# A USER GUIDE FOR DONJON VERSION4 

A. Hébert, D. Sekki, and R. Chambon

Institut de génie nucléaire Département de génie mécanique
École Polytechnique de Montréal January 15, 2016

## Contents

Contents ..... ii
List of Tables ..... v
List of Figures ..... vii
1 INTRODUCTION ..... 1
2 GENERAL SPECIFICATION OF DONJON ..... 3
2.1 Modules ..... 3
2.2 Data structures ..... 5
2.3 Syntactic rules for input specification ..... 6
2.4 General input structure ..... 6
3 GENERAL CORE-DESCRIPTION MODULES ..... 8
3.1 The RESINI: module ..... 8
3.1.1 Main input data to the RESINI: module ..... 9
3.1.2 Input of global and local parameters ..... 10
3.2 The USPLIT: module ..... 14
3.2.1 Input data to the USPLIT: module ..... 14
3.3 The MACINI: module ..... 16
3.4 The DEVINI: module ..... 17
3.4.1 Input data to the DEVINI: module ..... 17
3.4.2 Description of dev-rod input structure ..... 18
3.4.3 Description of rod-group input structure ..... 20
3.5 The DETINI: module ..... 21
3.5.1 Input data to the DETINI: module ..... 21
3.5.2 Description of the detector data ..... 22
3.6 The LZC: module ..... 24
3.6.1 Input data to the LZC: module ..... 24
3.6.2 Description of dev-lzc input structure ..... 25
3.6.3 Description of lzc-group input structure ..... 27
3.7 The DSET: module ..... 28
3.7.1 Input data to the DSET: module ..... 28
3.8 The MOVDEV : module ..... 30
3.8.1 Input data to the MOVDEV : module ..... 30
3.9 The NEWMAC: module ..... 32
3.10 The FLPOW: module ..... 33
3.10.1 Input data to the FLPOW: module ..... 34
3.11 The TAVG: module ..... 36
3.11.1 Input data to the TAVG: module ..... 36
3.11.2 Time-average calculation using DONJON ..... 37
3.12 The TINST: module ..... 39
3.12.1 Input data to the TINST: module ..... 39
3.13 The SIM: module ..... 42
3.13.1 Input data to the SIM: module ..... 42
3.14 The XENON: module ..... 46
3.14.1 Input data to the XENON : module ..... 46
3.15 The DETECT: module ..... 48
3.15.1 Input data to the DETECT: module ..... 48
3.16 The CVR: module ..... 50
3.16.1 Input data to the CVR: module ..... 50
3.17 The HST: module ..... 53
3.17.1 Example ..... 56
4 CROSS-SECTION INTERPOLATION MODULES ..... 60
4.1 The CRE: module ..... 60
4.1.1 Input data for the CRE: module ..... 61
4.2 The NCR: module ..... 64
4.2.1 Interpolation data input for module NCR: ..... 64
4.2.2 Defining local and global parameters ..... 66
4.2.3 Interpolation in the parameter grid ..... 68
4.3 The SCR: module ..... 75
4.3.1 Interpolation data input for module SCR: ..... 75
4.3.2 Defining global parameters ..... 77
4.3.3 Depletion data structure ..... 79
4.3.4 Interpolation in the parameter grid ..... 80
4.4 The AFM: module ..... 85
4.4.1 Input data to the AFM: module ..... 85
4.5 The T16CPO: module ..... 90
4.5.1 Input data for the T16CPO: module ..... 91
5 THERMAL-HYDRAULICS MODULES ..... 94
5.1 The тнM: module ..... 94
5.1.1 Input data to the THM: module ..... 94
6 OPTIMIZATION MODULES ..... 99
6.1 The DLEAK: module ..... 99
6.1.1 Data input for module DLEAK: ..... 99
6.2 The GRAD : module ..... 101
6.2.1 Data input for module GRAD: ..... 101
6.3 The PLQ: module ..... 105
6.3.1 Data input for module PLQ: ..... 105
7 DONJON DATA STRUCTURES ..... 107
7.1 Contents of /fmap/ data structure ..... 107
7.1.1 The state-vector content ..... 107
7.1.2 The main /fmap/ directory ..... 108
7.1.3 The FUEL sub-directories ..... 110
7.1.4 The \{hcycle\} sub-directories ..... 110
7.1.5 The PARAM sub-directories ..... 111
7.2 Contents of /matex/ data structure ..... 112
7.2.1 The state-vector content ..... 112
7.2.2 The /matex/ directory ..... 112
7.3 Contents of /device/ data structure ..... 114
7.3.1 The state-vector content ..... 114
7.3.2 The main / device/ directory ..... 114
7.3.3 The DEV-ROD sub-directories ..... 115
7.3.4 The ROD-GROUP sub-directories ..... 116
7.3.5 The DEV-LZC sub-directories ..... 116
7.3.6 The LZC-GROUP sub-directories ..... 117
7.4 Contents of a / detect/ data structure ..... 118
7.4.1 The state-vector content ..... 118
7.4.2 The main / detect/ directory ..... 118
7.4.3 The /name_type/ sub-directories ..... 118
7.4.4 The /name_detect/ sub-directories ..... 119
7.5 Contents of / power/ data structure ..... 119
7.5.1 The state-vector content ..... 119
7.5.2 The /power/ directory ..... 120
7.6 Contents of /history/ data structure ..... 121
7.6.1 The main directory ..... 121
7.6.2 The fuel type sub-directory ..... 123
7.6.3 The cell type sub-directory ..... 123
7.7 Contents of /thm/ data structure ..... 124
7.7.1 The main /thm/ directory ..... 124
7.7.2 The HISTORY-DATA sub-directory ..... 128
7.8 Contents of a /optimize/ data structure ..... 129
7.8.1 The sub-directory /OLD-VALUE/ in /optimize/ ..... 131
8 EXAMPLES ..... 132
8.1 (Example1) - Compo related example ..... 133
8.2 (Example2) - Multicompo related example ..... 137
8.3 Procedures ..... 140
8.3.1 Input file for geometry ..... 140
8.3.2 Input file for devices ..... 143
8.3.3 Input file for fuel map ..... 152
8.3.4 Input file for exit burnups ..... 155
References ..... 158
Index ..... 160

## List of Tables

1 Structure (DONJON) ..... 6
2 Structure RESINI: ..... 8
3 Structure (descresini1) ..... 9
4 Structure (descresini2) ..... 11
5 Structure USPLIT: ..... 14
6 Structure (desclink) ..... 14
7 Structure MACINI: ..... 16
8 Structure DEVINI: ..... 17
9 Structure (descdev) ..... 17
10 Structure (dev-rod) ..... 19
11 Structure (rod-group) ..... 20
12 Structure DETINI: ..... 21
13 Structure (descinidet) ..... 21
14 Structure (descdet) ..... 22
15 Structure LZC: ..... 24
16 Structure (desclzc) ..... 25
17 Structure (dev-lzc) ..... 25
18 Structure (lzc-group) ..... 27
19 Structure DSET: ..... 28
20 Structure (descdset) ..... 28
21 Structure MOVDEV : ..... 30
22 Structure (descmove) ..... 30
23 Structure NEWMAC: ..... 32
24 Structure FLPOW : ..... 33
25 Structure (descflpow) ..... 34
26 Structure TAVG: ..... 36
27 Structure (desctavg) ..... 36
28 Structure TINST: ..... 39
29 Structure (desctinst) ..... 40
30 Structure SIM: ..... 42
31 Structure (descsim) ..... 42
32 Structure XENON : ..... 46
33 Structure (descxenon) ..... 46
34 Structure DETECT: ..... 48
35 Structure (descdetect) ..... 48
36 Structure CVR: ..... 50
37 Structure (descrcvr) ..... 50
38 Updating an HISTORY structure using a MAP structure ..... 53
39 Updating an HISTORY structure using a BURNUP structure ..... 53
40 Updating a BURNUP structure using an HISTORY structure ..... 53
41 Updating an HISTORY structure using a MAP structure ..... 53
42 Structure (hstdim) ..... 54
43 Structure (hstbrn) ..... 55
44 Structure (hstpar) ..... 56
45 Structure CRE: ..... 60
46 Structure (desccre1) ..... 61
47 Structure (desccre2) ..... 61
48 Structure (descdata1) ..... 62
49 Structure (descdata2) ..... 62
50 Structure (NCR:) ..... 64
51 Structure (ncr_data) ..... 64
52 Structure (descintf) ..... 66
53 NCR inputs for instantaneous cases ..... 71
54 NCR inputs for TA cases ..... 72
55 Structure (SCR:) ..... 75
56 Structure (scr_data) ..... 75
57 Structure (descints) ..... 77
58 Structure (descdepl) ..... 79
59 SCR inputs for instantaneous cases ..... 83
60 SCR inputs for TA cases ..... 84
61 Structure AFM: ..... 85
62 Structure (descafm) ..... 85
63 AFM options summary ..... 89
64 Structure T16CPO: ..... 90
65 Structure (desct16cpo) ..... 91
66 Structure THM: ..... 94
67 Structure (descthm) ..... 94
68 Structure (DLEAK:) ..... 99
69 Structure (dleak_data) ..... 99
70 Structure GRAD ..... 101
71 Structure grad_data ..... 101
72 Structure PLQ: ..... 105
73 Structure plq_data ..... 105
74 Records and sub-directories in /fmap/ data structure ..... 108
75 Records in FUEL sub-directories ..... 110
76 Records in \{hcycle\} sub-directories ..... 111
77 Records in PARAM sub-directories ..... 111
78 Records in /matex/ data structure ..... 113
79 Records and sub-directories in /device/ data structure ..... 114
80 Records in DEV-ROD sub-directories ..... 115
81 Records in ROD-GROUP sub-directories ..... 116
82 Records in DEV-LZC sub-directories ..... 117
83 Records in LZC-GROUP sub-directories ..... 117
84 Records and sub-directories in /detect/ data structure ..... 118
85 Records in /name_type/ sub-directories ..... 119
86 Records in /name_detect/ sub-directories ..... 119
87 Records in / power/ data structure ..... 120
88 Main records and sub-directories in /history/ ..... 121
89 Fuel type sub-directory ..... 123
90 Cell sub-directory ..... 123
91 Main records and sub-directories in /thm/ ..... 124
92 Sub-directories in HISTORY-DATA directory ..... 128
93 Records in each CHANNEL directory ..... 128
94 Main records and sub-directories in /optimize/ ..... 130
95 Main records and sub-directories in //OLD-VALUE// ..... 131

## List of Figures

1 Presentation of fully- and partially-inserted 3-part control rods. ..... 18
2 Complete grid, one point case ..... 73
3 Complete grid, TA case ..... 73
4 Partial grid, complete planes, one point case ..... 73
5 Partial grid, complete planes, TA case ..... 73
6 Partial grid, complete axis, one point case ..... 73
$7 \quad$ Partial grid, complete axis, TA case ..... 73
8 Partial grid, complete axis with another configuration, one point case ..... 74
$9 \quad$ Partial grid, one complete plane and one complete axis, one point case ..... 74
10 Partial grid, one complete plane and one complete axis, TA case ..... 74
11 Partial grid, one complete plane and one complete axis with another configuration, one point case 74
12 Face View of ACR Benchmark Core Model (292 Channels) ..... 132
13 Geometry definition (plane-1) ..... 141
14 Top View of ACR Benchmark Core Model ..... 144
15 Combustion zones definition ..... 155

## 1 INTRODUCTION

DONJON is a full-core modelization code designed around solution techniques of the neutron diffusion or simplified $P_{n}$ equation. ${ }^{[1]}$ The current DONJON package is an evolution version, released as an attempt to introduce the innovative capabilities for the full-core modeling and simulations of different types of nuclear reactors sush as Pressurized Water Reactors (PWRs), legacy CANDU reactors, and Advanced CANDU Reactors (ACRs). The computer code DONJON (Release 4.0) is part of Version4 distribution ${ }^{[2]}$, built around the GAN generalized driver ${ }^{[3]}$. Its execution depends on other computer codes, components of Version4, namely: GANLIB, UTILIB, DRAGON ${ }^{[4]}$, and TRIVAC ${ }^{[5]}$ codes. The DRAGON modules are used with DONJON code to define the reactor geometry, to provide the macroscopic cross-section libraries and to perform micro-depletion calculations. The TRIVAC solver modules are used to perform a spatial discretization of the reactor geometry and to provide the numerical solution according to the user-selected numerical procedure ${ }^{[6-11]}$. The UTILIB library provides the utility and linear algebra libraries. Finally, the GANLIB computer code provides CLE-2000 capabilities to control data flows and to implement computational schemes. GANLIB also provide LCM data structures to exchange information between modules.

The DONJON code is divided into several modules, each module is designed to perform some particular tasks. The transfer of information between the modules is achieved by means of well defined data structure. Several design features, data structure and computing algorithms were recovered, revised and adapted from the previous DONJON version ${ }^{[12,13]}$. One of the main concerns of the DONJON developers is to ensure the code reliability and extensibility.

The DONJON modules are first designed for the reactor full-core modeling in 3-D Cartesian geometry. These modules are built around the reactor fuel lattice specification corresponding to the common design features of CANDU reactors. The modules related to the modeling of reactivity mechanisms, which are normally presented in the reactor core, also constitute an important part of code. The DONJON code can perform several full-core calculations and can be used to determine some important core characteristics, such as the power and normalized flux distributions over the reactor core. All full-core calculations using current version of DONJON correspond to the reactor static conditions.

The modeling of the reactor fuel lattice using DONJON is made in considering that the fuel lattice is composed of a well defined number of fuel channels and bundles. All reactor channels contain the same number of fuel bundles and are identified by their specific names. The fuel bundles have a distinct set of properties that are recovered and interpolated according to the specified global and local parameters. The interpolation of fuel properties with respect to burnup distribution can be performed according to the time-average or instantaneous models ${ }^{[14]}$. The time-average calculation is performed in considering the bidirectional refuelling scheme of reactor channels and assuming that all channels have the same bundle-shift.

The modeling of the reactivity mechanisms is based on their specified parameters, which include the devices position, rods insertion level, water filling level, direction of movement, etc. The rod-devices insertion level can be set according to their nominal positions or they can be displaced in and out of core. The devices can also be divided into several groups so that they can be manipulated, displaced or moved simultaneously. The time-dependent behaviour of the moving devices can be modeled and used for the transient simulations or reactor control studies. The reactivity worth of devices can also be studied and predicted using DONJON.

The reactor material properties are essentially recovered from the reactor database, obtained from the lattice calculations using DRAGON code. The two distinct macroscopic cross-section libraries can be constructed using DONJON. The first macrolib is constructed only for the material properties which are evolution-independent, such as reflector and devices properties. The second macrolib is constructed only for the fuel properties, defined per each fuel bundle over the fuel lattice. The two libraries are next combined and updated, according to the devices insertion level. The produced extended macrolib is subsequently used to obtain the numerical solution, using TRIVAC modules.

Finally, it should be noted that the DONJON code development is permanently in progress. The future updates will provide several extended capabilities for the reactor design and calculations; they will
be gradually added to the subsequent DONJON versions.

## 2 GENERAL SPECIFICATION OF DONJON

### 2.1 Modules

Reactor calculations using DONJON are performed by means of sequential execution of several userselected modules, according to the user-defined computing scheme. Each module is designed to perform some particular tasks. The detailed description of DONJON modules is given in Section 3 to Section 6. In order to perform the reactor calculations, it is also required to use some DRAGON and TRIVAC modules. For more details on DRAGON modules specification, refer to its user guide ${ }^{[4]}$; for more details on TRIVAC modules specification, refer to its user guide ${ }^{[5]}$. Because the code execution is controlled by the GAN generalized driver, it is also possible to use its utility modules ${ }^{[3,4]}$. A brief description of each module that can be executed using DONJON is given below. A short description of each data structure that can be used in DONJON is given in Section 2.2.

- The following DRAGON modules can be executed using DONJON:

GEO: module used to create or modify a reactor geometry. The spatial locations of the reactor material mixtures must also be defined using the GEO: module. Only 3-D Cartesian reactor geometries are allowed with DONJON.

MAC: $\quad$ module used to create or modify a macrolib containing the material properties, by directly specifying the group-ordered macroscopic cross-sections for each selected material mixture.

