'C' < <vc>>> <<vc>>></vc></vc>	ADD 'C' < <vco>> MAP</vco>
	REF 'A' < <va0>></va0>	REF 'A' < <va0>></va0>
	'B' < <vb0>> ENDREF</vb0>	'B' < <vb0>> ENDREF</vb0>
	ENDMIX	ENDMIX
	;	,
PLANE +		
AXE (Fig.	MACROLIB := SCR: SAP FMAP ::	MACROLIB := SCR: SAP FMAP ::
10)	NMIX 1	NMIX 1
	TABLE SAP 'B'	TABLE SAP 'B'
	MIX 1	MIX 1
	SET 'A' < <va0>></va0>	SET 'A' < <va0>></va0>
	SET 'C' < <vc>></vc>	ADD 'A' < <va0>> MAP</va0>
	ADD 'A' < <va0>> <<va>></va></va0>	REF 'C' < <vc0>></vc0>
	REF 'C' < <vc0>></vc0>	'B' < <vb0>> ENDREF</vb0>
	'B' < <vb0>> ENDREF</vb0>	ENDMIX
	ENDMIX	;
	;	

Table 60: SCR inputs for TA cases

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4.4 The AFM: module

The AFM: module is used to create an extended MACROLIB containing set of interpolated nuclear properties from a feedback model database.^[20] The DATABASE information are obtained by previous DRAGON calculations using module CFC:.^[17]

There are two possible utilizations:

- Construction of an extended MACROLIB for fuel properties directly from DATABASE information with respect to local parameters contained in the fuel map object or directly input.
- Construction of an extended MACROLIB containing only one set of cross sections derivated from the DATABASE information. Properties can be obtained for fuel or reflector.

The calling specifications are:

Table 61: Structure AFM:

MACRO := AFM: [MACRO] DBASE [MAPFL] :: (descafm)

where

MACRO	$\tt character*12$ name of the extended MACROLIB. The MACROLIB can be in modification mode.
DBASE	$\tt character*12$ name of the <code>DATABASE</code> object containing fuel properties with respect to local parameters.
MAPFL	character*12 name of the MAP object containing fuel regions description and burnup informations. This file is only required when a MACRO is created for fuel area.
(descafm)	structure containing the data to module AFM:.

4.4.1 Input data to the AFM: module

Table 62: Structure (descafm)

```
{ MAP | MCR mmix } INFOR NAMDB
DNAME ntyp ( NAMTYP(i), i=1,ntyp )
REFT ( imix(i) NAMTYP(i), i=1,ntyp )
[ EDIT iprint ]
[ FIXP { INIT | pow } ]
[ { PWF | NPWF } ]
[ TFUEL tfuel ]
[ TCOOL tcool ]
[ TMOD tmod ]
```

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continued on next page

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Structure (descafm)

continued from last page

[BORON nB]
[RDCL dcool]
[RDMD dmod]
[PUR purity]
BURN bval
$\left[\left\{ \text{ XENON } nXe \mid \text{ XEREF } \right\} \right]$
$[\{ \text{NEP } nNp \mid \text{NREF } \}]$
[SAM nSm]
[IMET imet]
[BLIN]

where

MAP	keyword to specify that a MACROLIB for fuel properties will be computed.
MCR	keyword to specify that a MACROLIB containing only one non-zero mixture will be created.
mmix	maximum number of mixtures in the MACROLIB.
INFOR	keyword to specify the data base name.
NAMDB	character*72 title of the database as it has been created.
DNAME	keyword to specify the number of fuel types and their names as stored in the data base.
ntyp	number of fuel types. For MCR option, $ntyp$ must be 1.
NAMTYP(i)	$\verb+character*12 name of the directory where each fuel type information has been stored.$
REFT	keyword to specify a number associated with a fuel type name.
<i>imi</i> x(i)	fuel type index as specified for the fuel map or a non-zero mixture number for the single-property sc macrolib.
EDIT	keyword used to set <i>iprint</i> .
iprint	index used to control the printing in module $AFM: =0$ for no print(default value); =1 for minimum printing; larger values produce increasing amounts of output.
FIXP	keyword used to set the power used for cross-section interpolation.
INIT	a distributed beginning-of-transient bundle power in kW is used. This power distribution has to be pre-calculated in the FLPOW: module using the INIT keyword.
pow	uniform bundle power in kW. If this data is omitted, the reference value in the data base is used or the bundle powers present in a MAP. The reference value is 615 kW if none were provided at the database computation time.
PWF	keyword used to activate power bundle feedback on fuel properties using powers recovered from 'BUND-PW' record in $MAPFL$. This is the default option if MAP is selected.
NPWF	keyword used to desactivate ${\tt PWF}$ feedback. This is the only possible option if ${\tt MCR}$ is selected.

TFUEL	keyword used to set <i>tfuel</i> .
tfuel	fuel temperature in K. If this data is omitted and the bundle powers present in a MAP, fuel temperatures are computed with respect to powers. If this data is omitted and there is no bundle power, the reference value in the data base is used, where it is 941.29 K if none were provided at the database computation time.
TCOOL	keyword used to set <i>tcool</i> .
tcool	coolant temperature in K. If this data is omitted, the reference value in the data base is used. The reference value is 560.66 K if none were provided at the database computation time.
TMOD	keyword used to set <i>tmod</i> .
tmod	moderator temperature in K. If this data is omitted, the reference value in the data base is used. The reference value is 345.66 K if none were provided at the database computation time.
BORON	keyword used to set nB .
nB	Boron concentration in ppm. If this data is omitted, the reference value in the data base is used. The reference value is 0.0 ppm. See note below for inside equations.
RDCL	keyword used to set <i>dcool</i> .
dcool	coolant density in g/cm^3 . If this data is omitted, the reference value in the data base is used. The reference value is 0.81212 g/cm^3 if none were provided at the database computation time.
RDMD	keyword used to set <i>dmod</i> .
dmod	moderator density in g/cm^3 . If this data is omitted, the reference value in the data base is used. The reference value is 1.082885 g/cm^3 if none were provided at the database computation time.
PUR	keyword used to set <i>purity</i> .
purity	moderator purity in atm%. If this data is omitted, the reference value in the data base is used. The reference value is 99.911 atm% if none were provided at the database computation time.
BURN	keyword used to set $bval.$ This option is valid only when $\tt MCR$ is used and can not be omitted.
bval	fuel burnup in MWd/t. This value must be positive.
XENON	keyword used to set nXe .
nXe	Xenon concentration in $10^{24} at/cm^3.$ This concentration will be applied to every bundle.
XEREF	keyword used to specify that the Xenon concentrations as computed with DRAGON will be taken. If this option is omitted and MAP contains bundle fluxes, new Xenon concentrations will be computed and used.
NEP	keyword used to set nNp .
nNp	Neptunium concentration in $10^{24} at/cm^3$.

XEREF	keyword used to specify that the Neptunium concentrations as computed with DRAGON will be taken. If this option is omitted and MAP contains bundle fluxes, new Neptunium concentrations will be computed and used.
SAM	keyword used to set nSm .
nSm	Samarium concentration in $10^{24} at/cm^3$. If this data is omitted, bundle concentrations as computed by DRAGON is used.
IMET	keyword used to set <i>imet</i> .
imet	interpolation type for time-average calculations. $imet = 1$: using Lagrange approximations; $imet = 2$: using spline approximations; $imet = 3$: using Hermite approximations (default value).
BLIN	keyword used to linear interpolation for burnup instead of the Lagrangian interpolation method.

Note: The concentration of boron is provided in terms of $10^{24}at/cm^3$ in the database. However, the usual units are ppm(wt) of Boron. Thus, the input asks for ppm of Boron (n_B) , and automatically transform the units into $10^{24}at/cm^3$ using the following equations:

$$\begin{array}{lll} \rho_B(g/cm^3) &=& n_B \cdot \rho_{\rm water}(g/cm^3) \\ & \text{and} \\ \rho_{\rm water}(at/cm^3) &=& 3\rho_{\rm water}(molecule/cm^3) = \frac{3.N}{M_{\rm water}}\rho_{\rm water}(g/cm^3) \\ & \rho_B(at/cm^3) &=& \rho_B(molecule/cm^3) = \frac{N}{M_B}\rho(g/cm^3) \\ & \text{thus} \\ & \rho_B(10^{24}at/cm^3) &=& n_B \cdot \frac{M_{\rm water}}{3.M_B}\rho_{\rm water}(10^{24}at/cm^3) \end{array}$$

where M molar mass and N the Avogadro number.

They are many options on how to use the module AFM: for its different purposes. A compact summary is presented on Tab. 63.

The Rozon correlation for fuel temperature as a function of bundle power is:

$$T_{\rm fuel} = T_{\rm cool} + 0.476 P + 2.267 P^2 \times 10^{-4}$$

where P is in kW and temperatures are in Kelvin.

Table 63: AFM options summary

-		
Option	Keywords	Parameter values
MCR	REFT	Nominal values
	$REFT + \{TFUEL, TCOOL,$	Nominal values except for specified parameters
	}	
TAB	REFT	Nominal values except for TFUEL parameter
		which is computed according to the Rozon cor-
		relation using nominal power
	$REFT + \{TFUEL, TCOOL,$	Same as above except for specified parameters
	}	which will have a constant value
MAP with local	REFT	Nominal values except for local parameters in-
parameters		cluded in MAP
	$REFT + \{TFUEL, TCOOL,$	Same as above except for specified parameters
	}	which will have a constant value
MAP without	REFT	Nominal values except for TFUEL parameter
local parame-		which is computed according to the Rozon cor-
ters		relation if power distribution is available
	$REFT + \{TFUEL, TCOOL,$	Same as above except for specified parameters
	}	which will have a constant value

4.5 The T16CPO: module

The WIMS-AECL Tape16 file is a FORTRAN sequential binary file which is used to transfer the results of a WIMS-AECL calculation to other applications.^[25] The explicit contents of this file may vary from application to application since the output of most records to this file is controlled by the user who can activate specific keywords in the WIMS-AECL input file.

The standard CPO data structure used by the code DONJON is generally generated by the cell code DRAGON. This data structure can be stored on a FORTRAN direct access binary file in the form of a hierarchical data base. There is also the possibility to keep the contents of this data structure in memory (with the same hierarchical structure) for faster access. The structure of the data base is in the form of a list of material directories which contain burnup sub-directories. Inside each of these burnup sub-directories the isotopic contents of a mixture is described and the multigroup cross sections associated with a specific isotope are stored in individual sub-directories. Note that in this database the macroscopic cross sections associated with a mixture are stored in a default isotopic sub-directory.

The interface between the Tape16 file and the CPO data structure should be written as a new module of the code DONJON in order to facilitate the access to the GANLIB utilities which manage the hierarchical data structures. This module will be called T16CPO:. The transfer of information from a Tape16 format file to a CPO data structure will require the following DONJON instructions:

The T16CPO: module specifications for creating or updating a CPO data structure from a Tape16 file are:

Table 64: Structure T16CPO:

DONCPO := T16CPO: [DONCPO] WIMS16 :: (desct16cpo) ;

where

DONCPO	name of data structure where the output CPO is stored. This can be a new data
	structure or an old data structure which will be updated.

- (desct16cpo) input specifications for the execution of the T16CPO: module.
- ; end of record keyword. This keyword is used to delimit the part of the input data stream associated the current module.

In the following dataset

```
MODULE T16CPO: ;
SEQ_BINARY WIMS16 ;
LINKED_LIST DONCPO ;
DONCPO := T16CPO: WIMS16 ::
...
```

means that that the module will read the sequential binary file WIMS16 file (in readonly mode) and create the CPO data structure DONCPO while the dataset

```
MODULE T16CPO: ;
SEQ_BINARY WIMS16 ;
LINKED_LIST DONCPO ;
```

```
DONCPO := T16CPO: DONCPO WIMS16 :: ... ;
```

means that the data structure DONCPO will be updated. The input instructions (replaced by ... here) should indicate what part of the information located on WIMS16 should be transferred to DONCPO and in what order.

4.5.1 Input data for the T16CPO: module

The input data structure (desct16cpo) will take the form:

Tabl	e 65:	Structure	(d	lesct16cpo)
------	-------	-----------	----	------------	---

```
[ EDIT iprint ]
[ NMIX nmixt ]
[ CONDG ngcond (igc(i) , i=1,ngcond ) ]
[ LIST ]
[ MIX [[ MIXNAM [ { CELLAV | REGION noreg } ]
[ MIX [[ MIXNAM [ { CELLAV | REGION noreg } ]
[ RC [ nburn ] frstrec ]
[ [ NAMPER valref npert (valper(i), frstrec(i) , i=1,npert ) ]]
[ MTMD [ valreft valrefd ] npert (valpert(i), valperd(i), frstrec(i) , i=1,npert ) ]
] ]]
```

where

EDIT	optional keyword used to modify the print level <i>iprint</i> .
iprint	index used to control the printing in this module. It must be set to 0 if no printing on the output file is required while values <10 will print general information about each record requested on Tape16 as well as other generic information pertinent to the T16CPO: module. Finally for values of <i>iprint</i> \geq 10, additional information required for debugging will be printed. The default value is <i>iprint</i> =1.
NMIX	optional keyword used to define the number of mixtures created on the CPO data structure.
nmixt	the maximum number of mixtures created. The default value is $nmixt=1$.
CONDG	optional keyword used to define the group structure for condensation. In the case where the CPO is to be updated, the information following CONDG must yield an energy group structure compatible with that already available on this data structure. If it is absent, the code will first try to use the CPO group structure (if available). Then, it will try to use the editing group structure corresponding to NGREAC on the following Tape16 record:
	REACTION LL, FLUX

Finally, if everything else fails, it will select the main transport group structure corresponding to NGMTR on the following Tape16 record:

	$WIMS_{UUUUUU}$, $CONSTANT_{UU}$, NEL
ngcond	the number of condensed groups required.
ilg	the last group number associated with each condensed group.
LIST	keyword to specify that the complete contents of $\tt Tape16$ must be listed on the output file.
MIX	keyword to specify that the remaining information will be associated with mixture properties definition.
MIXNAM	character*6 name of the mixture to create or update on the CPO.
CELLAV	optional keyword to specify that cell averaged data will be taken from Tape16. This is the default option.
REGION	optional keyword to specify that regional data will be taken from Tape16. The default option is CELLAV.
noreg	region number associated with this material in Tape16.
RC	optional keyword to specify that the cross section taken from Tape16 are at reference value. This information must be defined at least once for each mixture. It must also precede the definition of perturbation parameters.
nburn	number of consecutive burnup steps associated with mixture. The default value is <i>nburn</i> =1. We will assume that the same number of burnup steps is also available for the nuclear properties associated with the perturbed local parameters.
frstrec	first Tape16 record number associated with this mixture.
NAMPER	character*2 name of the perturbation. Each perturbation is associated with a single local parameter. The values permitted for <i>NAMPER</i> are the following:
	1. FT for fuel temperature
	2. MT for moderator temperature
	3. MD for moderator density
	4. MP for moderator purity
	5. MB for moderator boron
	6. C1 for coolant temperature
	8 CP for coolant purity
	9. RT for reflector temperature
	10. RD for reflector density
	11. RP for reflector purity
	Note that these keywords are identical to those used in the Proc16 program. ^[26] Here the moderator, coolant and reflector can be D_2O , H_2O or any other mixture since DONJON is not aware of the compositions of these mixtures. In the case where many different Tape16 files contains the reference and the individual perturbation effects, one must first define the reference case before updating the CPO using the Tape16 files containing the perturbations.

valref reference value of the associated local parameter.

npert	number of local parameter perturbations.
valper	perturbed values of the local parameter.
MTMD	character*4 name of perturbation associated with combine temperature and density changes effects. Note that this keyword is equivalent to the MTS keyword used in the Proc16 program. ^[26] In principle, any combined perturbations effects could be built from the catenation of two individual perturbations given in <i>NAMPER</i> .
valreft	reference temperature. This is required if either the \mathtt{MT} or the \mathtt{MD} perturbation is not defined.
valrefd	reference density. This is required if either the MT or the MD perturbation is not defined.
npert	number of simultaneous perturbations in moderator temperature and density.
valpert	perturbed values of the moderator temperature.
valperd	perturbed value of the moderator density.

The explicit name of the mixtures MIXDIR that will be stored on the main CPO directory will correspond to a catenation of MIXNAM and a perturbation name and an index *i* describing the perturbation order. It is created using the following FORTRAN instructions for the reference mixture:

WRITE(MIXDIR, '(A6,A6)') MIXNAM, 'RC

while for the i^{th} perturbed state associated with NAMPER(J) we will use:

```
WRITE(MIXDIR, '(A6, A2, A2, I2)') MIXNAM, NAMPER(J), 'uu', i
```

Finally, for the i^{th} perturbed state associated with the MTMD perturbation we will use:

```
WRITE(MIXDIR, '(A6,A4,I2)') MIXNAM, 'MTMD', i
```

Typically if the (desct16cpo) structure takes the form:

```
EDIT 0
NMIX 2
MIX
Candu RC 15 1
FT 900.0 2 1100.0 16 1300.0 46
Maple RC 70
RP 1.0 1 0.5 71
```

Then the first 15 cases stored on the Tape16 file will correspond to a reference CANDU fuel with burnup. The reference fuel temperature is 900.0 K. The next 15 cases are for a fuel temperature of 1100.0 K. Finally cases 46 to 60 are for a fuel temperature of 1300.0 K. The Maple mixture will have no burnup. The reference Maple cross sections correspond to case 70, while case 71 contains the effect on the Maple fuel mixture cross sections of a 50 % reduction in reflector purity. As a result we will end up with a CPO data structure which contains 5 mixtures called respectively

```
\begin{array}{l} {\rm Candu}_{\sqcup}{\rm RC}_{\sqcup\cup\sqcup\sqcup}\\ {\rm Candu}_{\sqcup}{\rm FT}_{\sqcup\sqcup\sqcup}\\ {\rm Candu}_{\sqcup}{\rm FT}_{\sqcup\sqcup\sqcup}\\ {\rm Maple}_{\sqcup}{\rm RC}_{\sqcup\sqcup\sqcup\sqcup}\\ {\rm Maple}_{\sqcup}{\rm RP}_{\sqcup\sqcup\sqcup}\\ 1\end{array}
```

The beginning of a new case on Tape16 will be identified by the presence of the record:

 $\texttt{CELLAV}_{{\scriptstyle\sqcup}{\scriptstyle\sqcup}{\scriptstyle\sqcup}{\scriptstyle\sqcup}}, \texttt{MODERATOR}$

in a Tape16 file. Accordingly, the keyword CELLAV should be used in the WIMS-AECL run creating this file. In addition, if the REGION option is used in the T16CPO: input data structure, then it should also be used in the WIMS-AECL run creating this file.

5 THERMAL-HYDRAULICS MODULES

5.1 The THM: module

The THM: module is a simplified thermal-hydraulics module where the reactor is represented as a collection of independent channels with no cross-flow between them. Each channel is represented using 1D convection equations along the channel and 1D cylindrical equations for a single pin cell. A two-fluid homogeneous model is used. The THM: module is built around *freesteam*, an open source implementation of IAPWS-IF97 steam tables for light water.^[28]. The THM: module works both in steady-state and in transient conditions and includes a subcooled flow boiling model based on the Jens & Lottes correlation ^[32] and on Bowring's model for two-phase homogeneous flows ^[33].

The 1D thermal-hydraulics equations are solved in each channel as a fonction of two fixed inlet conditions for the coolant velocity and temperature and one fixed outlet condition for the pressure. The THM: module specification is:

Table 66: Structure THM:

THERMO MAPFL := THM: [THERMO] MAPFL :: (descthm)

where

THERMO	character*12 name of the THERMO object that will be created or updated by the THM: module. Object THERMO contains thermal-hydraulics information set or computed by THM: in transient or in permanent conditions such as the distribution of the enthalpy, the pressure, the velocity, the density and the temperatures of the coolant for all the channels in the geometry. It also contains all the values of the fuel temperatures in transient or in permanent conditions according to the discretisation chosen for the fuel rods.
MAPFL	character*12 name of the MAP object containing fuel regions description and local parameter informations.
(descthm)	structure describing the input data to the THM: module.

5.1.1 Input data to the THM: module

Table 67: Structure (descthm)

EDIT iprint]RELAX relax]TIME caltype timestep timeiter time]FPUISS fract] [CRITFL cflux]

continued on next page

Structure (descthm)

ASSMB sass nbf nbg INLET poutlet tinlet RADIUS $r1 \ r2 \ r3 \ r4$

RODMESH nb1 nb2]

[[SET-PARAM PNAME pvalue]]

FORCEAVE $[\{ BOWR \mid SAHA \}]$ continued from last page

{ CWSECT sect flow | SPEED velocity } $\{ [POROS poros] [PUFR pufr] | [CONDF n cond (k cond(k), k=0, n cond) [INV inv ref] unit] \}$ [CONDC ncond (kcond(k),k=0,ncond) unit] [HGAP hgap] [HCONV hconv] [TEFF wteff] CONV maxit1 maxit2 maxit3 ermaxt ermaxc]

where

;

EDIT	keyword used to set <i>iprint</i> .
iprint	integer index used to control the printing on screen: $= 0$ for no print; $= 1$ for minimum printing; larger values produce increasing amounts of output.
RELAX	keyword used to set the relaxation parameter <i>relax</i> .
relax	relaxation parameter selected in the interval $0 < relax \leq 1$ and used to update the fuel (average and surface) temperature, coolant temperature and coolant density. The updated value is taken equal to $(1-relax)$ times the previous iteration value plus <i>relax</i> times the actual iteration value. The default value is <i>relax</i> = 1.
TIME	keyword used to specify the type of calculation (steady-state or transient) performed by the THM: module and the temporal parameters in case of a transient calculation. By default, a steady-state calculation is performed.
caltype	integer value set to control the type of calculation that will be performed by the THM: module: =0 for steady-state; =1 for transient. The default value is 0.
timestep	real value set to the time step in case of a transient calculation. The default value is $0.0.$
timeiter	integer value of the current time step index, used for transient calculations. The default value is $0.$
time	real value of time in second, used for transient calculations. The default value is 0.0.
FPUISS	keyword used to specify the fraction of the power released in fuel. The remaining fraction is assumed to be released in coolant. The default value is 0.974.
fract	real value set to the fraction (f) . Power densities released in coolant and fuel are computed as
	$Q_{\text{cool}} = (1 - f) \frac{V_{\text{cool}} + V_{\text{fuel}}}{V_{\text{cool}}} \frac{P_{\text{mesh}}}{V_{\text{mesh}}}$ $Q_{\text{fuel}} = f \frac{V_{\text{cool}} + V_{\text{fuel}}}{V_{\text{fuel}}} \frac{P_{\text{mesh}}}{V_{\text{mesh}}}$

	where V_{cool} and V_{fuel} are coolant and fuel area computed from sass, nbf , nbg , $r3$ and $r4$. The mesh power P_{mesh} and volume V_{mesh} are recovered from $MAPFL$ object.
CRITFL	keyword used to specify the critical heat flux.
cflux	real value set to the critical heat flux in W/m ² . The default value is 2.0×10^6 W/m ² .
CWSECT	keyword used to specify the core coolant section and the coolant inlet flow.
sect	real value set to the core coolant section in m^2 .
flow	real value set to the coolant flow in m^3/hr . This value doesn't include the by-pass flow. The inlet coolant velocity in m/s is computed as
	$V = \frac{flow}{3600 \ cwsect}.$
SPEED	$V = \frac{flow}{3600\ cwsect}.$ keyword used to specify the inlet coolant velocity.
SPEED velocity	$V = \frac{flow}{3600\ cwsect}.$ keyword used to specify the inlet coolant velocity. real value set to the inlet coolant velocity in m/s.
SPEED velocity ASSMB	$V = \frac{flow}{3600\ cwsect}.$ keyword used to specify the inlet coolant velocity. real value set to the inlet coolant velocity in m/s. keyword used to specify the assembly characteristics.
SPEED velocity ASSMB sass	$V = \frac{flow}{3600\ cwsect}.$ keyword used to specify the inlet coolant velocity. real value set to the inlet coolant velocity in m/s. keyword used to specify the assembly characteristics. real value set to the assembly surface in m ² . This value is equal to the square of an assembly side (including the water gap).

nbg integer value set to the number of active guide tubes in a single assembly.

INLET keyword used to specify the outlet pressure and inlet absolute temperature.

poutlet real value set to the outlet coolant pressure in Pa. The pressure along each channel is assumed to be constant and equal to *poutlet* in permanent conditions.

tinlet real value set to the inlet coolant absolute temperature in K.

- RADIUS keyword used to set the pin-cell radii.
- r1 real value set to the fuel pellet radius in m.
- r2 real value set to the internal clad rod radius in m.
- r3 real value set to the external clad rod radius in m.
- r4 real value set to the guide tube radius in m.
- **POROS** keyword used to set the oxyde porosity of fuel. Porosity affects some built-in correlations used to represent the heat conduction phenomenon in fuel.
- poros real value set to the oxyde porosity. The default value is 0.05.
- PUFR keyword used to set the plutonium mass enrichment of fuel. Plutonium enrichment affects some built-in correlations used to represent the heat conduction phenomenon in fuel.

pufr real value set to the plutonium mass enrichment. The default value is 0.0.

CONDF

keyword used to set the fuel thermal conductivity as a function of local fuel temperature T_{fuel} . Fuel conductivity is computed as

$$\lambda_{fuel} = \sum_{k=0}^{ncond} kcond(k) * (T_{fuel})^k + \frac{inv}{T_{fuel} - red}$$

with λ_{fuel} in W/m/K and T_{fuel} in the selected unit (Kelvin or Celsius).

By default, built-in models are used, taking into account oxyde porosity and plutonium mass enrichment. Note that oxyde porosity and plutonium mass enrichment are ignored if this keyword is used.

- *ncond* integer value set to the degree of the conductivity polynomial.
- kcond real value set to the coefficient of the conductivity polynomial. ncond + 1 coefficients are expected.
- unit string value set to the unit of temperature T in the conductivity function. Can be either CELSIUS or KELVIN.
- INV keyword used to add an inverse term in the fuel conductivity function.
- *inv* real value set to the coefficient in the inverse term of fuel conductivity. The default value is 0.0 (i.e. no inverse term).
- ref real value set to the reference in the inverse term of fuel conductivity.
- CONDC keyword used to set the clad thermal conductivity as a function of local clad temperature T_{clad} . Clad conductivity is computed with the following polynomial

$$\lambda_{clad} = \sum_{k=0}^{n cond} k cond(k) * (T_{clad})^k$$

with λ_{clad} in W/m/K and T_{clad} in the selected unit (Kelvin or Celsius). By default, a built-in model is used.

- HGAP keyword used to set the heat exchange coefficient of the gap as a constant. By default, a built-in model is used.
- hgap real value set to the constant heat exchange coefficient of the gap in $W/m^2/K$.
- HCONV keyword used to set the heat transfer coefficient between clad and fluid as a constant. By default, this coefficient is computed using a built-in correlation.
- hconv real value set to the constant heat transfer coefficient between clad and fluid in $W/m^2/K$.
- TEFF keyword used to set the weighting factor in the effective fuel temperature approximation. The effective fuel temperature is used for the cross sections interpolations on fuel temperature.

wteff real value W_{teff} set to the weighting factor in the effective fuel temperature. The effective fuel temperature is computed as

$$T_{\text{eff}}^{\text{fuel}} = W_{\text{teff}} * T_{\text{surface}}^{\text{fuel}} + (1 - W_{\text{teff}}) * T_{\text{center}}^{\text{fuel}}$$

where $0 \leq W_{\text{teff}} \leq 1$, $T_{\text{surface}}^{\text{fuel}}$ is the temperature at the surface of the fuel pellet (K), and $T_{\text{center}}^{\text{fuel}}$ is the temperature at the center of the fuel pellet (K).

By default, the Rowlands weighting factor $W_{\text{teff}} = \frac{5}{9}$ is used^[35].

CONV	keyword used to set the convergence criteria for solving the conduction and the con- servation equation.
maxit1	integer value set to the maximum number of iterations for computing the conduction integral. The default value is 50.
maxit2	integer value set to the maximum number of iterations for computing the center pellet temperature. The default value is 50.
maxit3	integer value set to the maximum number of iterations for computing the coolant parameters (mass flux, pressure, enthalpy and density) in case of a transient calculation. The default value is 50.
ermaxt	real value set to the maximum temperature error in K. The default value is 1 K.
ermaxc	real value set to the maximum relative error for parameters given by the resolution of flow conservation equations (pressure, velocity and enthalpy). The default value is 10^{-3} .
RODMESH	keyword used to set the radial discretization of pin-cells.
nb1	integer value set to the number of discretisation points in fuel. The default value is 5.
nb2	integer value set to the number of discretisation points in the whole pin-cell (fuel+cladding). The default value is 8.
FORCEAVE	keyword used to force the use of the average approximation during the fuel conductivity evaluation. By default, a rectangle quadrature approximation is used.
BOWR	keyword used to set a subcooling model based on the Jens & Lottes correlation ^[32] with the Bowring model ^[33] (default option).
SAHA	keyword used to set a subcooling model based on the Saha-Zuber correlation ^[34] . This option is recommended for BWR applications.
SET-PARAM	keyword used to indicate the input (or modification) of the actual values for a parameter specified using its $PNAME$.
PNAME	keyword used to specify <i>PNAME</i> .
PNAME	character*12 name of a parameter.
pvalue	single real value containing the actual parameter's values. Note that this value will not be checked for consistency by the module. It is the user responsibility to provide the valid parameter's value which should be consistent with those recorded in the multicompo or Saphyb database.

6 OPTIMIZATION MODULES

This section is related to optimization capabilities available in Donjon and based on generalized perturbation theory.^[29, 30] General information about the generalized perturbation theory can be found in Sect. 5.3 of Ref. 1.

6.1 The DLEAK: module

The DLEAK: module is used to create a delta MACROLIB (type L_MACROLIB) with respect to leakage information. Derivatives of leakage-related information (recovered from the input MACROLIB) are stored in the STEP heteroneneous list components present in the output MACROLIB. Derivatives can be taken with respect to a leakage parameter itself $(D_{g,i} \text{ or } \Sigma_{1,g,i})$ or relative to factor μ in $\mu D_{g,i}$ or $\mu \Sigma_{1,g,i}$. Note that factor μ is not a SPH factor because it multiplies only leakage-related parameters. One component of the STEP heteroneneous list is created for each value of energy group g and for each value of mixture i.