- The following TRIVAC modules can be executed using DONJON:

TRIVAT: module used to perform a 3-D numerical discretization or "tracking" of the reactor geometry.

TRIVAA: module used to compute the set of system matrices with respect to the previously obtained "tracking" information.

FLUD: module used to compute the numerical solution to an eigenvalue problem, corresponding to a previously obtained set of system matrices.

- The following are short descriptions of utility modules that can be executed using DONJON:

UTL: module used to perform several utility actions on a data structure.
DELETE: module used to delete one or many data structures.
GREP: module used to extract a single value from a data structure.
END: module used to delete all the local linked lists, to close all the remaining local files and to return from a procedure; or to terminate the overall DONJON execution controlled by the GAN generalized driver.

- The following are short descriptions of DONJON modules:

CRE: module used to create a MACROLIB containing the material properties, by interpolating the nuclear properties from a mono-parameter database, previously generated in the lattice code.

NCR: module used to create a MICROLIB or a MACROLIB containing the material properties, by interpolating the nuclear properties from a multi-parameter database, previously generated in the lattice code.

AFM: module used to create a MACROLIB containing the material properties, by interpolating the nuclear properties from a multi-parameter feedback model database, previously generated in the lattice code.

USPLIT:

RESINI: module used to define the fuel lattice, to create the fuel-map geometry and to specify the global and local parameters.

MACINI: module used to create an extended MACROLIB, in which the properties are stored per each material region, over the whole mesh-splitted reactor geometry.

DEVINI: module used for 3-D modeling of rod-type devices in the reactor core.
DETINI: module used to read and store detector information.
LZC:
DSET:

MOVDEV :
NEWMAC:

FLPOW: module used to compute and print powers and normalized fluxes over the reactor core.
TAVG:

TINST: module used to perform burnups calculation according to the time-linear model and compute instantaneous burnups values. This module is specific to Candu reactor refuelling.

SIM: module used to perform burnups calculation according to the time-linear model and compute instantaneous burnups values. This module is specific to PWR reactor refuelling.

DETECT: module used to compute the mean flux at each detector site and the response of each detector according to different types of interpolation.

CVR: module used for the core-voiding simulations.
HST :
module used to manage a full reactor execution in DONJON using explicit DRAGON calculations for each cell (see Section 3.17). [18]

### 2.2 Data structures

The transfer of information between the modules is performed by means of well defined data structures, also called objects. The objects can be defined in either create, read-only or modification mode. Each object has its own specific signature that can be easily recognized by a module. A detailed description of DONJON data structures is given in Section 7. For more details on DRAGON and TRIVAC data structures, refer to their guide ${ }^{[17]}$. A brief description of all data structures that can be used in DONJON is given below.

| GEOMETRY | data structure containing the geometry information. This object has a signature L_GEOM; it is created using DRAGON module GEO:. |
| :---: | :---: |
| MACROLIB | data structure containing the multigroup macroscopic properties; it has a signature L_MACROLIB. This object can be created in several modules, namely: using DRAGON modules MAC: and NCR: ; or using DONJON modules CRE:, MACINI:, and NEWMAC:. |
| COMPO | data structure containing the mono-parameter database, generated by the lattice code. This object has a signature L_COMPO; it is created using DRAGON module CPO: |
| MULTICOMPO | data structure containing the multi-parameter database, generated by the lattice code. This object has a signature L_MULTICOMPO; it is created using DRAGON module COMPO: . |
| SAPHYB | data structure containing the multi-parameter database, generated by the lattice code. This object has a signature L_SAPHYB; it is created using the APOLLO2 lattice code or the DRAGON module SAP:. |
| FMAP | data structure containing the fuel-lattice specification. This object has a signature L_MAP; it is created using DONJON module RESINI: . |
| MATEX | data structure containing the extended reactor material index. This object has a signature L_MATEX; it is created using DONJON module USPLIT: |
| DEVICE | data structure containing the devices specification. This object has a signature L_DEVICE; it is created using DONJON module DEVINI: . |
| DETECT | data structure containing detector positions and responses. This object has a signature L_DETECT; it is created using DONJON module DETINI: and can be modified by the modules DETINI: and DETECT: . |
| TRACK | data structure containing a "tracking" information of the reactor geometry. This object has a signature L_TRACK; it is created using TRIVAC module TRIVAT: . |
| SYSTEM | data structure containing a set of system matrices. This object has a signature L_SYSTEM; it is created using TRIVAC module TRIVAA:. |
| FLUX | data structure containing the numerical solution to an eigenvalue problem. This object has a signature L_FLUX; it is created using TRIVAC module FLUD: . |
| POWER | data structure containing the powers and normalized fluxes over the reactor core. This object has a signature L_POWER; it is created using DONJON module FLPOW: . |
| HISTORY | This data structure contains the information required to ensure a smooth coupling of DRAGON with DONJON when an history based full reactor calculation is to be performed. It is used only by the HST: module. |

### 2.3 Syntactic rules for input specification

The input data to any module is read in free format using the subroutine REDGET. CLE-2000 variables ${ }^{[21,22]}$ are also allowed. The user guide for DONJON is written using the following convention:

- the parameters surrounded by single square brackets '[]' denote an optional input;
- the parameters surrounded by double square brackets '[[ ]]' denote an input which may be repeated as many times as needed;
- the parameters in braces separated by vertical bars ' $\{|\mid\}$ ' denote a choice where one and only one input is mandatory;
- the parameters in bold face and in brackets '( )' denote an input structure;
- the parameters in italics and in brackets with an index '( $\operatorname{data}(\mathrm{i}), \mathrm{i}=1, \mathrm{n})$ ' denote a set of n inputs;
- the words using the typewriter font KEYWORD are character constants used as keywords;
- the words in italics denote the user-defined variables: they are lower-case and of integer type (when starting from $i$ to $n$ ), or of real type (when starting from $a$ to $h$ or from $o$ to $z$ ); or they are upper-case and of character type CHARACTER.


### 2.4 General input structure

DONJON is built around the GAN generalized driver ${ }^{[3,22]}$. Accordingly, all the modules that will be used during the current execution must be first identified. It is also necessary to define the format of each object (data structure) that will be processed by these modules. Then, the modules required for the specific DONJON calculation are called successively, information being transferred from one module to the next via the objects. Finally, the execution of DONJON is terminated when it encounters the END: module, even if it is followed by additional data records in the input data stream. The general input data structure therefore follows the calling specifications given below:

Table 1: Structure (DONJON)

```
[ MODULE [[ MODNAME ]] ; ]
[ LINKED_LIST [[ STRNAME ]] ; ]
[ XSM_FILE [[ STRNAME ]] ; ]
[ SEQ_BINARY [[ STRNAME ]] ; ]
[ SEQ_ASCII [[ STRNAME ]] ; ]
[[ (module) ; ]]
END: ;
```

where
MODULE keyword used to specify the names of all modules that will be used in the current DONJON execution.

MODNAME character*12 name of a DONJON, or DRAGON, or TRIVAC, or utility module. The list of modules that can be executed using DONJON code is provided in Section 2.1.

| NKED LIST | keyword used to specify the names of data structure that will be stored as linked li |
| :---: | :---: |
| XSM_FILE | keyword used to specify the names of all data structure that will be stored on XSM format files. |
| SEQ BINARY | keyword used to specify the names of all data structure that will be stored on sequential binary files. |
| SEQ_ASCII | keyword used to specify the names of all data structures that will be stored on sequential ASCII files. |
| STRNAME | character*12 name of a data structure. The list of data structure that can be used in DONJON is presented in Section 2.2. |
| (module) | input specification for a module that will be executed. For DONJON specific modules, these input structures are described in Section 3 to Section 6. |
| End : | keyword to call the normal end-of-execution utility module. |
| ; | keyword to specify the end of record. This keyword is used to delimit the part of the input data stream associated with each module. |

Generally, the user has the choice to declare the most of data structure in the format of a linked list to reduce CPU times or as a XSM file to reduce memory resources. In general, the data structure are stored on the sequential ASCII files only for the backup purposes.

The input data normally ends with a call to the END: module. However, the GAN driver will insert automatically the END: module, even if it was not provided, upon reaching an end-of-file in the input stream.

Each (module) calling specification contains a module execution description and its associated input structure. All these modules, except the END: module may be called more than once.

## 3 GENERAL CORE-DESCRIPTION MODULES

### 3.1 The RESINI: module

The RESINI: module is used for modeling of the reactor fuel lattice in 3-D Cartesian geometry or 3-D Hexagonal geometry. This modeling is based on the following considerations:

- For 3-D Cartesian geometry, the reactor fuel lattice is composed of a well defined number of fuel channels. Each channel is composed of a well defined number of fuel bundles or assembly subdivisions. All channels contain the same number of fuel bundles or assembly subdivisions. Each reactor channel is identified by its specific name which corresponds to its position in the fuel lattice.

In a Candu reactor, the channels are refuelled according to the bidirectional refuelling scheme. The refuelling scheme of a channel corresponds to the number of displaced fuel bundles (bundle-shift) during each channel refuelling. The direction of refuelling corresponds to the direction of coolant flow along the channel.

In a PWR, a basic assembly layout can be projected over the fuel map using a naval-coordinate position system. Assembly refuelling and shuffling will be possible using the ad hoc module SIM: (see Section 3.13).

- For 3-D Hexagonal geometry, the reactor fuel lattice is composed of a well defined number of fuel channels and each channel is composed of a well defined number of fuel bundle. All fuel bundles have the same volume. All channels contain the same number of fuel bundles. Refuelling is not available during the calculation. The lattice indexation is kept to identify the hexagons.
- The fuel regions generally have a different set of global and local parameters. For example, the fuel bundles have a different evolution of the fuel properties according to the given burnup distribution, which is a global parameter. Consequently, the homogenized cell properties will differ from one fuel region to another, i.e., they are not uniform over the fuel lattice. Thus, the realistic modeling of a reactor core requires the fuel properties to be interpolated with respect to global and local parameters, which must be specified in the fuel map.

Note that the above considerations correspond to the typical core modeling of CANDU or PWR reactors. The RESINI: module will create a new FMAP object that will store the information related to the fuel lattice specification and properties (see Section 7.1).

The RESINI: module specifications are:

Table 2: Structure RESINI:

```
{ FLMAP MATEX := RESINI: MATEX :: (descresini1)
    FLMAP := RESINI: FLMAP :: (descresini2) }
```

where
FLMAP character*12 name of the RESINI object that will contain the fuel-lattice information. If FLMAP appears on both LHS and RHS, it will be updated; otherwise, it is created.

MATEX character*12 name of the MATEX object specified in the modification mode. MATEX is required only when FLMAP is created.
(descresini1) structure describing the main input data to the RESINI : module. Note that this input data is mandatory and must be specified only when FLMAP is created.
(descresini2) structure describing the input data for global and local parameters. This data is permitted to be modified in the subsequent calls to the RESINI: module.
3.1.1 Main input data to the RESINI: module

Note that the input order must be respected.

Table 3: Structure (descresini1)

```
[ EDIT iprint ]
    ::: GEO: (descgeo)
    NXNAME ( XNAME(i), i = 1, nx )
    NYNAME ( YNAME(i), i = 1, ny )
    NCOMB { ncomb B-ZONE (icz(i), i = 1, nch )| ALL }
    [SIM lx ly (naval(i), i = 1, nch )]
    (descresini2)
```

where

EDIT
iprint $\quad$ integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); larger values produce increasing amounts of output.
$::=\quad$ keyword used to indicate the call to an embedded module.
GEO: keyword used to call the GED: module. The fuel-map geometry differs from the complete reactor geometry in the sense that it must be defined as a coarse geometry, i.e. without mesh-splitting over the fuel bundles. Consequently, the mesh-spacings over the fuel regions must correspond to the bundle dimensions (e.g. $h_{x}=$ width; $h_{y}=$ height; $h_{z}=$ length or in 3-D Hexagonal geometry $h_{x}=$ side; $h_{z}=$ height). Note that the total number of non-virtual regions in the embedded geometry must equal to the number of fuel channels times the number of fuel bundles per channel. This means that only the fuel-type mixture indices are to be provided in the data input to the GEO: module for MIX record. Other material regions (e.g. reflector) must be declared as virtual, i.e. with the mixtures indices set to 0 .
(descgeo) structure describing the input data to the GEO: module (see the user guide ${ }^{[4]}$ ). Only $3-D$ Cartesian or 3-D Hexagonal fuel-map geometry is allowed.

NXNAME keyword used to specify XNAME. Not used for 3-D Hexagonal geometry.
XNAME character*2 array of horizontal channel names. A horizontal channel name is identified by the channel column using numerical characters ' 1 ', ' 2 ', ' 3 ', and so on. Note that the total number of X-names must equal to the total number of subdivisions along the X-direction in the fuel-map geometry. All non-fuel regions are to be assigned a single character '-'. This option is not available for 3-D Hexagonal geometry.

| nX | integer total number of subdivisions along the X-direction in the fuel-map geometry. <br> Not used for 3 -D Hexagonal geometry. |
| :--- | :--- |
| NYNAME | keyword used to specify YNAME. Not used for 3-D Hexagonal geometry. |
| YNAME | character*2 array of vertical channel names. A vertical channel name is identified <br> by the channel row using alphabetical letters 'A' (from the top), 'B', 'C', and so on. <br> The total number of Y-names must equal to the total number of subdivisions along <br> the Y-direction in the fuel-map geometry. All non-fuel regions are to be assigned a <br> single character '-'. This option is not available for 3 -D Hexagonal geometry. <br> integer total number of subdivisions along the Y-direction in the fuel-map geometry. |
| Not used for 3-D Hexagonal geometry. |  |

### 3.1.2 Input of global and local parameters

The information with respect to the fuel burnup is required for the fuel-map macrolis construction, using either the CRE:, NCR: or AFM: module. The fuel-region properties related to other local or global parameters can be interpolated only using the NCR: module.

## Table 4: Structure (descresini2)

```
EDIT iprint ]
BTYPE { TIMAV-BURN| INST-BURN } ]
[ TIMAV-BVAL (bvalue(i), i = 1, ncomb )]
[ INST-BVAL { SAME bvalue | CHAN (bvalue(i), i=1, nch )|BUND (bvalue(i), i=1,nch.nb )|
SMOOTH } ]
BUNDLE-POW { SAME pwvalue | CHAN (pwvalue(i), i = 1, nch )| BUND (pwvalue(i), i = 1, nch mb ) } ]
REF-SHIFT { ishift | COMB (ishift(i), i = 1, ncomb ) } ]
[ ADD-PARAM PNAME PNAME PARKEY PARKEY { GLOBAL | LOCAL } ]]
[ SET-PARAM PNAME { pvalue | { [ TIMES PNAMEREF ] SAME pvalue |
    CHAN (pvalue(i), i = 1, nch )| BUND (pvalue(i), i = 1, nch .nb ) } } ]]
[ FUEL { WEIGHT | ENRICH | POISON } (fvalue(i), i = 1, nfuel ) ]]
CELL (ialch(i), i = 1, nch )]
```

where
EDIT keyword used to set iprint.
iprint $\quad$ integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); $=2$ to print the channels refuelling schemes (if they are new or modified) $;=3$ initial burnup limits per each channel are also printed (if the axial power-shape has been reinitialized).

BTYPE keyword used to specify the type of interpolation with respect to burnup data. This information will be used during the execution of CRE:, NCR: or AFM: module.

TIMAV-BURN keyword used to indicate the burnups interpolation according to the time-average model. This option is not available in 3-D Hexagonal geometry.

INST-BURN keyword used to indicate the burnups interpolation according to the instantaneous model.

TIMAV-BVAL keyword used to indicate the input of average exit burnup values per each combustion zone. Note that the axial power-shape and the first burnup limits will be reinitialized each time the average exit burnups are modified by the user. These data are required for the time-average calculation (see Section 3.11). This option is not available with 3-D Hexagonal geometry.

INST-BVAL keyword used to specify the instantaneous burnup values for each fuel bundle.
SMOOTH

BUNDLE-POW keyword used to specify the power values for each fuel bundle. This option is not available in $3-D$ Hexagonal geometry.
bvalue real array containing the burnups values, given in $M W \cdot d a y$ per tonne/MW of initial heavy elements. The fuel burnup is considered as a global parameter.
pwvalue real array containing the powers values, given in kW .


## PARKEY

PARKEY character*12 corresponding name of a given parameter as it is recorded in the particular multi-parameter compo file. The PARKEY name of a parameter may not be same as its PNAME and can also differ from one multi-compo file to another.

GLOBAL keyword used to indicate that a given parameter is global, which will have a single and constant parameter's value.

LOCAL keyword used to indicate that a given parameter is local. In this case, the total number of recorded parameter's values will be set to $N_{\mathrm{ch}} \times N_{\mathrm{b}}$.

SET-PARAM keyword used to indicate the input (or modification) of the actual values for a parameter specified using its PNAME.

SAME keyword used to indicate that a core-average value of a local parameter will be provided. If the keyword SAME is specified, then this average value will be set for all fuel bundles for every reactor channel.
keyword used to indicate that the values of a local parameter will be provided per each reactor channel. If the keyword CHAN is specified, then the channel-averaged parameter's value will be set for all fuel bundles containing in the same reactor channel.

BUND keyword used to indicate that the values of a local parameter will be specified per each fuel bundle for every channel.
keyword used to indicate that the values of the local parameter PNAME is a translation of the local parameter PNAMEREF via a multiplication of the constant indicated by SAME.

PNAMEREF
pvalue

FUEL
WEIGHT
ENRICH
POISON
fvalue
nfuel
CELL
ialch
character*12 identification name of a given parameter.
real array (or a single value) containing the actual parameter's values. Note that these values will not be checked for consistency by the module. It is the user responsibility to provide the valid parameter's values which should be consistent with those recorded in the multicompo database.
keyword used to indicate the input of data which will be specified for each fuel type.
keyword used to indicate the input of fuel weight in a bundle, given in kg .
keyword used to indicate the input of fuel enrichment values, given in $w t \%$.
keyword used to indicate the input of poison load in a fuel.
real value of the fuel-type parameter, specified for each fuel type in the same order as the fuel mixture indices have been recorded in the matex object (see Section 3.2.1).
integer total number of the fuel types, as been defined in the USPLIT: module.
keyword used to specify that a patterned age distribution will be input and used to compute instantaneous bundle burnup.
real array containing the refueling sequence numbers. This channel is refueled the ialch(i)th one. The channels are ordering from the top left to the bottom right of the core. The expression of the resulting bundle burnups are given in Ref. 19.

### 3.2 The USPLIT: module

The USPLIT: module is used to create a MATEX object that will provide a link between the reactor geometry and material index. The 3-D Cartesian or 3-D Hexagonal reactor geometry, which is previously produced in the GEO: module, is analyzed and the material mixture indices are recomputed in order to provide a unique mixture number for each material sub-volume. Such renumbering permits a complex reactor core modeling. A MATEX object is also used to store some additional information that will be required and updated by other DONJON modules (see Section 7.2).

The USPLIT: module specification is:

Table 5: Structure USPLIT:

```
GEOM MATEX := USPLIT: { GEOM | GEOMOLD } :: (desclink)
```

where
GEOM character*12 name of a GEOMETRY object. This object is defined in creation (appears only on LHS) or modification (appears on both LHS and RHS) mode. An existing geometry previously created in the GEO: module is modified. Only 3-D Cartesian or 3-D Hexagonal reactor geometries are allowed.

MATEX character*12 name of a MATEX object to be created by the module.
GEOMOLD character*12 name of a GEOMETRY object previously created in the GEO: module. This object must be specified in read-only mode (appears only on RHS). It is copied into GEOM at the beginning of USPLIT : module. Only 3-D Cartesian or 3-D Hexagonal reactor geometries are allowed.
(desclink) structure describing the input data to the USPLIT: module.

### 3.2.1 Input data to the USPLIT: module

Note that the fuel-type and reflector-type mixture indices are need to be specified explicitly and the input order must be respected.

Table 6: Structure (desclink)

```
[ EDIT iprint]
NGRP ngrp
MAXR maxreg
NMIX nmixt
[ NREFL nrefl RMIX ( mixr(i), i = 1, nrefl )]
[ NFUEL nfuel FMIX ( mixf(i), i = 1, nfuel )]
```

where

| EDIT | keyword used to set iprint. |
| :---: | :---: |
| iprint | integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); larger values produce increasing amounts of output. |
| NGRP | keyword used to specify ngrp. |
| ngrp | integer total number of energy groups. This value must be greater than 0 . |
| MAXR | keyword used to specify maxreg. |
| maxreg | integer maximum number of mesh-splitted regions in the reactor geometry. In 3-D Hezagonal geometry, it corresponds to the total number of prismatic blocks $l_{h}{ }^{*} l_{z}$. |
| NMIX | keyword used to extend number of material mixtures in case new fuels are going to be inserted in the fuel map in upcoming fuel cycles. By default, nmixt is set to the maximum mixture index in RHS geometry GEOM or GEOMOLD. |
| nmixt | the maximum fuel mixture index in the complete life of the reactor. This number must be greater than the maximum mixture index in RHS geometry GEOM or GEOMOLD. |
| NREFL | keyword used to specify nrefl. |
| nrefl | integer total number of reflector types. A reactor should have at least one reflector material. |
| RMIX | keyword used to specify mixr. |
| mixr | integer array of the reflector-type mixture indices. Each reflector type is assigned a distinct mixture number as previously defined in the GEOMETRY object. |
| NFUEL | keyword used to specify nfuel. |
| nfuel | integer total number of fuel types. A reactor should have at least one fuel type. |
| FMIX | keyword used to specify mixf. |
| mixf | integer array of the fuel-type mixture indices. Each fuel type is assigned a distinct mixture number as previously defined in the GEOMETRY object. |

### 3.3 The MACINI: module

The MACINI: module is used to construct an extended mACrOLIB, in which the properties are stored per each material region over the whole mesh-splitted reactor geometry. This macrolib is obtained by combining the material properties which are contained in the two distinct MACROLIB objects:

- The first macrolib contains the material properties which are evolution-independent, such as reflector and device properties. It is created using either MAC:, CRE: , NCR: or AFM: module.
- The second is a fuel-map macrolib created using either CRE:, NCR: or AFM: module. It must contain the interpolated fuel properties per each fuel bundle.

The resulting MACROLIB will contain the properties that are stored for each reactor material and per each mesh-splitted volume. When the devices are not present in the reactor core, then the resulting MACROLIB can be considered as a complete reactor MACROLIB and it can be directly used for the numerical solving. However, when the devices are inserted into the reactor core, the resulting macrolib is not yet complete; it must be subsequently updated with respect to the device properties, using the NEWMAC: module (see Section 3.9).

The MACINI: module specification is:

Table 7: Structure MACINI:

```
MACRO2 MATEX := MACINI : MATEX MACRO [ MACFL ] : : [ EDIT iprint ];
```

where
MACRO2 character*12 name of the extended mACrOLIB to be created by the module.
MATEX character*12 name of the MATEX object containing an extended material index over the reactor geometry. MATEX must be specified in the modification mode; it will store the recovered h-factors per each fuel region.

MACRO character*12 name of a MACROLIB, created using either MAC:, CRE:, NCR: or AFM: module, for the evolution-independent material properties (see structure (desccre1) or refer to the user guide ${ }^{[4]}$ ).

MACFL character*12 name of a fuel-map MACROLIB, created using either CRE:, NCR: or AFM: module, for the interpolated fuel properties (see structure (desccre2) or refer to the user guide ${ }^{[4]}$ ).

EDIT keyword used to set iprint.
iprint $\quad$ integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing; larger values produce increasing amounts of output. The default value is iprint $=1$.

### 3.4 The DEVINI: module

The DEVINI: module is used for the modeling of reactivity mecanisms, based on the devices specifications which are read from the input data file. The module will create a new DEVICE object that will store the devices specifications and parameters (see Section 7.3). Note that only the rod-type (i.e. solid) devices are considered using the DEVINI : module; the liquid zone controllers can be added subsequently, using the LZC: module (see Section 3.6). A rod-type device is a reactivity controller rod (or plate), such as: a zone control rod (ZCR), a shutoff rod (SOR), etc. Several devices parameters can be modified using the DSET: module (see Section 3.7).

A device specification includes several controller rod parameters, such as: a rod position, rod insertion level, direction of movement, etc. The devices positions can not overlap in the reactor core; they are referred using 3 -D-Cartesian coordinates. The insertion level of rods can be set according to their nominal positions or they can be displaced in or out of core. The rods can also be divided into the several user-defined groups so that they can be manipulated, displaced or moved simultaneously.

The DEVINI: module specification is:

Table 8: Structure DEVINI:

DEVICE MATEX := DEVINI: MATEX :: (descdev)
where
DEVICE character*12 name of the DEVICE object that will be created by the module; it will contain the devices information.

MATEX character*12 name of the MATEX object that will be updated by the module. The rod-devices material mixtures are appended to the previous material index and the rod-devices indices are also modified, accordingly.
(descdev) structure describing the input data to the DEVINI: module.

### 3.4.1 Input data to the DEVINI: module

The DEVINI: module allows the definition of rod-type devices made of one or many (up to 10) parts, as depicted in Fig. 1.

Table 9: Structure (descdev)

```
[ EDIT iprint]
NUM-ROD nrod [ { FADE | MOVE } ]
((dev-rod), i = 1, nrod )
[ CREATE ROD-GR ngrp ( (rod-group), i = 1, ngrp )]
;
```



Figure 1: Presentation of fully- and partially-inserted 3-part control rods.
where
EDIT keyword used to set iprint.
iprint integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); larger values produce increasing amounts of output.

NUM-ROD keyword used to specify nrod.
nrod integer total number of the reactor rod-type devices. This number must be greater than 0 .

FADE
MOVE
CREATE
ROD-GR
ngrp
fading rod keyword. A fraction of the fully inserted rod vanishes (default option).
moving rod keyword. The complete rod is moving (DONJON3-type movement).
keyword used to create the rod-groups of devices. The creation of groups is optional.
keyword used to set ngrp.
integer total number of the rod groups to be created. This number must be greater than 0 .
(dev-rod) structure describing the input data for each individual rod.
(rod-group) structure describing the input data for each group of rods.

### 3.4.2 Description of dev-rod input structure

A rod position is referred by its 3-D Cartesian coordinates only. Note that the devices positions can not overlap. The input order of data must be respected.

Table 10: Structure (dev-rod)

```
ROD id
    ROD-NAME NAME
    AXIS {X|Y|Z }
    FROM { H+ | H- }
    [ LEVEL value ]
    [ SPEED speed]
    [ TIME time ]
    [[ MAXPOS (pos(i), i = 1, 6) DMIX mix1 mix2 ]]
ENDROD
```

where
ROD keyword used to specify the rod id number.
id integer identification number of the current rod. Each rod-type device must be assigned a unique id number, given in an ascending order ranging from 1 to nrod.

ROD-NAME keyword used to specify the rod NAME.
NAME character*12 name of the current rod. In general, this name is composed by the rod specific type (e.g. SOR, ZCR, etc.) followed by its sequential number (e.g. 01, 02, etc.).

AXIS keyword used to specify the rod movement axis. A rod can be displaced along only one of the axis.

X keyword used to specify that a rod is displaced along X axis.
Y
Z
FROM keyword used to specify the insertion side of geometry. The rod-devices can be inserted into the reactor core from only one side of geometry. For example, some vertically moving devices can be inserted only from the top, whereas other only from the bottom.
$\mathrm{H}+\quad$ keyword used to specify that a rod will be inserted into reactor core from the highest position (e.g. from the top for vertically moving rod-device).

H- keyword used to specify that a rod will be inserted into reactor core from the lowest position (e.g. from the bottom for vertically moving rod-device).

LEVEL keyword used to specify the actual rod insertion level value. By default, the rod insertion level is left undefined.
value real positive value of the rod insertion level. This value is used to compute the actual rod position in the reactor core. The rod insertion level is minimal (value $=0.0$ ) when the rod is completely withdrawn, and it is maximal (value $=1.0$ ) when the rod is fully inserted. For the partially inserted rod the insertion level must be: $0.0<$ value $<1.0$

SPEED keyword used to specify speed. By default, the speed is left undefined.
speed real positive value of the rod movement speed, given in $\mathrm{cm} / \mathrm{s}$. This value is needed only for the reactor regulating purpose.

| TIME | keyword used to specify time. By default, the insertion time is left undefined. |
| :--- | :--- |
| time | real value of time for the rod insertion (or extraction), given in sec. This value is <br> needed only for the reactor regulating purpose. |
| MAXPOS | keyword used to specify the full-inserted coordinates of a rod part. The sequence of <br> MAXPOS and DMIX data structures is repeated for each part making the rod. |
| real array containing 3-D Cartesian coordinates of the full-inserted rod. This is the |  |
| limiting rod position in the reactor core, which may or may not be the same as the |  |
| actual rod position. These coordinates must be given in the order: X-, X,$+ \mathrm{Y}-, \mathrm{Y}+$, |  |
| Z-, and Z+. |  |$\quad$| keyword used to specify mix1 and mix2. |
| :--- |
| mix1 |
| first of two integer rod mixture indices. Index mix1 corresponds to the perturbed cross |
| mix2 |

### 3.4.3 Description of rod-group input structure

The partition of devices into groups is very useful when the same action is to be applied to several rods, e.g. setting of new parameters (using the DSET: module) or rods moving (using the MOVDEV: module).

Table 11: Structure (rod-group)

```
GROUP-ID igrp { ROD-ID [[ id ]]| ALL }
```

where
GROUP-ID keyword used to set igrp number.
igrp integer identification number of a group to be created. Each rods group must be assigned a unique identification number, given in ascending order ranging from 1 to ngrp.

ROD-ID keyword used to set the rod id numbers.
id integer identification numbers of rods which belong to the same group igrp. A particular rod (or several rods) may belong to different groups, but it could not be repeated inside the same group. The total number of rods in any group must be between 1 and nrod.

ALL keyword used to specify that all rods will belong to the same group igrp.

### 3.5 The DETINI: module

The DETINI: module is used to read and store detector information. A detector is represented by a 2-D or 3-D Cartesian/Hexagonal geometry.

The DETINI: module specification is:

Table 12: Structure DETINI:

```
DETECT := DETINI: [ DETECT ] :: (descdet)
```

where
DETECT character*12 name of the DETECT object that will be created by the module; it will contain the detector informations. If DETECT appear on RHS, it is updated, otherwise, it is created.
(descdev) structure describing the input data to the DETINI: module.
3.5.1 Input data to the DETINI: module

Note that the input order must be respected.

Table 13: Structure (descinidet)

```
[ EDIT iprt ] [ HEXZ ] NGRP ngrp
[[ TYPE NAMTYP
INFO ndetect nrep { SPECTRAL ( spec(i), i=1,ngrp )| DEFAULT }
[ INVCONST ( tinv(i), i=1,nrep-2 ) ] [ FRACTION ( fract(i), i=1,nrep-1 )]
( (descdet), i=1,ndetect ) ]]
;
```

where
EDIT keyword used to set iprt.
iprt index used to control the printing in module INIDET: = $=1,2$ for no print(default value) $;=3$ for printing the contents of the output DETECT.

HEXZ keyword to specify that only hexagonal detectors will be defined. If this keyword is absent, Cartesian detectors will be defined.

NGRP keyword used to set ngrp.
ngrp number of energy groups in the calculation. It must be equal to the number set in the MACD : module or by the COMPO files.

TYPE keyword to specify the detector type.
NAMTYP character*12 name of the detector type. To correspond to the actual detector response model encoded, the type of detector must be in this list:

- PLATN_REGUL
- PLATN_SAU
- VANAD_REGUL
- CHION_SAU
- CHION_REGUL

For other type names, only a fixed normalisation can be performed.
INFO keyword to specify the information associated with the detector type.
ndetect number of detectors of the specified type.
nrep number of detector response components for the specified type. It must be greater or equal to 2 , corresponding to a response in fraction and the reference flux value.

SPECTRAL keyword to specify the energy spectral of a detector type.
spec
array containing the energy spectral of a detector type.
DEFAULT keyword to specify the energy spectral will be initialized as 1.0 for the highest energy group and 0.0 for other groups.