The calling specifications are:

Table 68: Structure (DLEAK:)

DMACRO OPTIM := DLEAK: MACRO :: (dleak_data)

where

- DMACRO character*12 name of a LCM object (type L_MACROLIB) containing the delta MACROLIB information. DMACRO is created by the module. A STEP heteroneneous list is present in DMACRO.
- OPTIM character*12 name of a second LCM object (type L_OPTIMIZE) created by the module. Leakage-related parameters are saved in the the control variable record 'VAR-VALUE' of OPTIM object. Input data defined in Sect. 6.1.1 is also saved in OPTIM object.
- MACRO character*12 name of the LCM object (type L_MACROLIB) containing the input MACROLIB.

(dleak_data) structure containing the data to module DLEAK: (see Sect. 6.1.1).

6.1.1 Data input for module DLEAK:

Table 69: Structure (dleak_data)

```
[ EDIT iprint ]
TYPE { DIFF | NTOT1 }
DELTA { VALUE | FACTOR }
[ MIXMIN ibm1 ] [ MIXMAX ibm2 ]
[ GRPMIN ngr1 ] [ GRPMAX ngr2 ]
;
```

where		
EDIT	keyword used to set <i>iprint</i> .	
iprint	index used to control the printing in module DLEAK:.	
TYPE	keyword used to set the leakage parameter that is differentiated.	
DIFF	differentiation with respect to diffusion coefficients.	
NTOT1	differentiation with respect to P_1 -weighted macroscopic total cross sections.	
DELTA	keyword used to set the type of differentiation.	
VALUE	differentiation with respect to the leakage parameter itself.	
FACTOR	differentiation with respect to the correction factor μ .	
MIXMIN	keyword used to set the first mixture where leakage parameters are differentiated. By default, the first mixture index is used.	7
ibm1	minimum mixture index where leakage parameters are differentiated.	
MIXMAX	keyword used to set the last mixture where leakage parameters are differentiated. By default, the total number of mixtures in $MACRO$ is used.	7
ibm2	maximum mixture index where leakage parameters are differentiated.	
GRPMIN	keyword used to set the first energy group where leakage parameters are differentiated. By default, the first energy group index is used.	7
ngr1	minimum energy group index where leakage parameters are differentiated.	
GRPMAX	keyword used to set the last energy group where leakage parameters are differentiated. By default, the total number of energy groups in $MACRO$ is used.	7
ngr2	maximum energy group index where leakage parameters are differentiated.	

6.2 The GRAD: module

The GRAD: module is designed to perform the following tasks:

- compute the gradients of the system characteristics using solutions of direct or adjoint fixed source eigenvalue problems. Here, we assume an optimization problem with *nvar* control variables and with *ncst* constraints. The total number of system characteristics is therefore equal to ncst+1.
- define options and parameters for the different method to solve the optimization problem. The nonlinear optimization problem can be solved as a converging sequence of linear optimization problems with a quadratic constraint of the form

$$\sum_{i=1}^{nvar} \omega_i \left(\Delta x_i^{(n)} \right)^2 \le \left(S^{(n)} \right)^2$$

where ω_i is a weight defined after keyword CST-WEIGHT and $\Delta x_i^{(n)}$ is a displacement for *i*-th control variable at iteration (*n*). The initial value of radius $S^{(1)}$ is defined after keyword OUT-STEP-LIM.

• reduces the radius $S^{(n)}$ of the quadratic constraint.

The calling specifications are:

Table 70: Structure GRAD:

OPTIM := GRAD: [OPTIM] DFLUX GPT :: (grad_data)

where

OPTIM	$character*12$ name of the OPTIMIZE object (L_OPTIMIZE signature) containing the optimization informations. Object <i>OPTIM</i> must appear on the RHS to be able to updated the previous values.
DFLUX	<pre>character*12 name of the FLUX object (L_FLUX signature) containing a set of solutions of fixed-source eigenvalue problems.</pre>
GPT	$\tt character*12$ name of the GPT object (L_GPT signature) containing a set of direct or adjoint sources.
(grad_data)	structure containing the data to the module $GRAD$: (see Sect. 6.2.1).

6.2.1 Data input for module GRAD:

Table 71: Structure grad_data

[EDIT iprint]

continued on next page
```
 \begin{bmatrix} \mathsf{METHOD} \{ \mathsf{SIMPLEX} \mid \mathsf{LEMKE} \mid \mathsf{MAP} \mid \mathsf{AUG-LAGRANG} \mid \mathsf{PENAL-METH} \} \end{bmatrix} \\ \begin{bmatrix} \mathsf{OUT-STEP-LIM} \ sr \end{bmatrix} \\ \begin{bmatrix} \mathsf{OUT-STEP-EPS} \ \epsilon_{ext} \end{bmatrix} \begin{bmatrix} \mathsf{INN-STEP-EPS} \ \epsilon_{inn} \end{bmatrix} \\ \begin{bmatrix} \mathsf{CST-QUAD-EPS} \ \epsilon_{quad} \end{bmatrix} \\ \begin{bmatrix} \mathsf{CST-QUAD-EPS} \ \epsilon_{quad} \end{bmatrix} \\ \begin{bmatrix} \mathsf{MAXIMIZE} \mid \mathsf{MINIMIZE} \} \end{bmatrix} \\ \begin{bmatrix} \mathsf{STEP-REDUCT} \{ \mathsf{HALF} \mid \mathsf{PARABOLIC} \} \end{bmatrix} \\ \begin{bmatrix} \mathsf{VAR-VALUE} \ ( \ control(i), \ i=1, nvar ) \end{bmatrix} \begin{bmatrix} \mathsf{VAR-WEIGHT} \ ( \ weight(i), \ i=1, nvar ) \end{bmatrix} \\ \begin{bmatrix} \mathsf{VAR-VAL-MIN} \{ \ ( \ vecmin(i), \ i=1, nvar ) \mid \mathsf{ALL} \ varmin \end{bmatrix} \\ \begin{bmatrix} \mathsf{VAR-VAL-MAX} \{ \ ( \ vecmax(i), \ i=1, nvar ) \mid \mathsf{ALL} \ varmax \end{bmatrix} \\ \\ \begin{bmatrix} \mathsf{FOBJ-CST-VAL} \ ( \ funct(i), \ i=1, ncst+1 ) \end{bmatrix} \\ \\ \begin{bmatrix} \mathsf{CST-TYPE} \ ( \ type(i), \ i=1, ncst ) \end{bmatrix} \begin{bmatrix} \mathsf{CST-OBJ} \ ( \ cstval(i), \ i=1, ncst ) \end{bmatrix} \\ \\ \end{bmatrix} \\ \\ \end{bmatrix} \\ \\ \end{bmatrix}
```

where

EDIT	keyword used to set <i>iprint</i> .
iprint	index used to control the printing in module.
METHOD	keyword used to define the quasi-linear programming method. Note: If the general Lemke method is used, the quadratic constraint must be active. The strategy consists to proceed in two steps:
	• At first step, the linear programming problem (i. e., without the quadratic con- traint) is solved and the control-variable displacement is computed. If this dis- placement is less than the radius of the quadratic constraint, the step one solution is accepted and step two is not performed. If this displacement is greater than the radius of the quadratic constraint, the step one solution is rejected and step two is performed. Step one can be solved with the SIMPLEX method or with the linear LEMKE method.
	• At step two, the general LEMKE method is used to find the correct solution. The general Lemke method is based on a parametric linear complementarity principle, as explained in Ref. 31.
SIMPLEX	keyword used to specify that the SIMPLEX method will be used at step one and the general LEMKE method at step two.
LEMKE	keyword used to specify that the linear LEMKE method will be used at step one and the general LEMKE method at step two.
MAP	keyword used to specify that the MAP method will be used. The quadratic constraint is linearized and a converging sequence of SIMPLEX calculations is performed.
AUG-LAGRANG	keyword used to specify that the augmented Lagrangian method will be used.
PENAL-METH	keyword used to specify that the penalty method will be used.
OUT-STEP-LIM	keyword used to set the initial radius of the quadratic constraint (default value is $sr = 1.0$).
sr	initial radius of the quadratic constraint (real).

OUT-STEP-EPS	keyword used to set the tolerance of outer iteration convergence inside module $\mathtt{PLQ:}$.
ϵ_{ext}	tolerance value (real).
INN-STEP-EPS	keyword used to set the tolerance used within the SIMPLEX or LEMKE method.
ϵ_{inn}	tolerance value (real).
CST-QUAD-EPS	keyword to set the convergence parameter $epsilon4$ for the radius of the quadratic constraint inside module <code>GRAD:</code> .
ϵ_{quad}	tolerance for convergence of the radius of the quadratic constraint (real).
MAXIMIZE	keyword used to specify that the optimization problem will be a maximization.
MINIMIZE	keyword used to specify that the optimization problem will be a minimization (default).
STEP-REDUCT	keyword used to define the method of the reduction of the outer step.
HALF	keyword used to specify that the step will be reduced by a factor of 2.
PARABOLIC	keyword used to specify that the step will be reduced with the parabolic method.
VAR-VALUE	keyword to specify the values of the control variables. These values can also be set in a previous call to module GRAD: or set in another module.
control	array containing <i>nvar</i> real values.
VAR-WEIGHT	keyword to specify the values of the control variable weights in the quadratic constraint. All weights are set to 1.0 by default.
weight	array containing <i>nvar</i> real values.
VAR-VAL-MIN	keyword to specify the minimum values of the control variables. These values can also be set in a previous call to module \texttt{GRAD} :.
vecmin	array containing <i>nvar</i> real values.
varmin	single real value used for all control variables.
VAR-VAL-MAX	keyword to specify the maximum values of the control variables. These values can also be set in a previous call to module GRAD:.
vecmax	array containing <i>nvar</i> real values.
varmax	single real value used for all control variables.
FOBJ-CST-VAL	keyword to specify the value of the objective function followed by the actual values of the constraints. These values can also be set in a previous call to module GRAD: or set in another module.
funct	array containing $ncst+1$ real values.
CST-TYPE	keyword to specify the relation types of the constraints. These values can also be set in a previous call to module GRAD:.
type	array containing <i>ncst</i> integer values. These values are: $= -1$ for \geq , $= 0$ for equalily and $= 1$ for \leq .
CST-OBJ	keyword to specify the RHS values of the constraints. These values can also be set in a previous call to module GRAD:.

cstval array containing *ncst* real values.

- CST-WEIGHT keyword to specify the weights (or penalties) of the constraints. These weights are not used with Lemke or MAP methods. These values can also be set in a previous call to module GRAD:.
- cstw array containing ncst real values.

6.3 The PLQ: module

The PLQ: module is used to solve the linear programming problem with a quadratic constraint. The gradients of the system characteristics are calculated with module GRAD:. The options and parameters for the different method to solve the optimization problem are also defined in module GRAD:.

The calling specifications are:

Table 72: Structure PLQ:

OPTIM := PLQ:	[OPTIM]	::	(plq_data)
---------------	-----------	----	------------

where

OPTIM	character*12 name of the OPTIMIZE object (L_OPTIMIZE signature) containing the optimization informations. Object <i>OPTIM</i> must appear on the RHS to be able to updated the previous values.
(plq_data)	structure containing the data to the module PLQ: (see Sect. 6.3.1).

6.3.1 Data input for module PLQ:

Table 73: Structure plq_data

[EDIT <i>iprint</i>]
[WARNING-ONLY]
CALCUL-DX [NO-STORE-OLD]
[COST-EXTRAP >> ecost <<]
$[\text{CONV-TEST} >> l_{conv} <<]$
:

where

EDIT	keyword used to set <i>iprint</i> .
iprint	index used to control the printing in module.
WARNING-ONLY	keyword used to specify that only a warning will be used when no valid previous decision vectors can be recall in case of error of the mathematical programming.
CALCUL-DX	keyword used to specify that the new step will be calculated.
NO-STORE-OLD	keyword used to specify that the old value of decision variables and gradients will not be stored in the L_OPTIMIZE/'OLD-VALUE' directory.
COST-EXTRAP	keyword used to calculate the extrapolated objective constant <i>ecost</i> .

ecost extrapolated objective constant.

CONV-TEST keyword used to calculate if the external convergence has been reached.

 l_{conv} = 1 means that external convergence has been reached; = 0 otherwise.

7 DONJON DATA STRUCTURES

A brief description of each DRAGON, DONJON and TRIVAC data structures, which can be used with DONJON code, is given in Section 2.2. In this section, a detailed description of the DONJON data structures is presented.

7.1 Contents of /fmap/ data structure

A /fmap/ data structure is used to store fuel assembly (or bundle) map and fuel information such as powers, average fluxes, control zones, burnup or refueling scheme. The fuel bundle location are given in an embedded sub-directory which contains the records as a /geometry/ data structure. This object has a signature L_MAP; it is created using the RESINI: module.

7.1.1 The state-vector content

The dimensioning parameters S_i , which are stored in the state vector for this data structure, represent:

- The number of fuel bundles per channel $N_b = S_1$
- The number of fuel channels $N_{\rm ch} = S_2$
- The number of combustion zones $N_{\text{comb}} = S_3$
- The number of energy groups $N_{\rm gr} = \mathcal{S}_4$
- The type of interpolation with respect to burnup $I_{\text{btyp}} = S_5$

 $I_{\rm btyp} = \begin{cases} 0 & \text{interpolation type is not provided} \\ 1 & \text{according to the time-average model} \\ 2 & \text{according to the instantaneous model} \end{cases}$

- The number of bundle shift. $N_{\text{sht}} = S_6$
- The number of fuel types $N_{\text{fuel}} = S_7$
- The number of recorded parameters $N_{\text{parm}} = S_8$
- The total number of fuel bundles $N_{\text{tot}} = S_9$
- The number of voided reactor channels $N_{\text{void}} = S_{10}$
- The option with respect to the core-voiding pattern $I_{\text{void}} = S_{11}$
 - $I_{\rm void} = \begin{cases} 0 & {\rm voiding \ pattern \ not \ provided} \\ 1 & {\rm full-core \ voiding \ pattern} \\ 2 & {\rm half-core \ voiding \ pattern} \\ 3 & {\rm quarter-core \ voiding \ pattern} \\ 4 & {\rm checkerboard-full \ voiding \ pattern} \\ 5 & {\rm checkerboard-half \ voiding \ pattern} \\ 6 & {\rm checkerboard-quarter \ voiding \ pattern} \\ 7 & {\rm user-defined \ voiding \ pattern} \end{cases}$

• The type of the geometry $F_t = S_{12}$

$$F_t = \begin{cases} 7 & \text{Cartesian 3-D geometry} \\ 9 & \text{Hexagonal 3-D geometry} \end{cases}$$

• The naval-coordinate layout used by the SIM: module $I_{sim} = S_{13}$.

The number of assemblies along X and Y axis are given using

$$L_{\rm x} = \frac{I_{\rm sim}}{100}$$
 and $L_{\rm y} = {\rm mod}(I_{\rm sim}, 100)$

7.1.2 The main /fmap/ directory

The following records and sub-directories will be found on the first level of /fmap/ directory:

Name	Туре	Condition	Units	Comment
SIGNATURE	C*12			Signature of the /fmap/ data structure
STATE-VECTOR	I(40)			Vector describing the various parameters as- sociated with this data structure S_{i}
FLMIX	$\mathrm{I}(N_{\mathrm{ch}},N_b)$			Fuel mixture indices per bundle or assembly subdivisions for each reactor channel
FLMIX-INIuuu	$I(N_{ch}, N_b)$	$I_{\rm sim} \neq 0$		Fuel mixture indices per bundle or assembly subdivisions for each reactor channel, as de- fined by user in PESINI : module
S-ZONE	$C(N_{ch}) * 4$	$I_{\rm sim} \neq 0$		identification name corresponding to the basic naval-coordinate position of an assembly, as
BMIX	$I(N_x, N_y, N_z)$			Renumbered mixture indices per each fuel re- gion over the fuel-map geometry; for the non- fuel regions these indices are set to 0
XNAME	$\mathcal{C}(N_x) * 4$			Channel identification names with respect to their horizontal position
YNAME	$\mathcal{C}(N_y) * 4$			Channel identification names with respect to their vertical position.
B-ZONE	$I(N_{ch})$	$N_{\rm comb} \ge 1$		Combustion-zone indices per channel.
BURN-AVG	$\mathrm{R}(N_{\mathrm{comb}})$		MW d t	⁻¹ Average exit burnups per combustion zone.
BURN-INST	$\mathrm{R}(N_{\mathrm{ch}}, N_b)$	$I_{\rm btyp} = 2$	MW d t	⁻¹ Instantaneous burnups per bundle or assembly subdivisions for each channel.
BURN-BEG	$\mathrm{R}(N_{\mathrm{ch}},N_b)$	$I_{\rm btyp} = 1$	MW d t	⁻¹ Low burnup integration limits according to
BURN-END	$\mathrm{R}(N_{\mathrm{ch}},N_b)$	$I_{\rm btyp} = 1$	MW d t	⁻¹ Upper burnup integration limits according to the time-average model.

Table 74: Records and sub-directories in /fmap/ data structure

Records and sub-directories in /fmap/ data structure

Name	Type	Condition	Units	Comment
BUND-PWuuuuu	$\mathrm{R}(N_{\mathrm{ch}},N_b)$	*	kW	Bundle-powers set in RESINI : module or re-
$BUND-PW-INI_{\sqcup}$	$\mathbf{R}(N_{\mathrm{ch}},N_b)$	*	kW	Beginning-of-transient bundle-powers recov- ered from L POWER object
FLUX-AV	$\mathrm{R}(N_{\mathrm{ch}}, N_b, N_{\mathrm{gr}})$	*	$\mathrm{cm}^{-2} \mathrm{s}^{-1}$	The normalized average fluxes recorded per each fuel bundle and for each energy group, recovered from L POWER object.
B-EXIT REF-SHIFT	R(1) I(N _{comb})		MW d t ⁻	¹ Core-average discharge burnup. Bundle-shifts per combustion zone. A bundle- shift corresponds to the number of displaced fuel bundles during the refueling operation.
REF-VECTOR	${f I}(N_{ m comb},N_b) \ {f I}(N_{ m ch})$			Refueling pattern vector per combustion zone. Refueling scheme of each channel; it corre- sponds to the positive or negative bundle-shift number according to the flow direction.
REF-RATE	${ m R}(N_{ m ch}) \ { m R}(N_{ m ch})$		$\begin{array}{c} \mathrm{kg} \ \mathrm{d}^{-1} \\ \mathrm{d} \end{array}$	Channel refueling rates. Time values at which channels are refueled in- side a refueling time period
$\begin{array}{l} \text{DEPL-TIME}_{\sqcup \sqcup \sqcup} \\ \{pshift\} \\ \{bshift\} \end{array}$	$ \begin{aligned} & \mathbf{R}(1) \\ & \mathbf{R}(N_{\mathrm{ch}}, N_b) \\ & \mathbf{R}(N_{\mathrm{ch}}, N_b) \end{aligned} $	$\begin{array}{l} N_{\rm sht} \geq 1 \\ N_{\rm sht} \geq 1 \end{array}$	$d \\ kW \\ MWdT^-$	Refueling time period: Refueling time period in days. The power of the bundles shifted the <i>i</i> -th time. ¹ The burnup of the bundles shifted the <i>i</i> -th time.
$\{ishift\}$	$\mathrm{I}(N_{\mathrm{ch}},N_b)$	$N_{\rm sht} \geq 1$		The number of shifts per bundle during refu- eling.
AX-SHAPE	$\mathrm{R}(N_{\mathrm{ch}},N_b)$	$I_{\rm btyp} = 1$		Normalized axial power-shape values over the fuel bundles. Equal to fuel-bundle powers di- vided by channel powers
EPS-AX	R(1)	$I_{\rm btyp} = 1$		Convergence factor for the axial power-shape calculation; it is defined as a relative error be- tween the two successives calculations
GEOMAP	Dir			Sub-directory containing the embedded $3D$ -Cartesian /geometry/ of the fuel lattice.
FUEL	$\operatorname{Dir}(N_{\mathrm{fuel}})$			List of fuel-type sub-directories. Each com- ponent of the list is a directory containing the
{hcycle}	$\operatorname{Dir}(N_{\mathrm{burn}})$	$I_{\rm sim} \neq 0$		Sub-directory containing information related to a fuel cycle in a PWR. N_{burn} is the number of burnup steps used during the simulation of the cycle. These burnup steps may not be of increasing values
PARAM	$\operatorname{Dir}(N_{\operatorname{parm}})$	$N_{\rm parm} > 0$		List of parameter-type sub-directories. Each component of the list is a directory containing the information relative to a single parameter. The total number of sub-directories corresponds to the total number of recorded parameters N_{parm} (excluding burnups).

The contents of the GEOMAP sub-directory correspond to the typical contents of the /geometry/ data structure. The dimensioning parameters N_x , N_y , and N_z represent the number of volumes along the corresponding axis in the fuel-map geometry.

The shifting information records {pshift}, {bshift} and {ishift} will be composed using the following FORTRAN instructions, respectively, as

WRITE(pshift,'(A6,I2)') 'PSHIFT', ell WRITE(bshift,'(A6,I2)') 'BSHIFT', ell WRITE(ishift,'(A6,I2)') 'ISHIFT', ell

for $1 \leq ell \leq N_{\text{sht}}$.

Each time a bundle is shifted and stay in the reactor, its burnup and power will be saved in the records $\{bshift\}$ and $\{pshift\}$. For example, $\{bshift i\}$ and $\{pshift i\}$ will contain all the burnups and powers of bundles that have been shifted *i*-th time.

7.1.3 The FUEL sub-directories

Each FUEL sub-directory contains the information corresponding to a single fuel type. Inside each sub-directory, the following records will be found:

Name	Type	Condition	Units	Comment
MIX TOT UUUUUUUUU MIX-VOID UUUUUU WEIGHT UUUUUUU POISON	I(1) I(1) I(1) R(1) R(1) R(1)		kg wt%	Fuel-type mixture number. Total number of fuel bundles for this fuel type. Voided-cell mixture number for this fuel type. Fuel weight in a bundle for this fuel type. Fuel enrichment for this fuel type. Poison load for this fuel type.

Table 75: Records in FUEL sub-directories

7.1.4 The {hcycle} sub-directories

Each {hcycle} sub-directory contains the information corresponding to a single PWR fuel cycle. Inside each sub-directory, the following records will be found:

Name	Type	Condition	Units	Comment
TIME	R(1)		d	Depletion time corresponding to instanta- neous burnup values.
BURNAVG	R(1)		$MW d t^{-1}$	Average burnup of the assembly.
NAME	$C(N_{ch}) * 12$			Names of each assembly or of each quart-of assembly during a refuelling cycle. All quart- of-assembly belonging to the same assembly have the same name.
FLMIX	$I(N_{\rm ch}, N_b)$			Fuel mixture indices per assembly subdivi- sions for each reactor channel.
$BURN-INST_{\cup\cup\cup}$	$\mathbf{R}(N_{\mathrm{ch}},N_b)$		$MW d t^{-1}$	Instantaneous burnups per assembly subdivi- sions for each channel.
POWER-BUND	$R(N_{ch}, N_b)$		kW	Powers per assembly subdivisions for each channel.

Table 76: Records in {hcycle} sub-directories

7.1.5 The PARAM sub-directories

Each PARAM sub-directory contains the information corresponding to a single local or global parameter (excluding burnups). Inside a such sub-directory, the following records will be found:

Name	Type	Condition	Units	Comment	
Ρ-ΝΑΜΕ	C*12			Unique id ter. This recommen values: C-BORE T-FUEL T-SURF	lentification name of this parame- name is user-defined; however, it is ided to use the following pre-defined Boron concentration Averaged fuel temperature Surfacic fuel temperature
				T-COOL	Averaged coolant temperature
				CANDU	-only parameters:
				T-MODE	Averaged moderator temperature
PARKEY	C*12			Correspon recorded i	Averaged moderator density adding name of this parameter as n a multi-parameter Compo file.

Table 77: Records in PARAM sub-directories

Records in PARAM sub-directories

continued from last page

Name	Туре	Condition	Units	Comment
Ρ-ΤΥΡΕυμμμμ	I(1)			Number associated to the type of recorded parameter: $ptype = 1$ for global parameter;
P-VALUE	$\begin{array}{l} {\rm R}(1) \\ {\rm R}(N_{\rm ch}, N_b) \end{array}$	ptype = 1 $ptype = 2$		ptype = 2 for local parameter. Recorded single value for global parameter. Recorded values for local parameter per each fuel bundle for every channel.

7.2 Contents of /matex/ data structure

A /matex/ data structure is used to store several information related to the reactor extended material index and geometry. This object has a signature L_MATEX; it is created using the USPLIT: module. The information contained in this data structure can be used and updated in other DONJON modules.

7.2.1 The state-vector content

The dimensioning parameters S_i , which are stored in the state vector for this data structure, represent:

- The number of energy groups $N_{gr} = S_1$
- The maximum number of material mixtures $N_m = S_2$ (N_m equals to the total number of material regions plus the number of device mixtures)
- The number of reflector types $N_r = S_3$
- The number of fuel types $N_f = S_4$
- The total number of mixtures indices $N_{tot} = S_5$ (N_{tot} equals to the total number of mesh-splitted volumes plus the number of device mixtures)
- The type of reactor geometry $I_g = S_6$ (only $I_g = 7$ for 3D-Cartesian geometry or $I_g = 9$ for 3D-Hexagonal geometry are allowed)
- The total number of mesh-splitted volumes $N_{el} = S_7$
- The number of mesh-splitted volumes along x-axis $L_x = S_8$
- The number of mesh-splitted volumes along y-axis $L_y = S_9$
- The number of mesh-splitted volumes along z-axis $L_z = S_{10}$

7.2.2 The /matex/ directory

The following records will be found on the /matex/ directory:

Name	Туре	Condition	Units	Comment
$SIGNATURE_{\cup\cup\cup}$	C*12			Signature of the /matex/ data structure (SIGNA = I. MATEX).
STATE-VECTOR	I(40)			Vector describing the various parameters as- sociated with this data structure S_i
RMIX	$I(N_r)$			The reflector-type mixture indices, as defined in the reactor geometry.
RTOT	$I(N_r)$			The total number of reflector regions per each reflector type
FMIX	$I(N_f)$			The fuel-type mixture indices, as defined in the reactor geometry
FTOTUUUUUUU	$I(N_f)$			The total number of fuel regions per each fuel two
MATUUUUUUUU	$I(N_{tot})$			The material mixture indices per each region and including the device mixtures. The fuel- type indices are set negative; the device in- dices are appended at the end of vector; the virtual-region indices are set to 0
INDEX	$I(N_{el})$			The renumbered mixture indices. A unique number is associated with each mesh-splitted volume. The device indices are not included; the virtual-region indices are set to 0
MESHX	$\mathbf{R}(L_x+1)$			The mesh-splitted coordinates along x-axis of the reactor geometry.
MESHY	$\mathcal{R}(L_y+1)$			The mesh-splitted coordinates along y-axis of the reactor geometry.
MESHZ	$\mathcal{R}(L_z+1)$			The mesh-splitted coordinates along z-axis of the reactor geometry
H-FACTOR	$\mathbf{R}(N_m, N_{gr})$			The h-factors per each mixture and per each energy group, as recovered from the extended /macrolib/ data structure.

Table 78: Records in /matex/ data structure

7.3 Contents of /device/ data structure

A /device/ data structure is used to store several information related to the reactor devices. This object has a signature L_DEVICE; it is created using the DEVINI: module. The information contained in this data structure can be used and updated in other DONJON modules which are related to the devices, namely: LZC:, DSET:, MOVDEV: and NEWMAC: modules.

7.3.1 The state-vector content

The dimensioning parameters S_i , which are stored in the state vector for this data structure, represent:

- The type of reactor geometry $I_g = S_1$ (only $I_g = 7$ for 3D-Cartesian geometry allowed)
- The total number of rod-type devices $N_{rod} = S_2$
- The total number of the rod-type groups $N_{rgrp} = S_3$
- The total number of lzc-type devices $N_{lzc} = S_4$
- The total number of the lzc-type groups $N_{lgrp} = S_5$
- Type of control rod movement $I_{mov} = S_6$ where

 $I_{\rm mov} = \begin{cases} 1 & \text{Fading. A fraction of the fully inserted rod vanishes} \\ 2 & \text{Moving. The complete rod is moving (DONJON3-type movement).} \end{cases}$

7.3.2 The main /device/ directory

The following records and sub-directories will be found on the first level of /device/ directory:

Name	Туре	Condition	Units	Comment
$SIGNATURE_{UUU}$	C*12			Signature of the /device/ data structure (SIGNA = I. DEVICE (SIGNA = I
STATE-VECTOR	I(40)			Vector describing the various parameters as- sociated with this data structure S_i
DEV_ROD	$\operatorname{Dir}(N_{rod})$			Sub-directories for each controller rod. A sub- directory is created for each controller rod ac- cording to the rod identification number.
ROD_GROUP	$\operatorname{Dir}(N_{rgrp})$			Sub-directories for each group of rod-type de- vices. A sub-directory is created for each group of rod-type devices according to the rod-group identification number.

Table 79: Records and sub-directories in /device/ data structure

continued on next page

Records and su	b-directories i	n /device/ da	ata structure	continued from last page
Name	Type	Condition	Units	Comment
DEV_LZC	$\operatorname{Dir}(N_{lzc})$			Sub-directories for each liquid zone controller. A sub-directory is created for each liquid con- troller according to the liquid controller iden- tification number.
LZC_GROUP	$\operatorname{Dir}(N_{lgrp})$			Sub-directories for each group of lzc-type de- vices. A sub-directory is created for each group of lzc-type devices according to the lzc- group identification number.

Records and sub-directories in /device/ data structure

7.3.3 The DEV-ROD sub-directories

Inside each ${\tt DEV-ROD}$ sub-directory, the following records will be found:

Name	Type	Condition	Units	Comment
ROD-ID ROD-NAME ROD-PARTS AXIS	I(1) C*12 I(1) I(1)			The identification number of the rod. The identification name of the rod. The number of parts in the rod $(N_{\text{part}} \ge 1)$. The number used to identify the rod mouve- ment direction: = 1 along x-axis; = 2 along
FROM	I(1)			y-axis; =3 along z-axis. The number used to identify the side of ge- ometry, from which the controller rod is in- serted into the reactor core along its direction of mouvement: = 1 if a rod is inserted from the highest position (e.g. from the top); = -1 if a rod is inserted from the lowest position (a.g. from the bottom)
LENGTH	R(2)		cm	(e.g. from the bottom). The initial and final position coordinates of the full-inserted rod along its direction of movement. The rod length is the distance be- tween these two coordinates.
$CORE-LIMITS_{\sqcup}$	R(6)		cm	The initial and final position coordinates of the full core along each Cartesian direction.
MAX-POSuuuu	$R(6 \times N_{part})$		cm	The limiting <i>3D</i> -Cartesian coordinates of the full-inserted rod. This data is given for each part of the rod.