INVCONST keyword to specify the inverse time constants of the detector type model. This option is only valid for platinum, (NAMTYP $(1: 5)=$ 'PLATN'), detector type.
tinv array containing the inverse time constants of the detector model.
FRACTION keyword to specify the fractions corresponding to each delayed or prompt reponse of the detector type model. This option is only valid for platinum, $(\operatorname{NAMTYP}(1: 5)=$ 'PLATN'), detector type.
frac array containing the detector type model fractions.
(descdet) structure describing the format used to read detector information.

### 3.5.2 Description of the detector data

Note that the information input order must be respected.

Table 14: Structure (descdet)

```
NAME NAMDET
[ NHEX nhex HEX ( ihex(i), i=1,nhex ) ]
POSITION ( pos(i), i=1,6 )
RESP ( rep(i), i=1,nrep )
ENDN
```

where
NAME keyword to specify the detector name.
character*12 name of the detector. The different names in alphabetical order must fit their usual numbering in the core.(Ex: PLATN01, CHION01C)
keyword to set the number of hexagons where the detector is placed.
number of hexagons.
keyword to set the hexagon numbers corresponding to the detector position.
array containing the hexagon numbers where the detector is present, as ordered in the geometry definition.
keyword to specify the detector coordinates.
array containing the positions of the specified detector. The positions must be read as $\mathrm{X}-\mathrm{X}+\mathrm{Y}-\mathrm{Y}+\mathrm{Z}-\mathrm{Z}+$. For 2-D geometry, Z coordinates must be 0.0 and a value greater than 1.0. For hexagonal geometry, only Z coordinates are used in 3-D representation.
keyword to specify the detector initial responses.
array containing the initial responses of the detector. To use the current detector models in DONJON, responses are given as

- For vanadium detectors: current response, last response.
- For platinum detectors: current response, reference flux, last detector slow responses.
- For ion chamber detectors: current logarithmic response, current log rate response, reference flux.
keyword to specify the end of the detector informations.


### 3.6 The LZC: module

The LZC: module is used for the modeling of liquid zone controllers, which are normally presented in the CANDU6-type reactor core. The liquid zone controllers specifications are read from the input data file. Note that this modeling can be made after the rod-type devices have been previously defined using the DEVINI: module (see Section 3.4). In this case, the previously created DEVICE object will be updated by the LZC: module; it will store the additional and separate information with respect to the liquid controllers (see Section 7.3).

The liquid zone controller specification includes several device parameters, such as: the whole device position, water filling level, direction of filling, etc. Note that a liquid zone controller is normally composed of two parts: one part is empty and the second part is full-filled. The water level can be adjusted according to the control reactivity requirements. The controllers positions are referred using 3-D-Cartesian coordinates. Several devices parameters can be modified using the DSET: module (see Section 3.7). The liquid controllers can also be divided into the several user-defined groups so that they can be manipulated simultaneously.

The LZC: module specification is:

Table 15: Structure LZC:

```
DEVICE MATEX := LZC: [ DEVICE ] MATEX :: (desclzc)
```

where

DEVICE \begin{tabular}{l}
character*12 name of the DEVICE object. Note, if the rod-type devices are not <br>
present in the reactor core, then DEVICE object must appear only on the LHS (i.e. <br>
in create mode), it will contain the information only with respect to the liquid zone <br>
controllers. However, if the rod-type devices are present in the reactor core, then they <br>
must be specified first (i.e. before the liquid controllers) using the DEVINI: module <br>
(see Section 3.4). In the last case, the DEVICE object must also appear on the RHS <br>
(i.e. in modification mode), it will contain the additional and separate information <br>
with respect to the liquid zone controllers. <br>
MATEX <br>
character*12 name of the matex object that will be updated by the module. The <br>
lzc-devices material mixtures are appended to the previous material index and the <br>
lzc-devices indices are also modified, accordingly. <br>
$($ desclzc)

$\quad$

structure describing the input data to the LZC: module.
\end{tabular}

3.6.1 Input data to the LZC: module

Note that the input order must be respected.

Table 16: Structure (desclzc)

```
[ EDIT iprint]
NUM-LZC nlzc
((dev-lzc), i = 1, nlzc)
    CREATE LZC-GR ngrp ((lzc-group), i = 1, ngrp)]
;
```

where
EDIT keyword used to set iprint.
iprint integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); larger values produce increasing amounts of output.

NUM-LZC keyword used to specify nlzc.
nlzc integer total number of liquid zone controllers. This number must be greater than 0 .
CREATE keyword used to create the lzc-groups of devices. The creation of groups is optional.
LZC-GR keyword used to set ngrp.
ngrp integer total number of the lzc groups to be created. This number must be greater than 0 .
(dev-lzc) structure describing the input data for each individual liquid controller.
(lzc-group) structure describing the input data for each group of liquid controllers.

### 3.6.2 Description of dev-lzc input structure

Note that the devices positions can not overlap in the reactor core. The input order of data must be respected.

Table 17: Structure (dev-lzc)

```
LZC id
MAXPOS ( pos(i), i = 1,6 )
MAX-FULL fmax
AXIS {X|Y|Z }
LEVEL value
[ RATE rate]
[ TIME time]
EMPTY-MIX(mixE(n), n = 1, 2 )
FULL-MIX( mixF(n), n = 1, 2 )
```

where

LZC
id

MAXPOS
pos

MAX-FULL keyword used to specify fmax.
fmax

AXIS

X
Y
Z
LEVEL
value

RATE
rate

TIME
time

EMPTY-MIX
$\operatorname{mixE}$

FULL-MIX keyword used to specify mixF.
$\operatorname{mixF}$ empty and full parts. Z- Z+ along only one (vertical) axis.
keyword used to specify the actual filling level.
keyword used to specify rate. for the reactor regulating purpose.
keyword used to specify time. regulating purpose.
keyword used to specify mixE. sections in the NEWMAC: module.
keyword used to specify the liquid controller id number.
integer identification number of the current liquid controller. Each controller must be assigned a unique id number, given in an ascending order ranging from 1 to nlzc.
keyword used to specify the entire position of a liquid zone controller, including its
real array containing 3-D Cartesian coordinates of the liquid zone controller position in the reactor core. These coordinates must be given in the order: $\mathrm{X}-\mathrm{X}+\mathrm{Y}-\mathrm{Y}+$
real value of the limiting coordinate along the controller filling axis, which corresponds to the maximum full-filling level for the current liquid controller.
keyword used to specify the controller filling axis. A liquid controller can be filled
keyword used to specify that a liquid controller is filled along X axis.
keyword used to specify that a liquid controller is filled along Y axis.
keyword used to specify that a liquid controller is filled along Z axis.
real positive value of the water level. This value is minimal (value $=0.0$ ) when the controller is empty, and it is maximal (value $=1.0$ ) when the controller is full-filled. For the partially filled controller the water level must be: $0.0<$ value $<1.0$
real positive value of the water filling rate, given in $\mathrm{m}^{3} / \mathrm{s}$. This value is needed only
real value of the filling time, given in sec. This value is needed only for the reactor
two integer mixture indices, specified for the empty-part of liquid controller. The first and the second mixture indices correspond to the perturbed and the reference cross sections, respectively. These indices will be used to compute the incremental cross
two integer mixture indices, specified for the full-part of liquid controller. The first and the second mixture indices correspond to the perturbed and the reference cross sections, respectively. These indices will be used to compute the incremental cross sections in the NEWMAC: module.

### 3.6.3 Description of lzc-group input structure

The partition of lzc-devices into groups is similar to that of rod-devices.

Table 18: Structure (lzc-group)

```
GROUP-ID igrp { LZC-ID [[ id ]]| ALL }
```

where
GROUP-ID keyword used to set igrp number.
igrp integer identification number of a group to be created. Each controllers group must be assigned a unique identification number, given in ascending order ranging from 1 to ngrp.

LZC-ID keyword used to set the controllers id numbers.
id integer identification numbers of the liquid controllers which belong to the same group igrp. A particular controller (or several devices) may belong to different groups, but it could not be repeated inside the same group. The total number of liquid controllers in any group must be between 1 and nlzc.

ALL keyword used to specify that all liquid controllers will belong to the same group igrp.

### 3.7 The DSET: module

The DSET: module is used to set or to update some of the devices parameters. The new parameters can be applied for the rod-type devices and/or for the liquid zone controllers, such as: the new insertion level for the rods or water filling level for the lzc-type devices, etc. It is possible to apply the new parameters to the individual user-selected devices as well as to the user-selected groups of devices. If the device (rod-insertion or lzc-filling) level is selected for the modification, then a new device position is recomputed accordingly. The DSET: module can be used to perform the device reactivity studies and also to predict the reactivity worth of the rod-devices.

The DSET: module specification is:

Table 19: Structure DSET:

```
DEVICE := DSET: DEVICE :: (descdset)
```

where
DEVICE character*12 name of the DEVICE object that will be updated by the module.
(descdset) structure describing the input data to the DSET: module.

### 3.7.1 Input data to the DSET: module

It is possible to set or to modify the parameters for several individual devices and/or for several groups of devices simultaneously.

Table 20: Structure (descdset)

```
EDIT iprint
[[ { ROD irod | ROD-GROUP irgrp | LZC ilzc | LZC-GROUP ilgrp }
[ LEVEL value ] [ SPEED speed ] [ TIME time ]
END ]]
;
```

where
EDIT keyword used to set iprint.
iprint $\quad$ integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing; larger values produce increasing amounts of output.

ROD keyword used to specify the rod irod number.
irod integer identification number of a rod to be modified. Each rod-type device has a
unique irod number, ranging from 1 to nrod, as been defined in the DEVINI: module (see Section 3.4.2).

ROD-GROUP keyword used to specify the rod-group irgrp number.
irgrp $\quad$ integer identification number of a rod-group of devices that will be modifed with the same parameters. Each rod-group has a unique irgrp number, ranging from 1 to ngrp, as been defined in the DEVINI: module (see Section 3.4.3).
keyword used to specify the liquid controller ilzc number.
ilzc
integer identification number of a liquid controller to be modified. Each lzc-type device has a unique ilzc number, ranging from 1 to nlzc, as been defined in the LZC: module (see Section 3.6.2).

LZC-GROUP keyword used to specify the lzc-group ilgrp number.
ilgrp integer identification number of a lzc-group of devices that will be modifed with the same parameters. Each lzc-group has a unique ilgrp number, ranging from 1 to ngrp, as been defined in the LZC: module (see Section 3.6.3).

LEVEL keyword used to specify a new level value.
value

SPEED
speed

TIME
time

END
real positive value of the new device level. For the rod-type devices this value must correspond to the new rod insertion level (see Section 3.4.3). For the lzc-type devices this value must correspond to the new water filling level (see Section 3.6.2). In any case, the new level value must be: $0.0 \leq$ value $\leq 1.0$
keyword used to specify a new value for speed.
real positive value of the device speed. For the rod-type devices this value must correspond to the speed of rod movement (insertion or extraction), given in $\mathrm{cm} / \mathrm{s}$. For the lzc-type devices this value must correspond to the water filling rate, given in $\mathrm{m}^{3} / \mathrm{s}$. The value of speed is required only for the reactor regulating purpose.
keyword used to specify a new value for time.
real value of time either for the rod insertion (or extraction) or for the liquid controller filling, given in sec. The value of time is required only for the reactor regulating purpose.
keyword used to indicate the end of input of the new parameters for the current device or group of devices.

### 3.8 The MOVDEV: module

The MOVDEV : module can be used for the transient simulations and reactor control studies, which are related to the time-dependent rod-devices displacement in the reactor core. The rods can be inserted into or extracted from the reactor core, at constant or at variable speed of movement. The rod positions are recomputed at every given time step of movement. The new rod positions can be computed in several ways, based on either: current time increment and movement speed; relative change in rod positions; or current rod insertion level. The MOVDEV : module allows the rod-devices to be displaced individually or simultaneously in groups.

The MOVDEV : module specification is:

Table 21: Structure MOVDEV:

```
DEVICE := MOVDEV : DEVICE :: (descmove)
```

where
DEVICE character*12 name of the DEVICE object that will be modified by the module. The rods positions are updated according to the current time step of movement.
(descmove) structure describing the input data to the MOVDEV : module.

### 3.8.1 Input data to the MOVDEV: module

It is possible to move several individual rods and/or several groups of rods simultaneously. A user must be aware that a particular device will not be displaced more than once during the same time step. Note that the input order of data to the module must be respected.

Table 22: Structure (descmove)

```
[ EDIT iprint]
DELT delt
[[ { ROD id | GROUP igrp }
{ INSR| EXTR }
{ LEVEL value | DELH delh | SPEED speed } ]]
;
```

where
EDIT keyword used to set iprint.
iprint integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); larger values produce increasing amounts of output.

| DELT | keyword used to set delt. |
| :---: | :---: |
| delt | real value of the time increment for the current time step, given in sec. |
| ROD | keyword used to specify the rod id number. |
| id | integer identification number of a rod-type device to be displaced. Each rod has a unique id number, ranging from 1 to nrod, as been defined in the DEVINI: module (see Section 3.4.2). |
| GROUP | keyword used to specify a rod-group igrp number. |
| igrp | integer number of a group of rods that will be displaced simultaneously, with the same parameters of movement. Each group of rod-devices has a unique igrp number, ranging from 1 to ngrp, as been defined in the DEVINI: module (see Section 3.4.3). |
| INSR | keyword used to specify that a particular rod or a group of rods will be inserted into the reactor core during the period of time delt. |
| EXTR | keyword used to specify that a particular rod or a group of rods will be extracted from the reactor core during the period of time delt. |
| LEVEL | keyword used to specify the new level value. |
| value | real positive value of the rod insertion level at current time step. This value will be used to compute the new rod position in the reactor core. The insertion level is minimal (value $=0.0$ ) when the rod is completely withdrawn, and it is maximal (value $=1.0$ ) when the rod is fully inserted. For the partially inserted rod the insertion level must be: $0.0<$ value $<1.0$ |
| DELH | keyword used to specify the value delh. |
| delh | real positive (absolute) value of the relative change in the rod position during the period of time delt. This is a time-dependent rod displacement along the rod movement axis, which must be given in cm . |
| SPEED | keyword used to set the current value of speed. |
| speed | real positive (absolute) value of the rod movement speed, given in $\mathrm{cm} / \mathrm{s}$. The rod speed can be kept constant or it can be modified at any time step delt. The devices could also have the different speeds of movement. |

### 3.9 The NEWMAC: module

The NEWMAC: module is used to create a complete MACROLIB with respect to the devices parameters. The resulting macrolib will contain the exact properties for every material region, over the whole meshsplitted reactor geometry. The material properties of each region are recomputed with respect to the actual position of each rod-type and if present lzc-type device. The computing algorithm is based on the determination of the volumic fraction occupied by each device; the incremental cross sections are then adjusted, accordingly. Note that the NEWMAC: module must be executed each time the devices positions are modified from the previously computed ones.

The NEWMAC: module specification is:

Table 23: Structure NEWMAC:

MACRO3 MATEX := NEWMAC: MATEX MACRO2 DEVICE : : [EDIT iprint ] [XFAC xfac ];
where
MACRO3 character*12 name of the MACROLIB to be created by the module. It will contain the updated properties of each material region with respect to the current position of each device.

MATEX character*12 name of the MATEX object, containing the complete reactor material index including devices. MATEX must be specified in the modification mode; it will store the updated h-factors, computed per each fuel region with respect to the devices positions.

MACRO2 character*12 name of the read-only extended mACROLIB, previously created by the MACINI: module.

DEVICE character*12 name of the read-only DEVICE object containing the devices information and parameters.

EDIT keyword used to set iprint.
iprint integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing; larger values produce increasing amounts of output. The default value is iprint $=1$.

XFAC keyword used to specify the number of cells on which incremental cross sections were computed in the supercell code.
xfac corrective factor for delta sigmas (real number). For DRAGON code, xfac is generally set to 2.0 and, for MULTICELL code, set to 1.0 . The default value is 2.0 .

### 3.10 The FLPOW: module

The FLPOW: module is used to compute and print the flux and power distributions over the reactor core. It also computes and prints some additional information, for example: the fluxes ratios with respect to the thermal energy-group fluxes; the mean power density; the power- and flux-form factors; etc. The computed fluxes and powers are printed either on files or on the screen. Note that the calculation using the FLPOW: module can be performed once the numerical solution has been previously established using the FLUD: or KINSOL: module.