Table 80:	Records	in DEV-ROD	sub-directories
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Records in DEV-ROD sub-directories

continued from last page

Name	Type	Condition	Units	Comment
ROD-MIX	$\mathrm{I}(2\times N_{\mathrm{part}})$			The rod-type mixture indices. The first num- ber corresponds to the inserted rod position and the second to the withdrawn rod position. This data is given for each part of the rod.
LEVEL	R(1)	*		The actual insertion level of the controller rod. This value must be between 0.0 for the full- withdrawn rod and 1.0 for the full-inserted rod.
SPEED	R(1)	*	${\rm cm~s^{-1}}$	The speed of rod movement (insertion or ex- traction).
TIME	R(1)	*	s	The time for the full rod insertion or extrac- tion.
ROD-POS	$R(6 \times N_{part})$	*	cm	The actual <i>3D</i> -Cartesian coordinates of the rod. This data is given for each part of the rod.

7.3.4 The ROD-GROUP sub-directories

Inside each ROD-GROUP sub-directory, the following records will be found:

Name	Type	Condition	Units	Comment
GROUP-ID	I(1) I(1)			The identification number of the rod-group. The total number N_{rd} of rod-devices in the group.
ROD-ID	$I(N_{rd})$			An array of identification numbers of rods which belong to the same group.

Table 81: Records in ROD-GROUP sub-directories

7.3.5 The DEV-LZC sub-directories

Inside each DEV-LZC sub-directory, the following records will be found:

Name	Type	Condition	Units	Comment
LZC-ID	I(1)			The identification number of the liquid zone controller.
MAX-POS	R(6)		cm	The limiting <i>3D</i> -Cartesian coordinates of the whole liquid controller, including its empty and full parts.
AXIS	I(1)			The number used to identify the water filling direction: $= 1$ along x-axis; $= 2$ along y-axis; $= 3$ along z axis
HEIGHT	R(1)		cm	The water height of the full-filled controller
LEVEL	R(1)			The actual water level of the liquid controller device. This value must be between 0.0 for the empty state and 1.0 for the full-filled state
EMPTY-POS	R(6)		cm	The actual 3D-Cartesian coordinates of the empty-part of liquid contoller.
FULL-POS	R(6)		cm	The actual <i>3D</i> -Cartesian coordinates of the full-part of liquid contoller.
EMPTY-MIX	I(2)			The empty-part mixture number and the ref- erence mixture number.
FULL-MIX	I(2)			The full-part mixture number and the reference mixture number.
RATE	R(1)		$m^3 s^{-1}$	The water filling rate.
TIME	R(1)		S	The water filling time.

Table 82: Records in DEV-LZC sub-directories

7.3.6 The LZC-GROUP sub-directories

Inside each $\tt LZC-GROUP$ sub-directory, the following records will be found:

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Name	Type	Condition	Units	Comment
GROUP-ID _{UUUU} NUM-LZC _{UUUUU} LZC-ID _{UUUUUU}	$I(1) \\ I(1) \\ I(N_{ld})$			The identification number of the lzc-group. The total number N_{ld} of lzc-devices in the group. An array of identification numbers of liquid controllers which belong to the same group.

7.4 Contents of a /detect/ data structure

The /detect/ data structure is used to store detector positions and responses. This object has a signature L_DETECT; it is created using the DETINI: module. The information contained in this data structure can be used and updated in other DONJON modules which are related to the detectors, namely: DETECT: and DETINI: modules.

7.4.1 The state-vector content

The dimensioning parameters S_i , which are stored in the state vector for this data structure, represent:

- The number of energy groups. $N_g = S_1$
- The total number of detectors $\sum \mathcal{I}_1 = \mathcal{S}_2$.
- Flag for hexagonal detector definition $S_3 = 1$ for hexagonal detector definition, = 0 otherwise.

The dimensioning parameters for a specific detector type, which are stored in the vector \mathcal{I}_i , represents:

- The number of detectors of type { name_type } \mathcal{I}_1 .
- The number of delayed responses $+2, \mathcal{I}_2$.

7.4.2 The main /detect/ directory

The following records and sub-directories will be found on the first level of /detect/ directory:

Name	Type	Condition	Units	Comment
SIGNATURE	C*12			Signature of the /detect/ data structure $(SIGNA = L_DETECT_{UUUU}).$
STATE-VECTOR	I(40)			Vector describing the various parameters as- sociated with this data structure S_i
{/name_type/}	Dir			Detector type sub-directory contains informa- tions for each detector of this type.

Table 84: Records and sub-directories in /detect/ data structure

7.4.3 The /name_type/ sub-directories

Inside each /name_type/ sub-directory, the following records will be found:

rarious pa- type \mathcal{I}_i .
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of the de-
of the de-
or.
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Table 85: Records in /name_type/ sub-directories

7.4.4 The /name_detect/ sub-directories

Inside each /name_detect/ sub-directory, the following records will be found:

Tal	ble 86:	Record	ls in	/name_detect	/ sub-c	lirectori	es
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Name	Type	Condition	Units	Comment
NHEX POSITION RESPON	I(nhex) R(6) R(\mathcal{I}_2)	hex = 1	cm	The numbers of affected hexagons in the first X-Y plane. The coordinates of the detector. The responses of the detector.

7.5 Contents of /power/ data structure

A /power/ data structure is used to store the information related to the powers and fluxes over the reactor core. This object has a signature L_POWER ; it is created using the FLPOW: module. The reactor fluxes and powers are recorded using several data formats.

$7.5.1~The\ state-vector\ content$

The dimensioning parameters S_i , which are stored in the state vector for this data structure, represent:

• The number of energy groups $N_{gr} = S_1$

- The total number of mesh-splitted volumes $N_{el} = S_2$
- The number of mesh-splitted volumes along x-axis $L_x = S_3$
- The number of mesh-splitted volumes along y-axis $L_y = S_4$
- The number of mesh-splitted volumes along z-axis $L_z = S_5$
- The number of reactor channels $N_{ch} = S_6$
- The number of bundles per channel $N_b = S_7$

7.5.2 The /power/ directory

The following records will be found on the /power/ directory:

Table 87: Records	in /	/power/	data	structure
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Name	Type	Condition	Units	Comment
SIGNATURE	C*12			Signature of the /power/ data structure $(SIGNA = L_POWER_{IIIIIII})$.
STATE-VECTOR	I(40)			Vector describing the various parameters as- sociated with this data structure S_i
PTOT	D(1)		MW	The total reactor power.
VTOTUUUUUUU	D(1)		cm^3	The total reactor volume.
NORM	D(1)			The flux normalization factor.
FLMIX	$I(N_{ch}, N_b)$			Fuel mixture indices per fuel bundle.
FLUX	$\mathbf{R}(N_{el}, N_{gr})$		$\mathrm{cm}^{-2} \mathrm{s}^{-2}$	⁻¹ The normalized fluxes over the whole reactor
				geometry, recorded per each mesh-splitted vol- ume and per each energy group. The flux val- ues over the virtual regions are set to 0.
VOLU-BUND	$R(N_{ch}, N_{b})$		cm^2	The volume of each fuel bundle.
FLUX-BUND	$R(N_{ch}, N_b, N_{ar})$		$\mathrm{cm}^{-2} \mathrm{s}^{-2}$	⁻¹ The normalized average fluxes recorded per
				each fuel bundle and per each energy group.
FLUX-DISTR	$R(L_x, L_u, L_z, N_{ar})$		$\mathrm{cm}^{-2} \mathrm{s}^{-2}$	⁻¹ The normalized flux distribution over the
				whole reactor geometry, recorded per each X-
				Y-Z planes and per each energy group.
FLUX-RATIO	$\mathcal{R}(L_x, L_y, L_z, N_{gr} - 1)$			The fluxes ratios with respect to the thermal
				energy-group fluxes.
POWER-BUND	$\mathrm{R}(N_{ch}, N_b)$		kW	The bundle powers.
POWER-CHAN	$\mathrm{R}(N_{ch})$		kW	The channel powers.
POWER-DISTR⊔	$\mathbf{R}(L_x, L_y, L_z)$		W	The power distribution over the reactor core,
				recorded per each X-Y-Z planes. The power
				values over the non-fuel regions are set to 0.
PMAX-CHAN	$\mathrm{R}(1)$		kW	The maximum channel power.
PMAX-BUND	$\mathrm{R}(1)$		kW	The maximum bundle power.
FORM-CHAN	R(1)			The radial power-form factor, defined as maximum-to-average channel power in core.

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Name	Type	Condition	Units	Comment
FORM-BUND	R(1)			The overall power-form factor, defined as maximum-to-average bundle power in core.
K-EFFECTIVE⊔	R(1)			The effective multiplication factor, recovered from the /flux/ data structure.

All stored fluxes are normalized either to the given total reactor power or using the previously recorded normalization factor. The recorded values of the maximum channel and bundle powers, the channel and bundle power-form factors, and the effective multiplication factor, can be used as power and criticity constraints for the optimization and fuel management purposes.

7.6 Contents of /history/ data structure

This data structure contains the information required to ensure a smooth coupling of DRAGON with DONJON when a history based full reactor calculation is to be performed.

7.6.1 The main directory

The following records and sub-directories will be found in the first level of a /history/ directory:

Name	Type	Condition	Units	s Comment
SIGNATURE	$C*12$ $I(40)$ $R(1)$ $C(\mathcal{S}_{1}^{h})*12$ $R(\mathcal{S}_{1}^{h})$ $C(\mathcal{S}_{2}^{h})*12$ $I(\mathcal{S}_{3}^{h},\mathcal{S}_{4}^{h})$		cm	parameter SIGNA containing the signature of the data structure array S_i^h containing various parameters that are re- quired to describe this data structure parameter L_z containing the fuel bundle length array \mathcal{G}_j containing the names of the global parame- ters array G_j containing the value of the global parame- ters array \mathcal{L}_j containing the names of the local parame- ters array \mathcal{L}_j containing an identification number asso- ciated with bundle <i>i</i> and channel <i>i</i>
FUELID	$I(\mathcal{S}_3^h, \mathcal{S}_4^h)$			array $F_{i,j}$ containing the fuel type associated with bundle <i>i</i> and channel <i>j</i>

Table 88: Main records and sub-directories in /history/

continued on next page

Main records and sub-directories in /history/

Name	Type	Condition	Units Comment
{/FUELDIR/}	Dir		list of sub-directories $FUEL_{i,j}$ that contain the properties associated with the fuel type $F_{i,j}$
{/CELLDIR/}	Dir		list of sub-directories $CELL_{i,j}$ that contain the properties associated with the cell $C_{i,j}$

The signature for this data structure is SIGNA=L_HISTORY_{UUU}. The array S_i^h contains the following information:

- $S_1^h = N_g$ contains the number of global parameters.
- $S_2^h = N_l$ contains the number of local parameters.
- $S_3^h = N_b$ contains the number of bundles per channel.
- $S_4^h = N_c$ contains the number of channels in the core.
- $S_5^h = N_s$ contains the number of bundle shift.
- $S_6^h = T_s$ contains the type of depletion solution used.
- $S_7^h = T_b$ contains the type of burnup considered.
- $S_8^h = N_I$ contains the number of isotopes.
- $S_9^h = G$ contains the number of transport groups.
- $S_{10}^h = N_r$ contains the number of regions.
- $S_{11}^h = N_F$ contains the number of fuel types.

The fuel directory name $\mathsf{FUEL}_{i,j}$ associated with fuel type $F_{i,j}$ is composed using the following FOR-TRAN instruction:

WRITE(FUEL, '(A4, 18.8)') 'FUEL', $F_{i,j}$

This directory will contain the initial isotopic content of this fuel type. The cell directory name $\mathsf{CELL}_{i,j}$ associated with $C_{i,j}$ is composed using the following FORTRAN instruction:

WRITE(CELL, '(A4, 18.8)') 'CELL', C_{i,i}

This directory will contain the value of the local parameters associated with cell $C_{i,j}$ as well as the current isotopic content of this cell.

The identification number $C_{i,j}$ associated with channel j and bundle i can be seen as the serial number of the bundle located at a position in space identified by (i, j). It is automatically managed by the HST: module.^[?] For a fresh core $C_{i,j} = n$ where n represents the cell order definition in the input file. Upon refueling, some bundles in channel k of the core are displaced from region (l, k) to (m, k), new bundles are introduced at location (l, k) and old bundles removed from location (m, k). If one assumes that C^{NEW} and C^{OLD} represents the value of C after and before refueling then we will have:

$$\begin{array}{lcl} C_{m.k}^{\rm NEW} & = & C_{l,k}^{\rm OLD} \\ C_{l,k}^{\rm NEW} & = & C_{m,k}^{\rm FRESH} \end{array}$$

continued from last page

where $C_{m,k}^{\text{FRESH}}$ represent a fresh fuel cell. The local parameters and burnup power density of the fuel cell previously located at (m, k) are preserved and the fresh fuel isotopic densities is that provided in $F_{m,k}$, the fuel type associated with $C_{m,k}^{\text{FRESH}}$.

7.6.2 The fuel type sub-directory

Each fuel sub-directory $\mathsf{FUEL}_{i,j}$ contains the following information

Name	Туре	Condition	Units	Comment
FUELDEN-INIT	R(2)			array containing the initial density of heavy element in the fuel ρ_f in g/cm ³ and the initial linear density of heavy element in the fuel m_f in g/cm
ISOTOPESUSED	$C(N_I)*12$			array containing the name of isotopes used in this fuel type
$\texttt{ISOTOPESMIX}_{\sqcup}$	$I(N_I)$			array containing the mixture associated with each isotopes in this fuel type
ISOTOPESDENS	$\mathbf{R}(N_I)$		$({\rm cm \ b})^{-1}$	array ρ_i containing the density of each isotopes

Table 89: Fuel type sub-directory

7.6.3 The cell type sub-directory

Each cell isotopic sub-directory $\mathsf{CELL}_{i,j}$ contains the following information

Table 90: Cell sub-directory

Name	Type	Condition	Units	Comment
FUELDEN-INIT	R(2)			array containing the initial density of heavy element in the fuel ρ_f in g/cm ³ and the initial linear density of heavy element in the fuel m_f in g/cm.
PARAMLOCALBR	$\mathbf{R}(N_l)$			array V_l^B containing the value of the local parameters before refueling
PARAMLOCALAR	$\mathbf{R}(N_l)$			array V_l^A containing the value of the local parameters after refueling

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Cell sub-directory

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Name	Type	Condition	Units	Comment
PARAMBURNTBR	R(2)			array containing the depletion time T^B in days and the burnup power rate P^B in kW/kg be-
PARAMBURNTAR	R(2)			fore refueling array containing the depletion time T^A in days and the burnup power rate P^A in kW/kg after refueling
DEPL-PARAMuu	R(3)			array containing the time step T in days, the burnup B in kWd/kg and the irradiation w in n/kb currently reached by the fuel in this cell
ISOTOPESDENS	$\mathbf{R}(N_I)$		$({\rm cm \ b})^{-1}$	array ρ_i containing the density of each isotopes

7.7 Contents of /thm/ data structure

This data structure contains the thermal-hydraulics information required in a multi-physics calculation

7.7.1 The main /thm/ directory

The following records and sub-directories will be found in the first level of a /thm/ directory:

Name	Type	Condition	Units Comment
SIGNATURE	C*12		parameter SIGNA containing the signature of the data structure
STATE-VECTOR	I(40)		array \mathcal{S}_i^{th} containing various integer parameters that are required to describe this data structure
$REAL-PARAM_{UU}$	R(40)		array \mathcal{R}_i^{th} containing various floating-point parameters that are required to describe this data structure
KCONDF	$R(\mathcal{S}_{16}^{th}+3)$	$\mathcal{S}_{12}^{th} \neq 0$	coefficients of the user-defined correlation for the fuel thermal conductivity
UCONDF	C12	$\mathcal{S}_{12}^{th} \neq 0$	string variable set to KELVIN or to CELSIUS
KCONDC	$R(\mathcal{S}_{17}^{th}+3)$	$\mathcal{S}_{13}^{\tilde{t}\tilde{h}} \neq 0$	coefficients of the user-defined correlation for the clad thermal conductivity
UCONDC	C12	$\mathcal{S}_{13}^{th} \neq 0$	string variable set to KELVIN or to CELSIUS
ERROR-T-FUEL	R(1)	10 /	K absolute error in fuel temperature
ERROR-D-COOL	R(1)		g/cc absolute error in coolant density

Table 91: Main records and sub-directories in $\rm /thm/$

continued on next page

IGE-300

		1 1	
Name	Type	Condition	Units Comment
ERROR-T-COOL MIN-T-FUEL MIN-D-COOL MIN-T-COOL MAX-T-FUEL MAX-D-COOL MAX-T-COOL HISTORY-DATA	R(1) R(1) R(1) R(1) R(1) R(1) Dir		 K absolute error in coolant temperature K minimum fuel temperature g/cc minimum coolant density K minimum coolant temperature K maximum fuel temperature g/cc maximum coolant density K maximum coolant temperature sub-directory containing the historical values taken by the thermal-hydraulics parameters (mass flux, density, pressure, enthalpy, temperature) in the coolant and in the fuel rod for the whole geometry

Main records and sub-directories in /thm/

The signature for this data structure is SIGNA=L_THM. The array S_i^h contains the following information:

- S_1^{th} contains the number of active fuel rods.
- \mathcal{S}_2^{th} contains the number of guide tubes.
- S_3^{th} contains the maximum number of iterations for computing the conduction integral.
- \mathcal{S}_4^{th} contains the maximum number of iterations for computing the center pellet temperature.
- S_5^{th} contains the maximum number of iterations for computing the coolant parameters (velocity, pressure, enthapy, density) in case of a transient calculation.
- S_6^{th} contains the number of discretisation points in fuel.
- \mathcal{S}_7^{th} contains the number of total discretisation points in the whole fuel rod (fuel+cladding).
- S_8^{th} contains the integer setting the type of calculation (steady-state or transient) performed by the THM: module.
- \mathcal{S}_9^{th} contains the current time index.
- S_{10}^{th} flag to set the gap correlation:

$$S_{10}^{th} = \begin{cases} 0 & \text{built-in correlation is used} \\ 1 & \text{set the heat exchange coefficient of the gap as a user-defined constant} \end{cases}$$

• S_{11}^{th} flag to set the heat transfer coefficient between the clad and fluid:

$$S_{11}^{th} = \begin{cases} 0 & \text{built-in correlation is used} \\ 1 & \text{set the heat exchange coefficient between the clad and fluid as a user-defined constant} \end{cases}$$

• S_{12}^{th} flag to set the fuel thermal conductivity:

$$S_{12}^{th} = \begin{cases} 0 & \text{built-in correlation is used} \\ 1 & \text{set the fuel thermal conductivity as a function of a simple user-defined correlation.} \end{cases}$$

continued from last page

• S_{13}^{th} flag to set the clad thermal conductivity:

 $S_{13}^{th} = \begin{cases} 0 & \text{built-in correlation is used} \\ 1 & \text{set the clad thermal conductivity as a function of a simple user-defined correlation.} \end{cases}$

• S_{14}^{th} type of approximation used during the fuel conductivity evaluation:

 $\mathcal{S}_{14}^{th} = \begin{cases} 0 & \text{use a rectangle quadrature approximation} \\ 1 & \text{use an average approximation.} \end{cases}$

• S_{15}^{th} type of subcooling model:

$$S_{15}^{th} = \begin{cases} 0 & \text{use the Jens-Lottes correlation and Bowring's model} \\ 1 & \text{use the Saha-Zuber subcooling model.} \end{cases}$$

- S_{16}^{th} contains the number of terms in the user-defined correlation for the fuel thermal confuctivity (if $S_{12}^{th} = 1$).
- S_{17}^{th} contains the number of terms in the user-defined correlation for the clad thermal confuctivity (if $S_{13}^{th} = 1$).

The array \mathcal{R}_i^{th} contains the following information:

- \mathcal{R}_1^{th} contains the current time step in s.
- \mathcal{R}_2^{th} contains the fraction of reactor power released in fuel.
- \mathcal{R}_3^{th} contains the critical heat flux in W/m².
- \mathcal{R}_4^{th} contains the inlet coolant velocity in m/s.
- \mathcal{R}_5^{th} contains the outlet coolant pressure in Pa.
- \mathcal{R}_6^{th} contains the inlet coolant temperature in K.
- \mathcal{R}_7^{th} contains the Plutonium mass fraction in fuel.
- \mathcal{R}_8^{th} contains the fuel porosity.
- \mathcal{R}_9^{th} contains the fuel pellet radius
- \mathcal{R}_{10}^{th} contains the internal clad rod radius in m.
- \mathcal{R}_{11}^{th} contains the external clad rod radius in m.
- \mathcal{R}_{12}^{th} contains the guide tube radius in m.
- \mathcal{R}_{13}^{th} contains the assembly surface in m².
- \mathcal{R}_{14}^{th} contains the temperature maximum absolute error (in K) allowed in the solution of the conduction equations.
- \mathcal{R}_{15}^{th} contains the maximum relative error allowed in the matrix resolution of the conservation equations of the coolant.
- \mathcal{R}_{16}^{th} contains the relaxation parameter for the multiphysics parameters (temperature of fuel and coolant and density of coolant).
- \mathcal{R}_{17}^{th} contains the time in s.

- \mathcal{R}_{18}^{th} contains the heat transfer coefficient of the gap (if $\mathcal{S}_{10}^{th} = 1$).
- \mathcal{R}_{19}^{th} contains the heat transfer coefficient between the clad and fluid (if $\mathcal{S}_{11}^{th} = 1$).
- \mathcal{R}_{20}^{th} contains the surface temperature weighting factor of effective fuel temperature for the Rowlands approximation.

7.7.2 The HISTORY-DATA sub-directory

In the HISTORY-DATA directory, the following sub-directories will be found:

Tal	ole	92:	Sub-d	lirectories	in	HISTORY	-DATA	director	y
-----	-----	-----	-------	-------------	----	---------	-------	----------	---

STATIC-PARAM $Dir(N_{ch})$ sub-directory containing all the values of the thermal-hydraulics parameters computed by the THM: module in steady-state conditions and sorted channel by channel. Each chan- nel is identified by an integer numc that can take values between 1 and 9999. For exam- ple, the first channel is identified by the string character "CHANNEL 0001".TIMESTEP numt $Dir(N_{ch})$ sub-directories containing all the values of the thermal-hydraulics parameters computed by the THM: module in transient conditions at a given time index numt and sorted channel by channel. numt can take values between 1 and 9999.

In each of the $N_{\rm ch}$ CHANNEL numc sub-directories, the following records will be found:

Table 93: Records in each CHANNEL directory

Name	Туре	Condition	Units	Comment
VINLET	$R(1) R(1) R(1) R(N_b) R(N_b) R(N_b) R(N_b) R(N_b) R(N_b, N_{dtot}) R(N_b) R(N_b)$		$m.s^{-1}$ K Pa $m.s^{-1}$ Pa $J.kg^{-1}$ $kg.m^{-3}$ $kg.m^{-3}$ K K	inlet velocity inlet temperature inlet pressure velocity in each of the N_b bundles of the chan- nel numbered <i>numc</i> pressure in each bundle of the channel enthalpy in each bundle of the channel density in each bundle of the channel density of liquid phase in each bundle of the channel distribution of the temperature in the fuel-pin for each bundle of the channel center fuel pellet temperature in each bundle of the channel

7.8 Contents of a /optimize/ data structure

The /optimize/ specification is used to store the optimization variables and functions values and definitions, limits and options.

In any case, the signature variable for this data structure must be SIGNA=L_OPTIMIZE_{III}. The dimensioning parameters for this data structure, which are stored in the state vector S_i^o , represents:

- The number of decision variables $N_{var} = S_1^o$.
- The number of constraints $N_{cst} = S_2^o$.
- The type of optimization \mathcal{S}_3^o , where

$$\mathcal{S}_3^o = \begin{cases} 1 & \text{minimization} \\ -1 & \text{maximization} \end{cases}$$

• The result of a test for external convergence of the quadratic constraint \mathcal{S}_4^o , where

$$\mathcal{S}_4^o = \begin{cases} 0 & \text{not converged} \\ 1 & \text{converged} \end{cases}$$

- The number of iterations relative to the quadratic constraint (S_5^o) .
- The type of reduction for the radius if the quadratic constraint (\mathcal{S}_6^o) , where

$$\mathcal{S}_6^o = \begin{cases} 1 & \text{half} \\ 2 & \text{parabolic} \end{cases}$$

- The number of inner iterations S_7^o .
- The number of outer iterations S_8^o .
- The resolution's method for the linear problem with quadratic constraint (S_{q}^{o}) , where

$$S_9^o = \begin{cases} 1 & \text{SIMPLEX/LEMKE} \\ 2 & \text{LEMKE/LEMKE} \\ 3 & \text{MAP} \\ 4 & \text{Augmented Lagragian} \\ 5 & \text{Penalty Method} \end{cases}$$

- The number of outer iterations without step-back S_{10}^o .
- S_{11}^o (not used).
- S_{12}^o (not used).
- A flag for unsuccessful resolution in module $\mathtt{PLQ}\colon S^o_{13},$ where

$$S_{13}^{o} = \begin{cases} 0 & \text{successful at last iteration} \\ \geq 1 & \text{number of iteration with unsuccessful resolution.} \end{cases}$$

Table 94: Main records and sub-directories in /optimize/

Name	Туре	Condition	UnitsComment
SIGNATURE	C*12 I(40)		Signature of the data structure (SIGNA) Vector describing the various parameters as- sociated with data structure S_i^o .
DLEAK-STATE⊔	I(40)	*	Vector describing the various parameters as- sociated with data structure S_i^g . This array is available if the OPTIMIZE object has been created using module DLEAK:.
VAR-VALUE	$R(N_{var})$		The values of the decision variables
$VAR-MAX-VAL_{\sqcup}$	$R(N_{var})$		The maximum values of the decision variables can be.
$VAR-MIN-VAL_{\sqcup}$	$\mathbf{R}(N_{var})$		The minimum values of the decision variables can be.
$VAR-WEIGHT_{\sqcup \sqcup}$	$\mathbf{R}(N_{var})$		The weight of the decision variables w_i in the quadratic constraint.
CST-OBJ _{UUUUU}	$\mathbf{R}(N_{cst})$		The limit value of the contraints. The units depends with the type of the constraint type.
CST-TYPE	$I(N_{cst})$		The type of the contraints: =-1 for \geq ; =0 for =; =1 for \leq .
$CST-WEIGHT_{\sqcup\sqcup}$	$\mathbf{R}(N_{cst})$		The weight of the constraint η_j and γ_j for the duals and meta-heuristic methods.
FOBJ-CST-VAL	$\mathcal{R}(N_{cst}+1)$		The actual values of the objective function (first value) and the contraints (the following values). The number of the constraints are assigned in the order they have been defined.
$OPT-PARAM-R_{\sqcup}$	R(40)		The different limits and values for the iterative calculations of the optimization problem.
GRADIENT	$\mathbf{R}(N_{var}, N_{cst} + 1)$		The gradients of the objective function and the constraints. The gradients of the objec- tive for all the decision variables are in first position, then follow the gradients of the con- straints.
OLD-VALUE	Dir		Directory containing differents informations of the previous iterations. the values of the deci- sion variables, the objective function, the con- straints and the gradients of these functions for the previous external iteration. This reper- tory will be created by the module QLP: unless it is specified to not do.

The array $\tt OPT-PARAM-R$ contains real values related with the different limits and values for the iterative calculations of the optimization problem:

1st	S	initial radius of the quadratic constraint (default: 1.0).
2nd	δ	initial size of the hypercube for MAP method. (default: 0.1).
3rd	$\varepsilon_{\mathrm{ext}}$	limit for external convergence (default: 10^{-4}).
4th	$\varepsilon_{\mathrm{int}}$	limit for internal convergence (default: 10^{-4}).
5th	$\varepsilon_{\rm quad}$	limit for convergence of the quadratic constraint (default: 10^{-4}).
The c	other value of t	the record are not used and set to 0.0.

The optional array DLEAK-STATE contains integer values related to the definition of mixture and group indices in module DLEAK:.

- The number of energy groups in macrolib \mathcal{S}_1^g .
- The number of mixtures in macrolib \mathcal{S}_2^g .
- The type of leakage parameters \mathcal{S}_3^g , where

$$S_3^g = \begin{cases} 1 & \text{use diffusion coefficients} \\ 2 & \text{use } P_1\text{-weighted macroscopic total cross sections.} \end{cases}$$

• The type of control variables \mathcal{S}_4^g , where

$$\mathcal{S}_4^g = \begin{cases} 1 & \text{use leakage parameter itself} \\ 2 & \text{use a correction factor.} \end{cases}$$

- The minimum group index \mathcal{S}_5^g , with $1 \leq \mathcal{S}_5^g \leq \mathcal{S}_1^g$.
- The maximum group index \mathcal{S}_6^g , with $\mathcal{S}_5^g \leq \mathcal{S}_6^g \leq \mathcal{S}_2^g$.
- The minimum mixture index \mathcal{S}_7^g , with $1 \leq \mathcal{S}_7^g \leq \mathcal{S}_2^g$.
- The maximum mixture index \mathcal{S}_8^g , with $\mathcal{S}_7^g \leq \mathcal{S}_8^g \leq \mathcal{S}_2^g$.

7.8.1 The sub-directory /OLD-VALUE/ in /optimize/

Table 95:	Main	records	and	sub-directories	; in	/	/OLD-VALUE//	/
10010 001	11100111	10001000	corr or	bab an octorio		/	/ 0 == ,= 0 = / /	

Name	Туре	Condition	UnitsComment
VAR-VALUE	$\mathbf{R}(N_{var})$		The values of the decision variables of the last valid iteration.
FOBJ-CST-VAL	$\mathcal{R}(N_{cst}+1)$		The values of the objective function and the contraints of the last valid iteration.
GRADIENT	$\mathbf{R}(N_{var}, N_{cst} + 1)$		The gradients of the objective function and the constraints of the last valid iteration.
VAR-VALUE2	$\mathbf{R}(N_{var})$		The values of the decision variables of the second-last valid iteration.
BEST-VAR	$\mathbf{R}(N_{var})$		The values of the decision variables corre- sponding to the best valid solution ever found.
BEST-FCT	R(1)		The value of the objective function corre- sponding to the best valid solution ever found.

8 EXAMPLES

The following examples of input files represent a typical core modeling using DONJON. The main characteristics of a simplified design for the ACR-700 benchmark core model are given below.