According to the user-selected module specification, the average fluxes and powers can be computed per each fuel region over the fuel lattice and/or per each material region over the whole reactor geometry. In either case, all fluxes are normalized to the given total reactor power corresponding to the reactor nominal conditions at core equilibrium. If the reactor is perturbed from its initial state, then a new total reactor power can be recomputed and, accordingly, the flux and power distributions will be updated using the previously computed normalization factor.

The FLPOW: module will create a new POWER object that will store the information related to the reactor fluxes and powers (see Section 7.5). In addition, the POWER object will store several parameters that can be used as power and criticity constraints for the optimization and fuel management purposes, namely: the maximum channel and bundle powers; the channel and bundle power-form factors; the effective multiplication factor (recovered from the FLUX or KINET data structure).

The FLPOW: module specifications are:

Table 24: Structure FLPOW:

```
{
    POWER [ NRMFLUX ] [ FMAP ]
        := FLPOW: [ POWOLD ] FMAP { FLUX | KINET } TRACK MATEX
        :: (descflpow)
|
    POWER := FLPOW: [ POWOLD ] { FLUX | KINET } TRACK MACRO
        :: (descflpow)
}
```

where
POWER character*12 name of the POWER object that will be created by the module. It will contain the information related to the reactor fluxes and powers.

NRMFLUX character*12 name of the FLUX object, in creation mode. According to the chosen option, this object contains either the fluxes normalized to the given total reactor power or the fluxes per bundle. Is it useful if you want to compute the detectors readings with the DETECT: module.

POWOLD character*12 name of the read-only POWER object. It must contain the previously computed flux normalization factor, which corresponds to the reactor nominal or equilibrium conditions.

FMAP character*12 name of the FMAP object containing the fuel lattice specification. When FMAP is specified on the RHS, the fluxes and powers calculations are performed over
the fuel lattice as well as over the whole reactor geometry. If FMAP is specified on the LHS, its records 'BUND-PW' and 'FLUX-AV' will be set according to the information present in POWER.

FLUX character*12 name of the FLUX object, previously created by the FLUD: module. The numerical flux solution contained in FLUX is recovered and all flux are normalized to the given total reactor power.

KINET character*12 name of the KINET object, previously created by the KINSOL: module. The numerical flux solution contained in KINET is recovered.

TRACK character*12 name of the TRACK object, created by the TRIVAT: module. The information stored in TRACK is recovered and used for the average flux calculation.

MATEX character*12 name of the MATEX object, containing the reactor material index and the h -factors that will be recovered and used for the power calculation.

MACRO character*12 name of the MACROLIB object, containing the h-factors that will be recovered and used for the power calculation.
(descflpow) structure describing the input data to the FLPOW: module .

### 3.10.1 Input data to the FLPOW: module

Note that the fuel-lattice power distribution can be printed only on the screen.

Table 25: Structure (descflpow)

```
[ EDIT iprint ]
{ PTOT power | P-NEW } ]
[ FSTH fsth] [ INIT ]
{ NORM|BUND } ]
[PRINT { MAP | DISTR [ FLUX ] [ RATIO ] [ POWER ]| ALL } ]
```

where
EDIT keyword used to set iprint.
iprint
integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum editing (default value) $;=2$ only channel powers in radial plane are printed; $=3$ only bundle powers per each radial plane are printed; $=10$ only bundle powers per each channel are printed. Any combination of the values 2,3 and 10 is possible, for example $5=2+3$. Note that any other value of iprint behaves as the first lower possible value, for example 7 gives the same output as 5 . Moreover channel and bundle powers can be printed only if the FMAP object was provided in the calling specification.

PTOT keyword used to specify the input of power. By default, a power is recovered from the KINET object.
power real total reactor power, given in MW. This value must correspond to the reactor nominal conditions.

FSTH keyword to specify the thermal to fission power ratio.
fsth thermal to fission power ratio. By default this value is not used, and the total power is the one given after the PTOT keyword.

INIT keyword used to save the actual power distribution in the BUND-PW-INI record of the fuel map object FMAP. It is used by the AFM: module to apply power feedback during a fast transient using the initial power distribution instead of the actual power.

P-NEW keyword used to indicate that a new total reactor power is to be recomputed, based on the previously calculated flux normalization factor. The flux and power distributions over the reactor core are updated, accordingly. Note that this option is valid only if a read-only POWOLD object is provided.

PRINT keyword used to indicate the printing on files. Note that all produced files will have the same extension ".res".
keyword used to specify the printing of the average fluxes and flux ratios per fuel bundle. The normalized bundle fluxes are computed and printed for each reactor channel and per each energy group. The flux ratios are computed with respect to the thermal energy-group fluxes; they are printed on the same file.

DISTR keyword used to indicate the printing of data computed over the whole reactor geometry.

FLUX keyword used to specify the printing of flux distribution. The normalized fluxes are printed in separated files, one file per energy group; the number of produced files will then equal to the total number of energy groups. The flux values are printed for each mesh-splitted volume, in X, Y and Z planes; the virtual regions will have the fluxes values set to 0 .

ALL keyword used to indicate the printing of all available information, i.e. without particular selection of data. element, normalized to the given power, as required by the DETECT: module. This is the default option.
keyword to specify that the output flux object will contain a value per bundle, normalized to the given power.

### 3.11 The TAVG: module

The TAVG: module is used to compute the burnup integration limits for each fuel bundle, the axial power-shape over the fuel lattice, the channel refuelling rates and the reactor core-average exit burnup. All calculations using the TAVG: module are performed according to the time-average model for the equilibrium-core conditions. The computing algorithm is based on bidirectional refuelling schemes of channels and average exit burnups specified over the fuel lattice, which should be recorded in the fuel map using the RESINI: module.

Note that the complete time-average calculation is a complex and iterative procedure, requiring of several full-core calculations (external iterations) to be performed. The main steps of the time-average calculation using DONJON are briefly described at the end of this section. The TAVG: module can also be used to compute the instantaneous fuel burnups according to the channel patterned-age-model, for the fuel management and optimization purposes.

The TAVG: module specification is:

Table 26: Structure TAVG:

```
FMAP := TAVG: FMAP POWER :: (desctavg)
```

where
FMAP character*12 name of a FMAP object, that will be updated by the TAVG: module. The FMAP object must contain the average exit burnups and refuelling schemes of channels.

POWER character*12 name of a POWER object containing the channel and bundle powers, previously computed by the FLPOW : module. The channel and bundle powers are used by the TAVG: module to compute the normalized axial power-shape over each channel.
(desctavg) structure describing the input data to the TAVG: module.

### 3.11.1 Input data to the TAVG: module

Note that the input order must be respected.

Table 27: Structure (desctavg)

```
[ EDIT iprint]
[ AX-SHAPE [ RELAX relval ]]
[B-EXIT ]
;
```

where

| EDIT | keyword used to set iprint. <br> iprint <br> integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum <br> printing (default value); $=2$ only the burnup limits over each channel are printed; $=3$ <br> only the axial power-shape values over each channel are printed; $=4$ only the channel <br> refuelling rates are printed; for larger values of iprint everything will be printed. |
| :--- | :--- |
| AX-SHAPE | keyword used to indicate the calculation of the new axial power-shape and correspond- <br> ing burnups limits over each reactor channel. |
| RELAX | keyword used to set the relaxation parameter relval. |
| relval | real value of the relaxation parameter, generally used to control the axial-shape conver- <br> gence over the external time-average iterations. The optimal value, which corresponds <br> to the minimal total number of such iterations, can be found by performing several <br> runs at different relval. The default value of the relaxation parameter is set to 0.5 |
| B-EXIT | keyword used to indicate the calculation of the core-average exit burnup and the chan- <br> nel refuelling rates. |

### 3.11.2 Time-average calculation using DONJON

When the average exit burnups are provided for each channel, the exact burnup integration limits for each fuel bundle are unknown and need to be determined. The burnups integration limits are function of the normalized axial power-shape, which in turn depends on the flux solution over the fuel lattice. Moreover, the flux solution depends on the fuel-map macrolib (i.e. fuel properties), which in turn depends on the burnups integration limits for each fuel bundle. Consequently, the time-average calculation is an iterative procedure that consists to repeat all the steps required for the axial power-shape computation. This repetition is to be made until the relative error between the two (successives) axial power-shape calculations becomes as small as required for the precision.

The axial power-shape computing scheme is composed of several steps, each step is performed using an appropriate DONJON or TRIVAC module:

1. An initial axial power-shape is set as a flat distribution over the fuel lattice and the first burnup integration limits are calculated approximately, using the RESINI: module.
2. A time-average integration is performed and a new fuel-map macrolib is created, using either NCR:, CRE: or AFM: module.
3. An extended macrolib over the whole reactor geometry is created, using the MACINI: module.
4. If the devices are inserted into the reactor core, then the previously created macrolib is to be updated for the devices properties using the NEWMAC: module.
5. The complete mACROLIB is subsequently used by the TRIVAA: module in order to create a matrix System.
6. The full-core numerical solution (i.e. fluxes and effective multiplication factor) is computed, using the FLUD: module.
7. The channel and bundle powers are next calculated, using the FLPOW: module.
8. Finally, the new axial power-shape and burnup limits are computed, using the TAVG: module.

Note that the steps from 2 to 8 are to be repeated until the required precision for the axial power-shape convergence is satisfied.

### 3.12 The TINST: module

The TINST: module is used to compute the instantaneous burnup for each fuel bundle. You can also use TINST: to refuel your reactor, according to a refueling-scheme. The scheme can be either specified with RESINI: or directly in TINST:

The TINST: module specification is:

Table 28: Structure TINST:

```
{ FMAP := TINST: FMAP [ POWER ] |
    MICLIB3 FMAP := TINST : FMAP MICLIB2 MICLIB }
:: (desctinst)
```

where
FMAP character*12 name of a FMAP object, that will be updated by the TINST: module. The FMAP object must contain the instantaneous burnups for each fuel bundle and the weight of each fuel mixture.

POWER character*12 name of a POWER object containing the channel and bundle powers, previously computed by the FLPOW : module. The channel and bundle powers are used by the TINST: module to compute the new burn-up of each bundle. If bundle-powers are previously specified with the module RESINI: you can refuel your core without a POWER object.

MICLIB3 character*12 name of a LIBRARY object, that will be created by the TINST: module. This MICROLIB contains the fuel properties after refueling when keyword MICRO is used in (desctinst).

MICLIB2 character*12 name of a LIBRARY object, that will be read by the TINST: module. This must be a fuel-map LIBRARY created either created by the NCR: or the EVO: module.

MICLIB character*12 name of a LIBRARY object, that will be read by the TINST: module. This MICROLIB contains the new fuel properties, that should be used for the refueling.
(desctinst) structure describing the input data to the TINST: module.
3.12.1 Input data to the TINST: module

Note that the input order must be respected.

Table 29: Structure (desctinst)

```
EDIT iprint]
BURN-STEP rburn | TIME rtime { DAY| HOUR|MINUTE | SECOND }]
[[ REFUEL [ MICRO ] CHAN NAMCHA nsh ]]
[[ NEWFUEL CHAN NAMCHA nsh { SOME ( imix(i), i=1,ABS(nsh) )| ALL imix ]]
[[ SHUFF CHAN NMCHA1 TO { NMCHA2 | POOL } ]]
;
```

where

EDIT
iprint

URN-STEP
rburn
TIME
rtime
DAY
HOUR
MINUTE
SECOND
REFUEL
MICRO

CHAN key word to specify the refueled channel information.
NAMCHA channel name as defined by NXNAME and NYNAME. NAMCHA is a character*4 variable, constructed as $W \operatorname{RITE}\left(N A M C H A,^{\prime}(A 1, A 3)^{\prime}\right) N Y N A M E(1: 1), N X N A M E(1$ : $2)$.
nsh refueling scheme. The absolute value of nsh is the number of fuel bundles inserted in the channel NAMCHA. The sign of nsh define the refueling direction: positive direction is from the first to the $n k$-th bundle and negative is from the $n k$-th to the first bundle.

NEWFUEL key word to specify that a channel will be refueled with a different type of fuel.
SOME
$\operatorname{imix}(\mathrm{i}) \quad$ index number of a fuel type with respect to the values defined in module NCR:, CRE: or AFM:.

ALL key word to specify that the nsh values of fuel types will be identical to imix.

SHUFF

CHAN
NMCHA1
TO
NMCHA2
POOL
key word to specify that a specified channel will move into an other one or discharge into the pool.
key word to specify the moved channel name.
channel name as defined by NXNAME and NYNAME. It is constructed as NAMCHA. key word to specify the bundle destination.
channel name as defined by NXNAME and NYNAME. It is constructed as NAMCHA.
key word to specify that the channel referenced by NMCHA1 is discharged into the pool.

### 3.13 The SIM: module

The SIM: module can perform a sequence of operations related to fuel management in PWRs:

- simulate a refuelling and shuffling scheme and update the burnup distribution accordingly. The refuelling scheme is specified directly in SIM:.
- increase the burnup using the power available in the $P O W E R$ object and compute the final instantaneous burnup of each assembly subdivision
- modify a local parameter such as the Boron concentration in the coolant.

The SIM: module specification is:

Table 30: Structure SIM:

```
FMAP := SIM: FMAP [ POWER ]
::(descsim)
```

where
FMAP character*12 name of a FMAP object, that will be updated by the SIM: module. The FMAP object must contain the instantaneous burnups for each assembly subdivision, a basic naval-coordinate assembly layout and the weight of each assembly subdivision.

POWER character*12 name of a POWER object containing the channel and powers of the assembly subdivisions, previously computed by the FLPOW: module. The channel and powers of the assembly subdivisions are used by the SIM: module to compute the new burn-up of each assembly subdivision. If the powers of the assembly subdivisions are previously specified with the module RESINI:, you can burn your core without a POWER object.
(descsim) structure describing the input data to the SIM: module.
3.13.1 Input data to the SIM: module

Note that the input order must be respected.

Table 31: Structure (descsim)

```
[ EDIT iprint ]
[ CYCLE hcnew [ FROM hcold [BURN { indcycle | burncycle } ] ]
    [ { MAP (hx(i), i=1,lx )
        (hy(j), (hcase(i,j), i=1,lx ), j=1,ly )|
    QMAP (hx(i), i=lx/2+1,lx )
            (hy(j),(hcase(i,j), i=lx/2+1, lx ), j=ly/2+1,ly ) } ]
```

```
    [ SPEC [[ [[ asmb1 ]]
            { SET AVGB avburn | SET FUEL ifuel | FROM hcold2 AT asmb2 [ BURN { indcycle | burncycle } ] }
            ]] ]
        [ DIST-AX [[ [[ asmb1 ]]
        { SET (axn(i), i=1,nb)| FROM hcold2 AT asmb2 [ BURN { indcycle | burncycle } ] }
                    ]] ]
    [ BURN-STEP rburn | TIME rtime { DAY | HOUR|MINUTE | SECOND } ]
ENDCYCLE ]
[[ COMPARE hc1 [ BURN { indcycle1 | burncycle1 } ] hc2 [BURN { indcycle2 | burncycle2 } ]
    { DIST-BURN >> epsburn << | DIST-POWR >> epspowr << } ]]
[ SET-PARAM PNAME pvalue ]]
;
```

where
EDIT keyword used to set iprint.
iprint
integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum printing (default value); for larger values of iprint everything will be printed.

CYCLE
hcnew

FROM
hcold
BURN
indcycle integer index of the burnup step in the previous fuel cycle.
burncycle
MAP

QMAP keyword defining the assembly layout in naval-coordinate positions using quarter-core symmetry conditions. Here, the lower-right quarter is defined. The full map is reconstructed through rotations around the center.
$h x \quad$ ordered list of available character*1 prefixes for the $X$-oriented naval-coordinate positions. Values are generally chosen between A and T.
ordered list of available character*2 suffixes for the $Y$-oriented naval-coordinate positions. Values are generally chosen between 01 and 17.
character*4 identification value for the (i,j) position. Accepted values are:

- |, - or -|- for a position outside the core,
- NEW for a new assembly (at zero burnup) selected according to the fuel map specified in Sect. 3.1,
- SPC for an assembly described later in the dataset using a SPEC specification,
- or a naval-coordinate position referring to the position of an assembly in cycle hcold that is recycled in the current cycle.

SPEC keyword defining specifications related to all assemblies previously identified with the SPC keyword. If QMAP keyword has been used with SPC values, the 4 equivalent assemblies must be specified (i.e. not only the lower-right quarter assembly).
asmb1 character*3 naval-coordinate position of an assembly identified with a SPC keyword. Up to 30 coordinates can be set aside if many assemblies have the same specification.

SET
AVGB
avburn
FUEL
fuel

FROM
hcold2
AT
asmb2
DIST-AX
axn
BURN-STEP
rburn
TIME
rtime
DAY
HOUR
MINUTE
SECOND
ENDCYCLE
COMPARE
hc2
hc1 character*12 identification name of the first fuel cycle to compare.
keyword indicating that a user-defined value will be assigned to the assembly.
keyword indicating that an averaged burnup will be assigned to the assembly.
real value of the average burnup in MWd/t.
keyword indicating that a new fuel assembly will be used.
integer index of the fuel type corresponding to the new fuel assembly. Fuel type indices are those used in the RESINI : PLANE descriptions of Sect. 3.1.
keyword indicating that a value recovered from another assembly will be assigned to the current assembly.
character*12 identification name of a previous fuel cycle.
keyword indicating that the naval-coordinate position of the other assembly will be given.
character*3 naval-coordinate position of the other assembly in cycle hcold2.
keyword used to impose an axial burnup distribution to the assembly. The burnup distribution is recovered from an existing assembly or is set to user-suppled values.
real values of the axial burnup distribution.
keyword used to indicate an increase of core average burn-up.
keyword used to indicate in MWd/t the average increase of burn-up in the core.
keyword used to indicate the time of combustion at the power specified in POWER structure.
keyword used to set the time combustion value in DAY or HOUR or MINUTE or SECOND.
keyword used to specify that rtime is a number of days.
keyword used to specify that rtime is a number of hours.
keyword used to specify that rtime is a number of minutes.
keyword used to specify that rtime is a number of seconds. keyword indicating the end of data specific to the actual fuel cycle.
keyword for obtaining a CLE-2000 variable that is a measure of the discrepancy between two cycles.
character*12 identification name of the second fuel cycle to compare.

DIST-BURN keyword used to recover the discrepancy on burnup distribution in a CLE-2000 variable.
epsburn character*12 CLE-2000 variable name in which the extracted burnup discrepancy (expressed in MW-day/tonne) will be placed.

DIST-POWR keyword used to recover the relative error on power distribution in a CLE-2000 variable.
epspowr character*12 CLE-2000 variable name in which the extracted power relative error will be placed.

SET-PARAM keyword used to indicate the input (or modification) of the actual values for a parameter specified using its PNAME.

PNAME keyword used to specify PNAME.
PNAME character*12 name of a parameter.
pvalue single real value containing the actual parameter's values. Note that this value will not be checked for consistency by the module. It is the user responsibility to provide the valid parameter's value which should be consistent with those recorded in the multicompo or Saphyb database.

### 3.14 The XENON: module

The XENON : module is used to correct the Xenon distribution coming from an interpolation calculation. This module computes the new densities according to the bundle flux, and the equation providing the balance concentration of Xenon-135 :

$$
\begin{equation*}
N_{X_{e q}}=\frac{\left(Y_{I}+Y_{X}\right) \Sigma_{f} \phi}{\lambda_{X}+\sigma_{X} \phi} \tag{3.1}
\end{equation*}
$$

where

- $Y_{I}$ is the fission yield of I135
- $Y_{X}$ is the fission yield of Xe135
- $\sigma_{X}$ is the capture cross section of Xe135
- $\lambda_{X}$ is the decay constant of Xe135
- $\Sigma_{f}$ is the total fission cross section
- $\phi$ is the bundle flux

The XENON: module specification is:

Table 32: Structure XENON:

```
MICROLIB := XENON : MICROLIB [ POWER ]
::(descxenon)
```

where
MICROLIB character*12 name of a LIBRARY object, that will be updated by the XENON: module. The Xenon should be extracted in this library for the use of this module.

POWER character*12 name of a POWER object containing the bundle fluxes, previously computed by the FLPOW: module. The fluxes should be normalized to the reactor power.
(descxenon) structure describing the input data to the XENON: module.
3.14.1 Input data to the XENON: module

Note that the input order must be respected.

Table 33: Structure (descxenon)

```
[ EDIT iprint ]
```

Structure (descxenon)
continued from last page

```
[ INIT ]
```

where
EDIT keyword used to set iprint.
iprint integer index used to control the printing on screen.
INIT keyword used to indicate the initialization of the library for a recursive calculation using the XENON : module. The Xenon concentration is set to zero for all the bundles.

### 3.15 The DETECT: module

The DETECT: module is used to compute the mean flux at each detector site and the response of each detector.
The DETECT: module specifications are:

Table 34: Structure DETECT:

```
DETEC := DETECT : DETEC FLUX TRACK GEOM :: (descdetect) ;
```

where
DETEC character*12 name of the DETECT containing the detector positions and responses.
FLUX character*12 name of the FLUX containing the flux solution computed by the FLUD: or FLPOW: modules. To obtain a correct result, the best is to use a normalized flux, coming from the FLPOW: module. In this case, the fluxes are normalized to the reactor power.

TRACK character*12 name of the TRACK containing the TRIVAC tracking.
GEOM character*12 name of the GEOMETRY containing the mesh-splitting geometry created by the USPLIT: or GEO: modules.
(descdetect) structure containing the data to module DETECT: .
3.15.1 Input data to the DETECT: module

Note that the fuel-lattice power distribution can be printed only on the screen.

Table 35: Structure (descdetect)

```
EDIT iprt ] TIME dt REF kc
[ NORM vnorm ]
[ SIMEX { SPLINE | PARAB } ]
;
```

where
EDIT key word used to set iprt.
iprt index used to control the printing in module DETECT: = $=0$ for no print; $=1$ for minimum printing(default value); $=4$ for printing each detector name; $=5$ for finite element numbers and total number of finite elements for each detector.

TIME key word used to set dt.
$d t \quad$ time step between two calls to the DETECT: module.
REF key word used to set kc.
kc
index used to control the type of calculation, $=0$ for reference calculation; $=1$ normal calculation. The reference responses are used to obtain detector current responses in full power fractions.

NORM key word used to set vnorm.
value used to normalized responses of all the detectors present in DETECT.
key word used to specify that a polynomial interpolation of detector fluxes according to HQSIMEX method. This interpolation will be applied only for vanadium detectors, under NAMTYP of value VANAD_REGUL.
key word to specify that the flux at detector site will be computed with a spline method.
key word to specify that the flux at detector site will be computed with a parabolic method.

### 3.16 The CVR: module

The CVR: module is used to update the fuel-type index and the coolant densities throughout the reactor core as required for the voiding simulations. A particular core-voiding pattern is either selected from the several pre-defined patterns or directly defined by the user in an arbitrary fashion. In the last case, the user may specify the individual voided channels by indicating their identification names. The CVR: module will create a new (perturbed) FMAP object, in which the fuel-type mixtures indices are modified according to the specified core-voiding pattern. The information with respect to the relative coolant densities is required only for the subsequent interpolation of fuel properties using the NCR: module. These data will also be reordered by the CVR: module according to the specified voiding pattern and recorded as local parameter in the perturbed fuel-map object (see Section 3.1.2).

The CVR: module specification is:

Table 36: Structure CVR:

```
FMAPV := CVR: FMAP :: (descrcvr)
```

where

| FMAP | character*12 name of a read-only FMAP object, created in the RESINI : module. This <br> object must contain the non-perturbed fuel-cell properties. |
| :--- | :--- |
| FMAPV | character*12 name of a new FMAP object, that will contain the modified fuel-type <br> indices and reordered coolant densities according to the specified core-voiding pattern. |
| (descrcvr) | structure describing the input data to the CVR: module. |

3.16.1 Input data to the CVR: module

Note that the input order must be respected.

Table 37: Structure (descrcvr)

```
EDIT iprint
( MIX-FUEL mixF(i) MIX-VOID mixV (i), i = 1, nfuel )
[ DENS-COOL PNAME SET dcoolV ]
VOID-PATTERN { FULL | HALF | QUARTER | CHECKER | CHECKER-1/2 | CHECKER-1/4 |
CHAN-VOID nvoid ( YNAME(i) XNAME(i), i = 1, nvoid ) }
;
```

where
EDIT keyword used to set iprint.

| iprint | integer index used to control the printing on screen: $=0$ for no print; $=1$ for minimum <br> printing; $=2$ modified fuel indices and coolant densities are printed per bundle over <br> each channel; $=3$ modified fuel indices are printed per each radial plane; for larger <br> values of iprint everything will be printed. |
| :--- | :--- |
| MIX-FUEL | keyword used to specify mixF. <br> integer fuel-type mixture number of the non-perturbed fuel cell. This number must be <br> specified for each fuel type as been recorded in the mATEX object (see Section 3.2.1). |
| MIX-VOID | keyword used to specify mixV. |
| mixV |  |
| integer new mixture number assigned to the voided fuel cell. Note that this number |  |
| must be specified for each fuel type and it must be different from any other reactor |  |
| material mixtures. |  |

CHAN-VOID keyword used to specify the user-defined voiding pattern. Each voided channel must be identified by its YNAME name followed by its XNAME.
nvoid

YNAME

XNAME
integer total number of the voided channels. This number must be greater than 0 and less than (or equal to) the total number of reactor channels.
character*2 vertical name of the voided channel. A vertical channel name is identified by the channel row using an alphabetical letter ('A', 'B', 'C', etc). The total number of the specified Y-names must equal to the total number of voided channels nvoid.
character*2 horizontal name of the voided channel. A horizontal channel name is identified by the channel column using a numerical character (' 1 ', ' 2 ', ' 3 ', etc.). The total number of the specified X-names must equal to the total number of voided channels nvoid.

### 3.17 The HST: module

The HST: module has been designed to manage a full reactor execution in DONJON using explicit DRAGON calculations for each cell. ${ }^{[18]}$ This module saves in an HISTORY data structure the information available in BURNUP data structures generated by DRAGON. It can also read mAP data structure generated by DONJON to prepare the HISTORY data structure for a new series of cell calculations in DRAGON. The history data structure can also be used to update the map data structure. Finally, the module HST: can be used to create an initial BURNUP data structure that can be used to evolve the cell another time step in DRAGON.

The HST: module can be used to create or update an HISTORY data structure. The possible options are:

Table 38: Updating an HISTORY structure using a MAP structure

```
HISTORY := HST:[ HISTORY ] MAP [ : : [ (hstdim) ] [ GET (hstpar) ] ]
```

Table 39: Updating an HISTORY structure using a BURNUP structure

```
HISTORY := HST: [ HISTORY ] [ BURNUP ] [ : : [ (hstdim) ]
    [ GET (hstpar) ] [ CELLID icha ibun [ idfuel ] [ GET (hstpar) ] ] ]
```

It can also be used to create a BURNUP data structure from the information available on an HISTORY data structure:

Table 40: Updating a BURNUP structure using an HISTORY structure

```
BURNUP := HST: HISTORY [ :: [ (hstdim) ]
    [ PUT (hstpar)]
    CELLID icha ibun
    [ PUT { BREFL (hstbrn) (hstpar) AREFL (hstbrn) (hstpar) | [ AREFL ] (hstbrn) (hstpar)
} ] ]
```

It can also be used to update a MAP data structure from the information available on an HISTORY data structure:

Table 41: Updating an HISTORY structure using a MAP structure

```
MAP := HST: MAP HISTORY
```

where

| HISTORY | character*12 name of an HISTORY data structure. |
| :---: | :---: |
| BURNUP | character*12 name of a BURNUP data structure. |
| MAP | character*12 name of a MAP data structure. |
| (hstdim) | structure containing the dimensions for the HISTORY data structure. |
| CELLID | keyword to identify the cell for which history information is to be processed. |
| icha | channel number for which history information is to be processed. |
| ibun | bundle number for which history information is to be processed. |
| idfuel | fuel type number associated with this cell. One can associate to each fuel cell a different fuel type. By default a single fuel type is defined and it fills every fuel cell. Only the initial properties of each fuel type are saved. These properties are used for refueling. |
| GET | keyword to specify that the values of the parameters selected in (brnpar) will be read from the input stream or CLE-2000 local variables and stored on the HISTORY data structure. |
| PUT | keyword to specify that the values of the parameters selected in (brnpar) will be read from the HISTORY data structure and transferred to local CLE-2000 variables. |
| BREFL | to specify that the information to extract from the HISTORY data structure is related to the properties of the cell before refueling takes place. |
| AREFL | to specify that the information to extract from the HISTORY data base is related to the properties of the cell after refueling took place. |
| (hstbrn) | structure containing the burnup options. |
| (hstpar) | structure containing the local parameters options. |

The (hstdim) input structure is required for general dimensioning purpose. It is generally used only when creating the HISTORY data structure. However, the number of global and local parameters used in a HISTORY data structure can be increased at all time. The number of channels, bundles and the refueling scheme must be defined at the creation of the HISTORY data structure. This information can be provided manually or extracted from a MAP data structure. The general form of the (hstdim) input structure follows:

Table 42: Structure (hstdim)

```
[ EDIT iprint ]
[ DIMENSIONS [ GLOBAL nglo ] [ LOCAL nloc ] [BUNDLES nbun bunl ] [ CHANNELS ncha ] ]
```

where

EDIT
iprint

DIMENSIONS
keyword used to modify the print level iprint.
index used to control the printing in this module. It must be set to 0 if no printing on the output file is required.
keyword used to indicate that the general dimensioning of the HISTORY data structure will be modified.

| GLOBAL | keyword used to modify the number of global parameters on the HISTORY data structure. |
| :---: | :---: |
| nglo | the number of global parameters. Note that the history module will use the maximum value between the current nglob and the value, if any, defined on the HISTORY data structure. |
| LOCAL | keyword used to modify the number of local parameters on the HISTORY data structure. |
| nloc | the number of local parameters. Note that the history module will use the maximum value between the current nloc and the value, if any, defined on the HISTORY data structure. |
| BUNBLES | keyword used to specify the number of bundles per channels for the reactor model considered in the HISTORY data structure. |
| nbun | the number of bundles per channels for the reactor model. Note that if nbun is different from the value already defined on the HISTORY data structure or the MAP data structure, the execution will be aborted. |
| bunl | bundle length in cm. This information is required to compute inital fuel weight. |
| CHANNELS | keyword used to specify the number of fuel channels for the reactor model considered in the HISTORY data structure. |
| ncha | the number of fuel channels for the reactor model. Note that if ncha is different from the value already defined on the HISTORY data structure or the MAP data structure, the execution will be aborted. |

The (hstbrn) serves a unique purpose, mainly to extract from the HISTORY file the information required to process a burnup evaluation in DRAGON using the EVO: module. The information must be stored inside CLE-2000 variables. The general form of this output structure is:

Table 43: Structure (hstbrn)

## BURN period power

where
BURN keyword to indicate that burnup information follows.
period the burnup period (in days) that will be transferred to a real CLE-2000 variable.
power the power density (in $\mathrm{kW} / \mathrm{kg}$ ) that will be transferred to a real CLE-2000 variable.
The (hstpar) serves two purposes. First, it is used to define the names of the local and global parameters that may be used in our calculations as well as the values of these local parameters. In can also be used to extract from a history data structure the values of these parameters. The general form of this structure is:

Table 44: Structure (hstpar)
[[ NAMPAR valpar ]]
where
NAMPAR name of a local or global parameter to process. The parameters specified before the keyword CELLID is read will be considered global otherwise they will be considered local.
valpar real value for the local or global parameter to process. In the case where the GET option is activated, the history module will extract this parameter from the input data stream. In the case where the PUT option is activated, the history module will try to transfer this information into a real CLE-2000 variable.

### 3.17.1 Example

The history interface between the codes DRAGON and DONJON has been written as a new module in order to facilitate the access to the GANLIB utilities that manage the required hierarchical data structures. The resulting HST: module can be called both by DRAGON and DONJON.