Figure 12: Face View of ACR Benchmark Core Model (292 Channels)

- Number of reactor channels 292
- Number of fuel bundles per channel 12
- Core radius 260 cm
- $\bullet~{\rm Core~length}~594.36~{\rm cm}$
- Lattice pitch 22 cm
- Reactor thermal power 1800 MW(th)

8.1 (Example1) – Compo related example

Input data for test case: Example1.x2m

```
******
*
                                                          *
* Input file : Example1.x2m
                                                          *
* Purpose : Test for non-regression using DONJON-4
                                                          *
* Author(s) : D. Sekki (2007/11)
                                                          *
                                                          *
***********
PROCEDURE
             assertS Pgeom Pfmap Pburn Pdevc ;
MODULE
             DELETE: GREP: END: CRE: MACINI: FLUD: USPLIT:
             DSET: TAVG: FLPOW: TRIVAT: TRIVAA: NEWMAC: ;
LINKED_LIST GEOM TRACK MATEX FMAP FLUX POWER MACFL
             DEVICE MACRO1 MACRO2 MACRO SYSTEM ;
LINKED_LIST LREFL1 LREFL2 LFUEL1 LFUEL2
            LZCRin LZCRot LSORin LSORot ;
*--
* variables:
*--
INTEGER nbMix := 8 ;
INTEGER nbRefl nbFuel := 2 2 ;
INTEGER mFuel1 mFuel2 := 1 2 ;
INTEGER mRefl1 mRefl2 := 3 4 ;
INTEGER mZCRin mZCRot := 5 6 ;
INTEGER mSORin mSORot := 7 8 ;
INTEGER MaxReg := 100000 ;
STRING Method := "MCFD";
INTEGER degree quadr := 1 1 ;
INTEGER iter iEdit := 0 5 ;

      REAL
      Power := 1800.;

      REAL
      epsil := 1.E-5;

      REAL
      Precf := 1.E-5;

      REAL
      Eps Keff Bexit;

*--
* compo files:
*--
SEQ_ASCII SFUEL1 :: FILE 'CpoFuel1' ;
SEQ_ASCII SFUEL2 :: FILE 'CpoFuel2';
SEQ_ASCII SREFL1 :: FILE 'CpoMode1';
SEQ_ASCII SREFL2 :: FILE 'CpoMode2';
SEQ_ASCII SZCRin :: FILE 'CpoZCRin';
SEQ_ASCII SZCRot :: FILE 'CpoZCRot' ;
SEQ_ASCII SSORin :: FILE 'CpoSORin';
SEQ_ASCII SSORot :: FILE 'CpoSORot' ;
*--
* compo directories:
*--
         NamFuel1 := "FUEL1 1";
STRING
                                1";
STRING NamFuel2 := "FUEL2
STRING NamRefl1 := "MODE1
                                1";
STRING NamRefl2 := "MODE2
                                 1";
```

```
STRING NamZCRin := "ZCRIN
                              1";
STRING NamZCRot := "ZCROT
                               1";
                              1";
STRING NamSORin := "SORIN
STRING NamSORot := "SOROT
                             1";
*-----
                                     _____
                 FULL-CORE CALCULATION
*
                 ------
*
*--
* geometry construction:
*--
GEOM := Pgeom ;
*--
* reactor material index:
*--
GEOM MATEX := USPLIT: GEOM :: EDIT O NGRP 2 MAXR <<MaxReg>>
            NREFL <<nbRefl>> RMIX <<mRefl1>> <<mRefl2>>
             NFUEL <<nbFuel>> FMIX <<mFuel1>> <<mFuel2>> ;
*--
* numerical discretization:
*--
IF Method "MCFD" = THEN
  TRACK := TRIVAT: GEOM :: EDIT 1
          MAXR <<MaxReg>> MCFD <<degree>> ;
ELSEIF Method "PRIM" = THEN
  TRACK := TRIVAT: GEOM :: EDIT 1
           MAXR <<MaxReg>> PRIM <<degree>> ;
ELSEIF Method "DUAL" = THEN
  TRACK := TRIVAT: GEOM :: EDIT 1
           MAXR <<MaxReg>> DUAL <<degree>> <<quadr>> ;
ENDIF ;
*--
* macrolib for reflector:
*--
LREFL1 := SREFL1 ;
LREFL2 := SREFL2 ;
MACRO1 := CRE: LREFL1 LREFL2 :: EDIT 1 NMIX <<nbMix>> READ
         COMPO LREFL1 MIX <<mRefl1>> <<NamRefl1>> ENDMIX
         COMPO LREFL2 MIX <<mRef12>> <<NamRef12>> ENDMIX ;
*--
* device specification:
*--
DEVICE MATEX := Pdevc MATEX ::
    <<mZCRin>> <<mZCRot>> <<mSORin>> <<mSORot>> ;
*--
* full insertion of ZCR-devices:
*--
DEVICE := DSET: DEVICE :: EDIT 1
         ROD-GROUP 1 LEVEL 1.0 END
         ROD-GROUP 2 LEVEL 1.0 END
         ROD-GROUP 3 LEVEL 1.0 END ;
*--
* update macrolib for devices:
```

```
*--
LZCRin := SZCRin ;
LZCRot := SZCRot ;
LSORin := SSORin ;
LSORot := SSORot ;
MACRO1 := CRE: MACRO1 LZCRin LZCRot LSORin LSORot :: EDIT 1
         READ
         COMPO LZCRin MIX <<mZCRin>> <<NamZCRin>> ENDMIX
         COMPO LZCRot MIX <<mZCRot>> <<NamZCRot>> ENDMIX
         COMPO LSORin MIX <<mSORin>> <<NamSORin>> ENDMIX
         COMPO LSORot MIX <<mSORot>> <<NamSORot>> ENDMIX ;
*--
* fuel-map specification:
*--
FMAP MATEX := Pfmap MATEX ;
*--
* average exit burnups:
*--
FMAP := Pburn FMAP ;
*--
* initialization:
*--
LFUEL1 := SFUEL1 ;
LFUEL2 := SFUEL2 ;
EVALUATE Eps := epsil 1. + ;
*-----
                          _____
                                       _____
              TIME-AVERAGE CALCULATION
*-----
WHILE Eps epsil > iter 20 < * DO
  EVALUATE iter := iter 1 + ;
*--
* fuel-map macrolib:
*--
  MACFL := CRE: LFUEL1 LFUEL2 FMAP :: EDIT O READ
           TABLE LFUEL1
            MIX <<mFuel1>> <<NamFuel1>> ENDMIX
           TABLE LFUEL2
            MIX <<mFuel2>> <<NamFuel2>> ENDMIX ;
*--
* extended macrolib:
*--
  MACRO2 MATEX := MACINI: MATEX MACRO1 MACFL :: EDIT 0 ;
  MACFL := DELETE: MACFL ;
*--
* complete macrolib:
*--
  MACRO MATEX := NEWMAC: MATEX MACRO2 DEVICE :: EDIT 0 ;
  MACRO2 := DELETE: MACRO2 ;
*--
* numerical solution:
*--
  SYSTEM := TRIVAA: MACRO TRACK :: EDIT 0 ;
```

```
MACRO := DELETE: MACRO ;
  IF iter 1 = THEN
     FLUX := FLUD: SYSTEM TRACK :: EDIT 0
             ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
             THER 1000 ;
  ELSE
     FLUX := FLUD: FLUX SYSTEM TRACK :: EDIT O
            ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
             THER 1000 ;
  ENDIF ;
  SYSTEM := DELETE: SYSTEM ;
*--
* flux and power:
*--
  POWER := FLPOW: FMAP FLUX TRACK MATEX ::
           EDIT 0 PTOT <<Power>> ;
*--
* burnups integration limits:
*--
  FMAP := TAVG: FMAP POWER :: EDIT O
           AX-SHAPE RELAX 0.5 B-EXIT ;
  POWER := DELETE: POWER ;
*--
* current parameters:
*--
  GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;</pre>
  GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
  ECHO "Iteration No. " iter ;
  ECHO "AXIAL-SHAPE ERROR : " Eps ;
  ECHO "RESULTING K-EFF : " Keff ;
ENDWHILE ;
*-----
*--
* edit resulting fluxes and powers:
*--
POWER := FLPOW: FMAP FLUX TRACK MATEX ::
       EDIT <<iEdit>> PTOT <<Power>> ;
*--
* last parameters:
*--
GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;</pre>
GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
GREP: FMAP :: GETVAL B-EXIT 1 >>Bexit<< ;</pre>
ECHO "Number of Iterations " iter ;
                       : " Eps
ECHO "AXIAL-SHAPE ERROR
ECHO "CORE-AVERAGE EXIT BURNUP : " Bexit ;
ECHO "RESULTING K-EFFECTIVE : " Keff ;
assertS FLUX :: 'K-EFFECTIVE' 1 1.050128 ;
END: ;
QUIT .
```

8.2 (Example2) – Multicompo related example

```
Input data for test case: Example2.x2m
```

```
*
                                                    *
* Input file : Example2.x2m
                                                    *
* Purpose : Test for non-regression using DONJON-4
                                                    *
* Author(s) : D. Sekki (2007/11)
                                                    *
                                                    *
***********
PROCEDURE
           assertS Pgeom Pfmap Pburn Pdevc ;
MODULE
           DELETE: GREP: END: NCR: MACINI: FLUD: USPLIT:
           DSET: TAVG: FLPOW: TRIVAT: TRIVAA: NEWMAC: ;
LINKED_LIST GEOM TRACK MATEX FMAP FLUX POWER MACFL
           DEVICE MACRO1 MACRO2 MACRO SYSTEM LCPO ;
*--
* variables:
*--
INTEGER nbMix := 8 ;
INTEGER nbRefl nbFuel := 2 2 ;
INTEGER mFuel1 mFuel2 := 1 2 ;
INTEGER mRefl1 mRefl2 := 3 4 ;
INTEGER mZCRin mZCRot := 5 6 ;
INTEGER mSORin mSORot := 7 8 ;
INTEGER MaxReg := 100000 ;
STRING Method := "MCFD" ;
INTEGER degree quadr := 1 1 ;
INTEGER iter iEdit := 0 5 ;
REALPower := 1800.;REALepsil := 1.E-5;REALPrecf := 1.E-5;REALEps Keff Bexit;
*--
* multi-compo file:
*--
SEQ_ASCII SCPO :: FILE 'MultiCompo';
*-----
*
*
                FULL-CORE CALCULATION
*
                _____
*--
* geometry construction:
*--
GEOM := Pgeom ;
*--
* reactor material index:
*--
GEOM MATEX := USPLIT: GEOM :: EDIT 1 NGRP 2 MAXR <<MaxReg>>
            NREFL <<nbRefl>> RMIX <<mRefl1>> <<mRefl2>>
            NFUEL <<nbFuel>> FMIX <<mFuel1>> <<mFuel2>> ;
*--
* numerical discretization:
```
```
*--
IF Method "MCFD" = THEN
   TRACK := TRIVAT: GEOM :: EDIT 1
           MAXR <<MaxReg>> MCFD <<degree>> ;
ELSEIF Method "PRIM" = THEN
   TRACK := TRIVAT: GEOM :: EDIT 1
            MAXR <<MaxReg>> PRIM <<degree>> ;
ELSEIF Method "DUAL" = THEN
   TRACK := TRIVAT: GEOM :: EDIT 1
            MAXR <<MaxReg>> DUAL <<degree>> <<quadr>> ;
ENDIF ;
*--
* macrolib for reflector and devices:
LCPO := SCPO ;
MACRO1 := NCR: LCPO :: EDIT 1 MACRO NMIX <<nbMix>>
          COMPO LCPO MODE
          MIX <<mRefl1>> SET MTYPE CELL20 ENDMIX
          MIX <<mRef12>> SET MTYPE CELL18 ENDMIX
          COMPO LCPO FUEL
          MIX <<mZCRin>>
            SET FTYPE ZCU SET RDTPOS 1. SET RDDPOS 1.
          ENDMIX
          MIX <<mZCRot>>
            SET FTYPE ZCU SET RDTPOS 1. SET RDDPOS 0.
          ENDMIX
          MIX <<mSORin>>
            SET FTYPE SOR SET RDTPOS 1. SET RDDPOS 1.
          ENDMIX
          MIX <<mSORot>>
            SET FTYPE SOR SET RDTPOS 1. SET RDDPOS 0.
          ENDMIX :
*--
* device specification:
*--
DEVICE MATEX := Pdevc MATEX ::
    <<mZCRin>> <<mZCRot>> <<mSORin>> <<mSORot>> ;
*--
* full insertion of ZCR-devices:
*--
DEVICE := DSET: DEVICE :: EDIT 1
          ROD-GROUP 1 LEVEL 1.0 END
          ROD-GROUP 2 LEVEL 1.0 END
          ROD-GROUP 3 LEVEL 1.0 END ;
*--
* fuel-map specification:
*--
FMAP MATEX := Pfmap MATEX ;
*--
* average exit burnups:
*--
FMAP := Pburn FMAP ;
```

```
EVALUATE Eps := epsil 1. + ;
*-----
               TIME-AVERAGE CALCULATION
*-----
WHILE Eps epsil > iter 10 < * DO
  EVALUATE iter := iter 1 + ;
*--
* fuel-map macrolib:
*--
  MACFL := NCR: LCPO FMAP :: EDIT O MACRO
           TABLE LCPO FUEL BURN
           MIX <<mFuel1>> SET FTYPE CELL20 ENDMIX
           TABLE LCPO FUEL BURN
           MIX <<mFuel2>> SET FTYPE CELL18 ENDMIX ;
*--
* extended macrolib:
*--
  MACRO2 MATEX := MACINI: MATEX MACRO1 MACFL :: EDIT 0 ;
  MACFL := DELETE: MACFL ;
*--
* complete macrolib:
*--
  MACRO MATEX := NEWMAC: MATEX MACRO2 DEVICE :: EDIT 0 ;
  MACRO2 := DELETE: MACRO2 ;
*--
* numerical solution:
*--
  SYSTEM := TRIVAA: MACRO TRACK :: EDIT 0 ;
  MACRO := DELETE: MACRO ;
  IF iter 1 = THEN
     FLUX := FLUD: SYSTEM TRACK :: EDIT 0
            ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
            THER 1000 ;
  ELSE
     FLUX := FLUD: FLUX SYSTEM TRACK :: EDIT O
            ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
            THER 1000 ;
  ENDIF ;
  SYSTEM := DELETE: SYSTEM ;
*--
* flux and power:
*--
  POWER := FLPOW: FMAP FLUX TRACK MATEX ::
          EDIT 0 PTOT <<Power>> ;
*--
* burnups integration limits:
*--
  FMAP := TAVG: FMAP POWER :: EDIT O
          AX-SHAPE RELAX 0.5 B-EXIT ;
  POWER := DELETE: POWER ;
*--
* current parameters:
```

```
*--
   GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;</pre>
  GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
  ECHO "Iteration No. " iter ;
  ECHO "AXIAL-SHAPE ERROR : " Eps ;
   ECHO "RESULTING K-EFF : " Keff ;
ENDWHILE ;
*-----
*--
* edit resulting fluxes and powers:
*--
POWER := FLPOW: FMAP FLUX TRACK MATEX ::
        EDIT <<iEdit>> PTOT <<Power>> ;
*--
* last parameters:
*--
GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;</pre>
GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;</pre>
GREP: FMAP :: GETVAL B-EXIT 1 >>Bexit<< ;</pre>
ECHO "Number of Iterations " iter ;
ECHO "AXIAL-SHAPE ERROR : " Eps ;
ECHO "CORE-AVERAGE EXIT BURNUP : " Bexit ;
ECHO "RESULTING K-EFFECTIVE : " Keff ;
assertS FLUX :: 'K-EFFECTIVE' 1 1.050102 ;
END: ;
QUIT .
```