The reactor model we will consider as an example is a $3-\mathrm{D}$ model with an $x=3, y=3$ and $z=3$ mesh. Here we will assume that the $x-y$ plane describes fuel channels. The $z$ plane will be associated with the so-called fuel bundles. This choice is somewhat arbitrary, however it is useful if the refueling takes place in a specific direction as in a CANDU reactor. Here, a 2-bundle shift fueling strategy will be considered. To each fresh fuel cell introduced in the core the HST: module will associate a unique cell number between 1 and Nc , the maximum number of cells in the reactor. Most of the information associated with the fresh fuel cells will be extracted from a DRAGON BURNUP file or defined using variable local parameters. Each fresh fuel cell inserted in the core will also be associated with a specific fuel type. Each fuel type is defined as a unique initial fuel composition. The fuel management for the reactor, including burnup and refueling will be performed by the DONJON code. Here the HST: will interact with this code via the MAP data structure. Typically, each cell in the reactor will be burned inside DRAGON using the power provided in the AX-SHAPE record and the depletion time provided in the BURNUP-BEG record stored in the MAP structure. When refueling takes place some of the fuel cells will be extracted, other will be displaced from one position to another and finally new fresh fuel cells inserted. The fresh fuel cells properties will be extracted from the fuel types properties available on the HISTORY data structure.

In a coupled DRAGON/DONJON execution, the HST: module will be called at various points and for various reasons. The first call to HST : can be performed using:

```
MODULE HST: ;
*----
* Map data structure for initialization: MAPO
* History data structure : History
*----
SEQ_ASCII MAPO ;
XSM_FILE History ;
XSM_FILE Reseau ;
*----
* Reactor parameters
```

```
* ncha = nunber of channels = 9
* nbun = nunber of bundles = 3
* nevo = nunber of evolution = 3
* nglo = nunber of global parameters = 1
* nloc = nunber of local parameters = 2
* bunl = bundle length in cm = 49.53 cm
*----
INTEGER ncha nbun nevo nglo nloc :=
9 3 3 1 2 ;
REAL bunl := 49.53 ;
*----
* Initialize History using MAPO
*----
Reseau := MAPO ;
History := HST: Reseau ::
DIMENSIONS GLOBAL <<nglo>> LOCAL <<nloc>>
BUNDLES <<nbun>> <<bunl>>
CHANNELS <<ncha>> ;
```

Here, the history data structure will be stored in the XSM file History. One global and two local parameters are considered. No information about the name or the value of the global and local parameters will be available. This initialization procedure stores information only on the main level of the history data structure if the MAP data structure is not available. In this case the history is updated using a MAP data structure (in sequential ASCII file MAPO). The number of channels and bundles per channel are stored and compared with the same information in the MAP structure. For each bundle in the MAP, cell type and fuel type directories are constructed. The bundle powers and burnups available in MAP are used to generate the power rates in $\mathrm{kW} / \mathrm{kg}$ and the depletion time in days required to reach the specified burnups. These values are stored in the history in the Paramburntar record. The fuel mass is mandatory for such calculation, thus the fuel weight is recovered from the map. If the history is in modification mode, the fuel weight is computed using the bundle lenght and the initial fuel density. Now, let us assume that a DRAGON calculation was performed for the cell located in bundle $j=1$ of channel $i=1$. We will also assume that these cells contain a single type of fuel. Here the moderator temperature TMod is a global parameter while the fuel (TComb) and coolant (TCalo) temperatures are considered local parameters. We assume that after the cell flux calculation a burnup data structure was generated using the following instructions:

```
*----
* Procedures for cell calculation: CellCalc
*----
PROCEDURE CellCalc ;
*----
* Global parameter: Tmod for moderator temperature
* Local parameters: TComb for fuel temperature
* TCalo for coolant temperature
*----
REAL TMod := 345.66 ;
REAL TComb TCalo := 941.29 560.66 ;
*----
* Initial burnup options for cell calculation
*----
REAL Power DeltaT := 31.9713 5.0 ;
*----
* Local data structures
*----
```

```
LINKED_LIST Burnup Edition ;
*----
* Execution control parameters
* icha = channel number = 1
* ibun = bundle number = 1
*----
INTEGER icha ibun := 1 1 ;
*----
* Perform cell calculation
*----
Burnup Edition := CellCalc Burnup ::
<<TComb>> <<TCalo>> <<TMod>>
<<Power>> <<DeltaT>> ;
```

Then, assuming that the history structure HistXSM was created using the options above, we can use

```
*----
* Update history structure
*----
History := HST: History Burnup ::
GET TMod <<TMod>>
CELLID <<icha>> <<ibun>>
GET TComb <<TComb>> TCalo <<TCalo>> ;
```

where no idfuel is given (see Table 39), thus we have used the default value for idfuel=1 to store in HISTORY the general information associated with fuel channel 1 and bundle 1. Here, the initial properties associated with fuel type 1 will be generated from the initial isotope densities in the BURNUP. For the CELLID, here $i$ cha $=1$ and $i$ bun $=1$, the burnup information, isotope densities, depletion parameters and initial fuel density are stored in a /celldir/ directory. Moreover the power rate $31.9713 \mathrm{~kW} / \mathrm{kg}$ and the depletion time 5.0 days are kept in the PARAMBURNTAR record.

A HISTORY data structure that contains the initial cell information can be updated using a map data structure:
*----

* Map data structure for refueling: MAP1

```
*----
```

SEQ_ASCII MAP1 ;
*----

* Refuel
*----
Reseau := MAP1 ;
History := HST: History Reseau ;

Here, new burnup power ratings will be stored in the HISTORY data structure reflecting the power distribution in the DONJON calculation. The refueling information available in the MAP structure will also be used to redistribute the fuel in the HISTORY structure at various cell location.

Finally the last option is to recover this information in DRAGON to perform a new series of cell calculations:

```
*----
* Local parameters
* Initial burnup options for cell calculation
* *A is after refueling
* *B is before refueling
*----
```

```
REAL TCombA TCaloA TCombB TCaloB ;
REAL PowerA DeltaTA PowerB DeltaTB ;
Burnup := HST: History ::
PUT TMod >>TMod<<
CELLID <<icha>> <<ibun>>
PUT BREFL BURN >>DeltaTB<< >>PowerB<<
TComb >>TCombB<< TCalo >>TCaloB<<
AREFL BURN >>DeltaTA<< >>PowerA<<
TComb >>TCombA<< TCalo >>TCaloA<< ;
IF DeltaTB 0.0 > THEN
*----
* Burn before refueling
*----
Burnup Edition := CellCalc Burnup ::
<<TCombB>> <<TCaloB>> <<TMod>>
<<PowerB>> <<DeltaTB>> ;
Edition := DELETE: Edition ;
ENDIF ;
*----
* Burn after refueling
*----
Burnup Edition := CellCalc Burnup ::
<<TCombA>> <<TCaloA>> <<TMod>>
<<PowerA>> <<DeltaTA>> ;
*----
* Update History
*----
History := HST: History Burnup ::
CELLID <<icha>> <<ibun>> ;
```

Note that here, there are two sets of local parameters that can be extracted from the history data structure, namely the before (BREFL) and the after (AREFL) refueling information. In the case of fresh fuel (single fuel description or a refueled bundle) extracting the before information is not required. However, if one uses the general procedure described above to extract the before and after information, one will be able to identify the new fuel bundles as well as the bundle that have not been moved in the core by the fact that $\Delta t=0$ for burnup before refueling. For bundles that have been displaced in the core during refueling then $\Delta t>0$.

## 4 CROSS-SECTION INTERPOLATION MODULES

### 4.1 The CRE: module

The CRE: module is used for the recovering and interpolation of nuclear properties from one or many COMPO objects, originated from the transport calculations using lattice code DRAGON. A resulting macrolib will be created (or updated) by the CRE: module, it will contain the nuclear properties of some selected reactor materials.

Two types of macrolib can be constructed using the CRE: module:

- A macrolib that will be constructed for the few reactor materials, namely for the devices and/or reflector properties. It can also be created for the few fuel regions defined in the reactor core. This MACROLIB is permitted to be updated for the new properties in the subsequent calls to the CRE: module.
- A fuel-map macrolib that will be constructed over the fuel lattice only. This macrolib will contain a set of interpolated fuel properties with respect to the burnup distribution over the fuel lattice and according to the interpolation option defined in the FMAP object. The total number of mixtures in the resulting MACROLIB will equal to the total number of fuel bundles.

Note that the CRE: module can be used only with the mono-parameter COMPO objects and the nuclear properties can be interpolated only with respect to the burnup data. In case of the macrolib construction from a multi-parameter database, the NCR: module should be used instead. In this case, the interpolation of nuclear properties can be made with respect to global and local parameters, if they were previously specified in the fuel-map (see Section 3.1.2).

The CRE: module specifications are:

Table 45: Structure CRE:

```
{ MACRO := CRE: [ MACRO ] [[ CPO ]] :: (desccre1) |
    MACFL := CRE: [[ CPO ]] FMAP :: (desccre2) }
```

where
MACRO character*12 name of the MACROLIB object to be created or updated for the few reactor material properties. Note that if $M A C R O$ appears on the RHS, the information previously stored in MACRO is kept.

CPO character*12 name of the COMPO object containing the mono-parameter database from transport calculations.

MACFL character*12 name of the fuel-map MACROLIB that will be created only for the fuel properties over the fuel lattice.

FMAP character*12 name of the FMAP object containing the fuel-map specification and burnup informations.
(desccre1) structure describing the input data to the CRE: module when the FMAP object is not specified.
(desccre2) structure describing the input data to the CRE: module for the fuel-map MACROLIB construction.

### 4.1.1 Input data for the CRE: module

Table 46: Structure (desccre1)

```
[ EDIT iprint]
[ NMIX nmix ]
READ [[ COMPO CPO (descdata1) ]]
;
```

Table 47: Structure (desccre2)

```
[ EDIT iprint]
READ [[ TABLE CPO (descdata2) ]]
;
```

where

EDIT
iprint integer index used to control the printing of information on screen: $=0$ for no print; $=1$ for minimum printing; larger values will produce increasing amounts of output.

NMIX keyword used to define the number of material mixtures nmix. This data must be given only if MACRO is created and the FMAP object is not specified.
nmix integer maximum number of reactor material mixtures, as defined in the reactor geometry.

READ keyword used to read the MACROLIB specification from the input data file.
COMPO keyword used to indicate a simple MACROLIB creation, i.e. according to the first calling specification when FMAP object is not specified.

TABLE keyword used to indicate a fuel-map mACROLIB creation, i.e. according to the second calling specification with FMAP object specified.

CPO character*12 name of the selected COMPO object. This name must appear in the calling specification to the CRE: module.
(descdata1) structure containing the interpolation specification if COMPO is the selected option.
(descdata2)
keyword used to set iprint. structure containing the interpolation specification if TABLE is the selected option.

Table 48: Structure (descdata1)

```
[[ MIX mix NAMDIR [ DERIV ] [ UPS ]
    [{ I-BURNUP burn | T-BURNUP burn0 burn1 } ]
    [ MICRO { [[ HISO { conc|* } ]]| ALL } ]
ENDMIX ]]
```

Table 49: Structure (descdata2)

```
[[ MIX mix NAMDIR [ DERIV ] [ UPS ]
    [ { TIMAV-BURN | INST-BURN | AVG-EX-BURN ivarty } ]
    [ MICRO { [[ HISO { conc |* } ]]| ALL } ]
ENDMIX ]]
```

where
MIX keyword used to set the material mixture mix.
mix

NAMDIR

DERIV

UPS
TIMAV-BURN

INST-BURN

AVG-EX-BURN keyword used to compute the derivatives of cross-section information relative to the exit burnup of a single combustion zone. The derivatives are computed using Eq. (3.3) of Ref. 15, written as

$$
\frac{\partial \bar{\Sigma}_{x}}{\partial B_{j}^{\mathrm{e}}}=\frac{1}{B_{j}^{\mathrm{e}}\left(B_{j, k}^{\mathrm{eoc}}-B_{j, k}^{\mathrm{boc}}\right)}\left[-\int_{B_{j, k}^{\mathrm{boc}}}^{B_{j, k}^{\mathrm{eoc}}} d B \Sigma_{x}(B)+B_{j, k}^{\mathrm{eoc}} \Sigma_{x}\left(B_{j, k}^{\mathrm{eoc}}\right)-B_{j, k}^{\mathrm{boc}} \Sigma_{x}\left(B_{j, k}^{\mathrm{boc}}\right)\right]
$$

where $B_{j, k}^{\mathrm{boc}}, B_{j, k}^{\mathrm{eoc}}$, and $B_{j}^{\mathrm{e}}$ are the beginning of cycle burnup of bundle $\{j, k\}$, end of cycle burnup of bundle $\{j, k\}$ and exit burnup of channel $j$. This option is available only if TABLE is the selected option.

| ivarty | index of the combustion zone for |
| :---: | :---: |
| I-BURNUP | keyword used to perform a single interpolation and to set the burnup interpolation value burn. |
| burn | real interpolation value of the burnup, given in MW•day per tonne of initial heavy elements. |
| T-BURNUP | keyword used to perform a time-average MACROLIB evaluation between the burnup values burn0 and burn1. |
| burn0 | real initial value of the burnup, given in MW•day per tonne of initial heavy elements. |
| burn1 | real final value of the burnup, given in MW•day per tonne of initial heavy elements. |
| MICRO | keyword used to set the number densities of the extracted isotopes present in the COMPO linked list or XSM file. By default, the extracted isotopes are not added to the resulting MACROLIB. |
| HISO | character*12 name of an extracted isotope. |
| conc | user-defined real number density of the extracted isotope, given in $10^{24}$ particles per $\mathrm{cm}^{3}$. |
| * | keyword used to indicate that the number density for the isotope HISO will be recovered from the COMPO object. |
| ALL | keyword used to indicate that all the number densities are to be recovered from the compo object. |
| ENDMIX | keyword used to indicate the end of data specification for the material mixture mix. |

### 4.2 The NCR: module

This component of DONJON is dedicated to the interpolation of microlib and macrolib data from a MULTICOMPO object, the reactor database produced by COMPO: A set of global and/or local parameters are defined for each material mixture and used as multi-dimensional interpolation variables.

The calling specifications are:

Table 50: Structure (NCR:)

MLIB := NCR: [ \{ MLIB | MLIB2 \} ] CPONAM1 [[ CPONAM2 ]] [ MAPFL ] : : (ncr_data)
where
MLIB character*12 name of a MICROLIB (type L_LIBRARY) or MACROLIB (type L_MACROLIB) containing the interpolated data. If this object also appears on the RHS, it is open in modification mode and updated. A macrolib object cannot be specified on the RHS.

MLIB2 character*12 name of an optional MICROLIB object whose content is copied on MLIB.
CPONAM1 character*12 name of the LCM object containing the MULTICOMPO data structure (L_MULTICOMPO signature).

CPONAM2 character*12 name of an additional LCM object containing an auxiliary MULTICOMPO data structure (L_MULTICOMPO signature). This object is optional.