8.3 Procedures

8.3.1 Input file for geometry

Input data for test case: Pgeom.c2m

			1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18				
									3	3	3	3	3	3	3	3								
							3	3	3	3	3	3	3	3	3	3	3	3						
					3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3				
Α				3	3	3	3	1	1	1	1	1	1	1	1	1	1	3	3	3	3			
в				3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3			
С			3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3		
D		3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3	
F		3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	
-	2	о 2	3	1	1		1	1	1	1	1	1	1	•	1				1	1	1	3	3	3
-	2	2	2	-	-	1	-	-	1	1	-	1		-	1	-	-	-	1	4	1	2	2	2
	о О	3	3			•					-	-	<u>'</u>	-	-	-	-	_				3	3	3
H	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3
J	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3
Κ	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3
L	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3
М	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3
Ν	3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3
0		3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	
Ρ		3	3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	3	
Q			3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3		
R				3	3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3			
s				3	3	3	3	1	1	1	1	1	1	1	1	1	1	3	3	3	3			
-					3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3				
							3	3	3	3	3	3	3	3	3	3	3	3						\square
									3	3	3	3	3	3	3	3								

Figure 13: Geometry definition (plane-1)

```
EDIT 1
     X- VOID X+ VOID
     Y- VOID Y+ VOID
     Z- VOID Z+ VOID
MIX
PLANE 1
* - - - 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 - - -
! -
0 0 0 0 0 3 3 3 3 3 3 3 3 3 3 3 3 3 3 0 0 0 0 0 0
                              ! -
! -
! A
0 0 0 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 3 3 0 0 0
                              ! B
0 0 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 3 3 0 0
                              ! C
0 3 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 3 3 3 0
                              ! D
! E
! F
                              ! G
3 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 3 3 3
                              ! H
```

PLANE 9 SAME 1 PLANE 10 SAME 1 PLANE 11 SAME 1 PLANE 12 SAME 1 MESHX 0.0 20. 40. 62. 84. 106. 128. 150. 172. 194. 216. 238. 260. 282. 304. 326. 348. 370. 392. 414. 436. 458. 480. 500. 520. MESHY 0.0 20. 40. 62. 84. 106. 128. 150. 172. 194. 216. 238. 260. 282. 304. 326. 348. 370. 392. 414. 436. 458. 480. 500. 520. MESHZ 0.0 49.53 99.06 148.59 198.12 247.65 297.18 346.71 396.24 445.77 495.30 544.83 594.36 SPLITZ 2 2 2 2 2 2 2 2 2 2 2 2 ; END: ; QUIT .

8.3.2 Input file for devices

Input data for test case: $\mathbf{Pdevc.c2m}$

```
*
                                            *
* Procedure : Pdevc.c2m
                                            *
* Purpose : Reactor rod-devices specification
                                            *
* Author(s) : D. Sekki (2007/06)
                                            *
* CALL
       : DEVICE MATEX := Pdevc MATEX ::
                                            *
      <<mZCRin>> <<mZCRout>> <<mSORin>> <<mSORout>> ;
*
                                            *
PARAMETER DEVICE MATEX ::
                   ::: LINKED_LIST DEVICE MATEX ; ;
MODULE
       END: DEVINI: ;
INTEGER mZCRin mZCRout mSORin mSORout ;
*--
* Read arguments:
*--
 :: >>mZCRin<< >>mZCRout<< >>mSORin<< >>mSORout<< ;
```



Figure 14: Top View of ACR Benchmark Core Model

```
DEVICE MATEX := DEVINI: MATEX :: EDIT 1 NUM-ROD 56 FADE
*--
* ZCR:
*--
ROD 1
ROD-NAME ZCRO1A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS 161.0 183.0 0.0 260.0 123.825 173.355
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 2
```

```
ROD-NAME ZCR01B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 161.0 183.0 260.0 520.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 3
     ROD-NAME ZCRO2A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 205.0 227.0 0.0 260.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 4
     ROD-NAME ZCR02B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 205.0 227.0 260.0 520.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 5
     ROD-NAME ZCRO3A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 249.0 271.0 0.0 260.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 6
     ROD-NAME ZCRO3B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 249.0 271.0 260.0 520.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 7
     ROD-NAME ZCR04A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 293.0 315.0 0.0 260.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 8
     ROD-NAME ZCR04B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 293.0 315.0 260.0 520.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 9
     ROD-NAME ZCR05A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 337.0 359.0 0.0 260.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
```

IGE-300

```
ENDROD
*
   ROD 10
     ROD-NAME ZCR05B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 337.0 359.0 260.0 520.0 123.825 173.355
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 11
     ROD-NAME ZCRO6A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 161.0 183.0 0.0 260.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 12
     ROD-NAME ZCR06B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 161.0 183.0 260.0 520.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 13
     ROD-NAME ZCR07A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 205.0 227.0 0.0 260.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 14
     ROD-NAME ZCR07B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 205.0 227.0 260.0 520.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 15
     ROD-NAME ZCRO8A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 249.0 271.0 0.0 260.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 16
     ROD-NAME ZCR08B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 249.0 271.0 260.0 520.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 17
    ROD-NAME ZCR09A
```

```
LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 293.0 315.0 0.0 260.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 18
     ROD-NAME ZCR09B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 293.0 315.0 260.0 520.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 19
     ROD-NAME ZCR10A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 337.0 359.0 0.0 260.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 20
     ROD-NAME ZCR10B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 337.0 359.0 260.0 520.0 272.415 321.945
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 21
     ROD-NAME ZCR11A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 161.0 183.0 0.0 260.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 22
     ROD-NAME ZCR11B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 161.0 183.0 260.0 520.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 23
     ROD-NAME ZCR12A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 205.0 227.0 0.0 260.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 24
     ROD-NAME ZCR12B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 205.0 227.0 260.0 520.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
```

```
*
   ROD 25
     ROD-NAME ZCR13A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 249.0 271.0 0.0 260.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 26
     ROD-NAME ZCR13B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 249.0 271.0 260.0 520.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 27
     ROD-NAME ZCR14A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 293.0 315.0 0.0 260.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 28
     ROD-NAME ZCR14B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 293.0 315.0 260.0 520.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 29
     ROD-NAME ZCR15A
     LEVEL 0.0 AXIS Y FROM H-
     MAXPOS 337.0 359.0 0.0 260.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*
   ROD 30
     ROD-NAME ZCR15B
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 337.0 359.0 260.0 520.0 421.005 470.535
     DMIX <<mZCRin>> <<mZCRout>>
   ENDROD
*--
* SOR:
*--
   ROD 31
     ROD-NAME SORO1
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 49.53 99.06
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
```

```
ROD 32
     ROD-NAME SORO2
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 183.0 205.0 24.5 495.5 49.53 99.06
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 33
     ROD-NAME SORO3
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 227.0 249.0 24.5 495.5 49.53 99.06
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 34
     ROD-NAME SOR04
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 271.0 293.0 24.5 495.5 49.53 99.06
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 35
     ROD-NAME SORO5
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 315.0 337.0 24.5 495.5 49.53 99.06
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 36
     ROD-NAME SORO6
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 49.53 99.06
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 37
     ROD-NAME SORO7
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 123.825 173.355
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 38
     ROD-NAME SORO8
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 123.825 173.355
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 39
     ROD-NAME SOR09
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 222.885 272.415
```

```
DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 40
     ROD-NAME SOR10
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 227.0 249.0 24.5 495.5 198.12 247.65
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 41
     ROD-NAME SOR11
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 271.0 293.0 24.5 495.5 198.12 247.65
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 42
     ROD-NAME SOR12
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 222.885 272.415
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 43
     ROD-NAME SOR13
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 272.415 321.945
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 44
     ROD-NAME SOR14
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 272.415 321.945
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 45
     ROD-NAME SOR15
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 321.945 371.475
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 46
     ROD-NAME SOR16
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 227.0 249.0 24.5 495.5 346.71 396.24
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 47
```

```
ROD-NAME SOR17
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 271.0 293.0 24.5 495.5 346.71 396.24
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 48
     ROD-NAME SOR18
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 321.945 371.475
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 49
     ROD-NAME SOR19
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 421.005 470.535
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 50
     ROD-NAME SOR20
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 421.005 470.535
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 51
     ROD-NAME SOR21
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 117.0 139.0 53.75 466.25 495.3 544.83
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 52
     ROD-NAME SOR22
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 183.0 205.0 24.5 495.5 495.3 544.83
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 53
     ROD-NAME SOR23
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 227.0 249.0 24.5 495.5 495.3 544.83
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 54
     ROD-NAME SOR24
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 271.0 293.0 24.5 495.5 495.3 544.83
     DMIX <<mSORin>> <<mSORout>>
```

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```
ENDROD
*
   ROD 55
     ROD-NAME SOR25
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 315.0 337.0 24.5 495.5 495.3 544.83
     DMIX <<mSORin>> <<mSORout>>
   ENDROD
*
   ROD 56
     ROD-NAME SOR26
     LEVEL 0.0 AXIS Y FROM H+
     MAXPOS 381.0 403.0 53.75 466.25 495.3 544.83
     DMIX <<mSORin>> <<mSORout>>
    ENDROD
*--
* create rod-devices groups:
*--
   CREATE ROD-GR 5
   GROUP-ID 1
   ROD-ID 1 2 15 16 19 20 23 24 27 28
   GROUP-ID 2
   ROD-ID 3 4 7 8 9 10 13 14
   GROUP-ID 3
   ROD-ID 5 6 11 12 17 18 21 22 25 26 29 30
   GROUP-ID 4
   ROD-ID 31 36 37 38 39 42 43 44 45 48 49 50 51 52 53 54 55
   GROUP-ID 5
   ROD-ID 32 33 34 35 40 41 46 47 53 56 ;
END: ;
QUIT .
```

Input data for test case: $\mathbf{Pfmap.c2m}$

^{8.3.3} Input file for fuel map

```
PARAMETER FMAP MATEX :: ::: LINKED_LIST FMAP MATEX ; ;
MODULE
        END: RESINI: ;
FMAP MATEX := RESINI: MATEX :: EDIT 1
     ::: GEO: CAR3D 20 20 12
       EDIT O
       X- VOID X+ VOID
       Y- VOID Y+ VOID
       Z- VOID Z+ VOID
    MIX
   PLANE 1
  - 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 -
*
   ! -
   0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0 0 0 0
                                       ! A
   0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0 0
                                       ! B
   0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0
                                      ! C
   0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0
                                       ! D
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                       ! E
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                      ! F
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                      ! G
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                      ! H
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                       ! J
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                       ! K
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                       ! L
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                      ! M
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                      ! N
   0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0
                                      ! 0
   0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0
                                       ! P
   0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0
                                       ! Q
   0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0 0
                                      ! R
   0 0 0 0 0 1 1 1 1 1 1 1 1 1 0 0 0 0 0
                                      1 5
   ! -
   PLANE 2 SAME 1
   PLANE 3 SAME 1
   PLANE 4 SAME 1
   PLANE 5
  - 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 -
*
   ! -
   0 0 0 0 2 2 2 2 2 2 2 2 2 2 0 0 0 0 0
                                       ! A
   0 0 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 0 0
                                       ! B
   0 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 0
                                      ! C
```

32 31 30 29 38 39 40 41 42 43 44 45 46 46

9

22

21

33

45	44	43	42	41	40	39	38	47	48	49	50	51	52
53	54	55	55	54	53	52	51	50	49	48	47	56	57
58	59	60	61	62	63	64	64	63	62	61	60	59	58
57	56	65	66	67	68	69	70	71	72	73	73	72	71
70	69	68	67	66	65	65	66	67	68	69	70	71	72
73	73	72	71	70	69	68	67	66	65	56	57	58	59
60	61	62	63	64	64	63	62	61	60	59	58	57	56
47	48	49	50	51	52	53	54	55	55	54	53	52	51
50	49	48	47	38	39	40	41	42	43	44	45	46	46
45	44	43	42	41	40	39	38	29	30	31	32	33	34
35	36	37	37	36	35	34	33	32	31	30	29	21	22
23	24	25	26	27	28	28	27	26	25	24	23	22	21
13	14	15	16	17	18	19	20	20	19	18	17	16	15
14	13	6	7	8	9	10	11	12	12	11	10	9	8
7	6	1	2	3	4	5	5	4	3	2	1		
;													

END: ;

QUIT .

8.3.4 Input file for exit burnups

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Α					1	2	3	4	5	5	4	3	2	1				
в			6	7	8	9	10	11	12	12	11	10	9	8	7	6		
С		13	14	15	16	17	18	19	20	20	19	18	17	16	15	14	13	
D		21	22	23	24	25	26	27	28	28	27	26	25	24	23	22	21	
Е	29	30	31	32	33	34	35	36	37	37	36	35	34	33	32	31	30	29
F	38	39	40	41	42	43	44	45	46	46	45	44	43	42	41	40	39	38
G	47	48	49	50	51	52	53	54	55	55	54	53	52	51	50	49	48	47
н	56	57	58	59	60	61	62	63	64	64	63	62	61	60	59	58	57	56
J	65	66	67	68	69	70	71	72	73	73	72	71	70	69	68	67	66	65
к	65	66	67	68	69	70	71	72	73	73	72	71	70	69	68	67	66	65
L	56	57	58	59	60	61	62	63	64	64	63	62	61	60	59	58	57	56
Μ	47	48	49	50	51	52	53	54	55	55	54	53	52	51	50	49	48	47
Ν	38	39	40	41	42	43	44	45	46	46	45	44	43	42	41	40	39	38
0	29	30	31	32	33	34	35	36	37	37	36	35	34	33	32	31	30	29
Ρ		21	22	23	24	25	26	27	28	28	27	26	25	24	23	22	21	
Q		13	14	15	16	17	18	19	20	20	19	18	17	16	15	14	13	
R			6	7	8	9	10	11	12	12	11	10	9	8	7	6		
S					1	2	3	4	5	5	4	3	2	1				

Figure 15: Combustion zones definition

Input data for test case: Pburn.c2m

```
*
* Procedure : Pburn.c2m
                                                *
* Purpose : Provide average exit burnups
                                                *
* Author(s) : D. Sekki (2007/11)
                                                *
        : FMAP := Pburn FMAP ;
* CALL
PARAMETER FMAP :: ::: LINKED_LIST FMAP ; ;
        END: RESINI: ;
MODULE
 FMAP := RESINI: FMAP :: EDIT 2 REF-SHIFT 8
  BTYPE TIMAV-BURN
  TIMAV-BVAL
*A
  1008.98 1057.69 1071.61 1095.41 1137.92
*B
  1365.60 1586.43 1643.79 1656.34 1756.62
  2014.25 2364.85
*C
  1806.72 2019.33 2425.27 2556.62 2822.28
  3250.93 3391.85 3761.47
*D
  2279.49 2267.03 2563.72 2898.28 3261.49
  3409.15 3715.98 4136.73
*E
  2258.14 2345.30 3173.47 3111.80 3212.21
  3456.56 3705.48 3801.69 3953.67
*F
  2678.92 3263.24 3614.41 3764.97 3813.93
  3857.62 3925.74 4046.12 4119.31
*G
  2792.21 3087.13 3705.48 3960.65 4030.43
  4025.20 3978.10 3990.31 4037.40
*H
  1693.96 2811.67 3666.96 4115.83 4241.15
  4134.99 4025.20 3910.02 3915.26
*.J
  2268.81 3065.97 3826.17 4232.46 4380.19
  4121.05 3995.54 3889.07 3890.81
;
```

END: ; QUIT .

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