MAPFL character*12 name of the MAP object containing fuel regions description, global and local parameter information (burnup, fuel/coolant temperatures, coolant density, etc). Keyword TABLE is expected in (ncr_data).
ncr_data input data structure containing interpolation information (see Section 4.2.1).
4.2.1 Interpolation data input for module NCR:

Table 51: Structure (ncr_data)

```
[EDIT iprint ]
[ ALLX nbfuel ] [ RES ]
[ { MACRO | MICRO } ] [ { LINEAR | CUBIC } ] [ LEAK b2 ]
[ NMIX nmixt ]
{ [[ COMPO CPONAM NAMDIR (descintf) ]]
    | [[ TABLE CPONAM NAMDIR [ namburn ] (descintf) ]] }
;
```

where
EDIT keyword used to set iprint.

| iprint | index used to control the printing in module NCR: $=0$ for no print; $=1$ for minimum printing (default value). |
| :---: | :---: |
| ALLX | keyword used to register the region number of each isotope before merging. This option is useful if the same keyword has been specified in EDI: and COMPO: before. |
| nbfuel | number of fuel rings used for micro-depletion calculations. |
| RES | keyword indicating that the interpolation is done only for the microscopic cross sections and not for the isotopic densities. In this case, a RHS microlib must be defined and the number densities are recovered from it. This option is useful for micro-depletion applications. Important note: It is possible to force interpolation of some isotopic densities with RES option if these isotopes are explicitely specified with a "*" flag after MICRO keyword in descintf input data structure (see Section 4.2.2). |
| MACRO | keyword indicating that MLIB is a MACrolib (default option). |
| MICRO | keyword indicating that MLIB is a microlib. Object MLIB contains an embedded macrolib, but the CPU time required to obtain it is longer. |
| LINEAR | keyword indicating that interpolation of the multicompo uses linear Lagrange polynomials. |
| CUBIC | keyword indicating that interpolation of the multicompo uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16 (default option). |
| LEAK | keyword used to introduce leakage in the embedded macrolib. This option should only be used for non-regression tests. |
| b2 | the imposed buckling corresponding to the leakage. |
| NMIX | keyword used to define the maximum number of material mixtures. This information is required only if MLIB is created. |
| nmixt | the maximum number of mixtures (a mixture is characterized by a distinct set of macroscopic cross sections) the MACROLIB may contain. The default value is nmixt $=0$ or the value recovered from MLIB if it appears on the RHS. |
| COMPO | keyword used to set CPONAM and to define each global and local parameter. |
| TABLE | keyword used to set CPONAM and to recover some global and local parameter from a MAP object named MAPFL. |
| CPONAM | character*12 name of the LCM object containing the MULTICOMPO data structure where the interpolation is performed. This name must be set in the RHS of the (NCR:) data structure. |
| NAMDIR | access the MULTICOMPO structure of CPONAM from the sub-directory named NAMDIR. This value must be set equal to 'default' if not previously defined by a STEP UP keyword in module COMPO. |
| namburn | name of the parameter for burnup (or irradiation) in the sub-directory named NAMDIR. This value is defined if option TABLE is set and if burnup (or irradiation) is to be considered as parameter. |
| descintf | input data structure containing interpolation information relative to the MULTICOMPO data structure named CPONAM (see Section 4.2.2). |

### 4.2.2 Defining local and global parameters

If a MAP object is defined on the RHS of structure (ncr_data), and if the TABLE keyword is set, some information required to set the interpolation points is found in this object. In this case, the NCR: operator search the multicompo object for global or local parameters having an arbitrary name specified in the MAP object or set directly in this module. Note that any parameter's value set directly in this module prevails on a value stored in the MAP object.

Each instance of descintf is a data structure specified as

Table 52: Structure (descintf)

```
[[ MIX imix [ { FROM imixold | USE } ]
    [ { TIMAV-BURN | InST-BURN | AVG-EX-BURN ivarty } ]
    [[ { SET | DELTA | ADD } } [ { LINEAR| CUBIC } ] PARKEY { val1 | MAP } [ { val2 | MAP } ]
            [ REF [[ PARKEY { valref | SAMEASREF } ]] ENDREF ] ]]
    [ MICRO { ALL | ONLY } [[ HISO { conc | * } ]] ]
ENDMIX ]]
```

where

MIX
imix
FROM
imixold

USE
TIMAV-BURN

INST-BURN

AVG-EX-BURN
keyword used to set imix. Discontinuity factor information present in the Multicompo is interpolated as mixture 1 values.
index of the mixture that is to be created in the microlib and macrolib.
keyword used to set the index of the mixture in the multicompo object.
index of the mixture that is recovered in the multicompo object. By default, imixold= 1.
keyword used to set the index of the mixture in the multicompo object equal to imix.
keyword used to compute time-averaged cross-section information. This option is available only if a MAPFL object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the MAPFL object.
keyword used to compute cross-section information at specific bundle burnups. This option is available only if a MAPFL object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the MAPFL object.
keyword used to compute the derivatives of cross-section information relative to the exit burnup of a single combustion zone. The derivatives are computed using Eq. (3.3) of Ref. 15, written as

$$
\frac{\partial \bar{\Sigma}_{x}}{\partial B_{j}^{\mathrm{e}}}=\frac{1}{B_{j}^{\mathrm{e}}\left(B_{j, k}^{\mathrm{eoc}}-B_{j, k}^{\mathrm{boc}}\right)}\left[-\int_{B_{j, k}^{\mathrm{boc}}}^{B_{j, k}^{\mathrm{eoc}}} d B \Sigma_{x}(B)+B_{j, k}^{\mathrm{eoc}} \Sigma_{x}\left(B_{j, k}^{\mathrm{eoc}}\right)-B_{j, k}^{\mathrm{boc}} \Sigma_{x}\left(B_{j, k}^{\mathrm{boc}}\right)\right]
$$

where $B_{j, k}^{\mathrm{boc}}, B_{j, k}^{\mathrm{eoc}}$, and $B_{j}^{\mathrm{e}}$ are the beginning of cycle burnup of bundle $\{j, k\}$, end of cycle burnup of bundle $\{j, k\}$ and exit burnup of channel $j$. This option is available only if a MAPFL object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the MAPFL object.
ivarty index of the combustion zone for differentiation of cross-section information.

| SET | keyword used to indicate a simple interpolation at vall or an averaging between vall and val2. The result $\sigma_{\text {ref }}$ is also used as the reference value when the ADD is used. Note: see at the ending note of this section for a detailed description and examples. |
| :---: | :---: |
| DELTA | keyword used to indicate a delta-sigma calculation between val2 and val1 (i.e., $\Delta \sigma_{\text {ref }}=$ $\sigma_{\text {val2 }}-\sigma_{\text {val1 }}$ is computed). Note: see at the ending note of this section for a detailed description and examples. |
| ADD | keyword used to indicate a delta-sigma calculation between val2 and vall is added to the reference value (i.e., $\Delta \sigma=\sigma_{\mathrm{val2}}-\sigma_{\mathrm{val} 1}$ is used as contribution, $\sigma_{\mathrm{ref}}+\Delta \sigma$ or $\Delta \sigma_{\mathrm{ref}}+\Delta \sigma$ is returned). Note: see at the ending note of this section for a detailed description and examples. |
| LINEAR | keyword indicating that interpolation of the MULTICOMPO for parameter PARKEY uses linear Lagrange polynomials. It is possible to set different interpolation modes to different parameters. By default, the interpolation mode is set in Sect. 4.2.1. |
| CUBIC | keyword indicating that interpolation of the MULTICOMPO for parameter PARKEY uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16. By default, the interpolation mode is set in Sect. 4.2.1. |
| PARKEY | character*12 user-defined keyword associated to a global or local parameter to be set. |
| val1 | value of a global or local parameter used to interpolate. vall is the initial value of this parameter in case an average is required. vall can be an integer, real or string value. |
| val2 | value of the final global or local parameter. By default, a simple interpolation is performed, so that val $2=$ vall. val 2 is always a real value with val $2 \geq$ vall. |
| MAP | keyword used to indicate that the value of parameter vall or the second value for the $\Delta \sigma$ calculation is recovered from MAPFL, i.e. the MAP object containing fuel regions description. |
| REF | keyword only available together with the ADD option. It is used to set all the other variable values when a $\Delta$ contribution is performed for one variable. |
| valref | value of the reference parameter, when it is directly given by the user. Note that there is no default value. |
| SAMEASREF | keyword used to specify that the reference value will be the same as in the refence case, i.e. for the $\sigma_{\text {ref }}$ computation. |
| ENDREF | keyword only available together with the ADD option. It is used to specify that all the other variable values which are required are given. |
| MICRO | keyword used to set the number densities of some isotopes present in the MULTICOMPO object. The data statement "MICRO ALL" is used by default. |
| ALL | keyword to indicate that all the isotopes present in the multicompo object will be used in the microlib and macrolib objects. Concentrations of these isotopes will be recovered from the MULTICOMPO object or set using the "HISO conc" data statement. |
| ONLY | keyword to indicate that only the isotopes set using the "HISO conc" data statement will be used in the microlib and macrolib objects. |
| HISO | character*8 name of an isotope. |
| conc | user-defined value of the number density (in $10^{24}$ particles per $\mathrm{cm}^{3}$ ) of the isotope. |

* 

the value of the number density for isotope HISO is recovered from the multicompo object.

ENDMIX end of specification keyword for the material mixture.

### 4.2.3 Interpolation in the parameter grid

The following example corresponds to a delta-sigma computation in mixture 1 corresponding to a perturbation. Note that in this case, the MACROLIB object may content negative cross-section.

```
MACROLIB := NCR: CPO ::
    EDIT 40 NMIX 1 MACRO COMPO CPO default
    MIX 1 !(* delta sigma contribution *)
        SET 'CELL' '3D'
        DELTA 'PITCH' 0.0 1.0
    ENDMIX
;
```

When the number of parameters used for the interpolation is increased, all the lattice computations corresponding to all the combinations of parameters may not be done for computation time reasons. In this case, some approximations may be required. The choice for the SET, DELTA and ADD is then dependent of the structure of the database (i.e. how the database grid of possibilities is filled). When a MAP object containing fuel regions description is used, the problem become even more complex, because values have to be automatically changed for all bundles. In order to clarify all the different possibilities and limitations dependently of the database structure, we will use a 3 parameter case. The paramaters are referenced by 'A', 'B' and 'C'. But before we explain the different cases, we want to remind that the interpolation factors are computed on each axis seperatly.

The first case corresponds to a complete grid, represented by a gray paralepiped on Fig. 2 and 3. The figure 2 shows that the interpolated value in point $V$ can be obtained directly without map object. For time-average (TA) computation, lets assume that the parameter 'B' represents the burnup (and keep this convention for other database structure also). In this case the figure 3 shows also that the direct interpolation can be done to compute an average value between the points $V^{\prime}$ and $V$. Note that the TA burnups are stored in the MAP object, and are then recovered automatically.

The second case corresponds to a partial grid where all the lattice computations have been perfomed for several pairs of parameters, which are represented as the gray rectangles on Fig. 4 and 5. If we use the notations of Fig. 4 and 5, the best estimate interpolated values, $f$, we can get are given by:
$f=f(V) \approx f\left(V_{B}\right)+\left(f\left(V_{B A}\right)-f\left(V_{B}\right)\right)+\left(f\left(V_{B C}\right)-f\left(V_{B}\right)\right)=f\left(V_{B C}\right)+\left(f\left(V_{B A}\right)-f\left(V_{B}\right)\right)=f\left(V_{B A}\right)+$ $\left(f\left(V_{B C}\right)-f\left(V_{B}\right)\right)$ for instataneous
$f=f\left(V^{\prime}, V\right) \approx f\left(V_{B}^{\prime}, V_{B}\right)+\left(f\left(V_{B A}^{\prime}, V_{B A}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)+\left(f\left(V_{B C}^{\prime}, V_{B C}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)=f\left(V_{B C}^{\prime}, V_{B C}\right)+$ $\left(f\left(V_{B A}^{\prime}, V_{B A}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)=f\left(V_{B A}^{\prime}, V_{B A}\right)+\left(f\left(V_{B C}^{\prime}, V_{B C}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)$ for TA
where $f(.,$.$) represents the average value between two points.$
The third case corresponds to a minimal grid, where the lattice computations have been perfomed only for one parameter variation at a time. In this case, the grid is represented by the thick gray lines on the axis on Fig. 6 and 7. If we use the notations of Fig. 6 and 7, the best estimate interpolated values, $f$, we can get are given by:
$f=f(V) \approx f\left(V_{0}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)+\left(f\left(V_{B}\right)-f\left(V_{0}\right)\right)+\left(f\left(V_{C}\right)-f\left(V_{0}\right)\right)=f\left(V_{B}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)+$ $\left(f\left(V_{C}\right)-f\left(V_{0}\right)\right)$ for instataneous
$f=f\left(V^{\prime}, V\right) \approx f\left(V_{B}^{\prime}, V_{B}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)+\left(f\left(V_{C}\right)-f\left(V_{0}\right)\right)$ for TA
Note that the reference point ( $V_{0}$ in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 8 can also been used. In this case, we even have two choices for the $\Delta f$ computation on axis ' A '.

The last case is in fact a mix of cases 2 and 3 . The gray rectangle and the gray line on Fig. 9 and 10 reprensent where all the lattice computations have been performed. With the notations used on those
figures, one can write that the best estimate interpolated values, $f$, we can get are given by:
$f=f(V) \approx f\left(V_{B}\right)+\left(f\left(V_{B C}\right)-f\left(V_{B}\right)\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)=f\left(V_{B C}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)$ for instataneous $f=f\left(V^{\prime}, V\right) \approx f\left(V_{B}^{\prime}, V_{B}\right)+\left(f\left(V_{B C}^{\prime}, V_{B C}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)=f\left(V_{B C}^{\prime}, V_{B C}\right)+\left(f\left(V_{A}\right)-\right.$ $\left.f\left(V_{0}\right)\right)$ for TA
Note once again that the reference point ( $V_{0}$ in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 11 can also been used.

The input files will actually reflect the previous equations. However, they are different if the parameters are stored in a MAP object, MAPFL, or provided directly by the user. For the case of one point interpolation (i.e. instantaneous), the input files will be:

| case | all parameters explicitly set | all parameters in MAP |
| :---: | :---: | :---: |
| GRID <br> (Fig. 2) | ```MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc>> ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 ENDMIX ;``` |
| PLANE <br> (Fig. 4) | ```MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'C' <<vcO>> <<vc>> REF 'A' <<va0>> 'B' <<vb>> ENDREF !or 'B' SAMEASREF ENDREF ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'C' <<vcO>> ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' SAMEASREF ENDREF !or SET 'A' <<va0>> !or ADD 'A' <<va0>> MAP !or REF 'C' <<vc0>> !or 'B' SAMEASREF ENDREF ENDMIX ;``` |
| $\begin{aligned} & \text { AXE (Fig } \\ & 6) \end{aligned}$ | ```MACROLIB := NCR: CPO :: NMIX 1 MACRO COMPO CPO default MIX 1 SET 'A' <<va0>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX``` |
| continued on next page |  |  |



Table 53: NCR inputs for instantaneous cases
For the TA, the burnup variable has no other choice than to be stored in the MAP object, MAPFL. Then the input files will be:

| case | only the burnup in MAP | all parameters in MAP |
| :---: | :---: | :---: |
| GRID <br> (Fig. 3) | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vc>> ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 ENDMIX ;``` |
| PLANE <br> (Fig. 5) | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vc0>> ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' SAMEASREF ENDREF ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'C' <<vc0>> ADD 'C' <<vcO>> MAP REF 'A' <<va0>> 'B' SAMEASREF ENDREF !or SET 'A' <<va0>> !or ADD 'A' <<va0>> MAP !or REF 'C' <<vc0>> !or 'B' SAMEASREF ENDREF ENDMIX ;``` |


| case | only the burnup in MAP | all param. in MAP |
| :---: | :---: | :---: |
| AXE (Fig. <br> 7) | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRD TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;``` |
| PLANE + AXE (Fig. 10) | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRO TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX ;``` | ```MACROLIB := NCR: CPO FMAP :: NMIX 1 MACRD TABLE CPO default 'B' MIX 1 SET 'A' <<va0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX ;``` |

Table 54: NCR inputs for TA cases

The following pictures correspond to the previous different examples:


Figure 2: Complete grid, one point case


Figure 3: Complete grid, TA case


Figure 4: Partial grid, complete planes, one point case


Figure 5: Partial grid, complete planes, TA case


Figure 6: Partial grid, complete axis, one point case


Figure 7: Partial grid, complete axis, TA case


Figure 8: Partial grid, complete axis with another configuration, one point case


Figure 9: Partial grid, one complete plane and one complete axis, one point case


Figure 10: Partial grid, one complete plane and one complete axis, TA case


Figure 11: Partial grid, one complete plane and one complete axis with another configuration, one point case

### 4.3 The SCR: module

This component of DONJON is dedicated to the interpolation of MACROLIB data from a SAPHYB object, the reactor database produced by module SAP : in DRAGON or by module SAPHYB: in APOLLO2. ${ }^{[24]}$ A set of global parameters are defined for each material mixture and used as multi-dimensional interpolation variables.

The calling specifications are:

Table 55: Structure (SCR:)

```
MLIB := SCR: [ { MLIB | MLIB2 } ] SAPNAM1 [[ SAPNAM2 ]] [ MAPFL ] ::(scr_data)
```

where
MLIB character*12 name of a MICROLIB (type L_LIBRARY) or MACROLIB (type L_MACROLIB) containing the interpolated data. If this object also appears on the RHS, it is open in modification mode and updated. A macrolib object cannot be specified on the RHS.

MLIB2 character*12 name of an optional MICROLIB object whose content is copied on MLIB.
SAPNAM1 character*12 name of the LCM object containing the SAPHYB data structure (L_SAPHYB signature).

SAPNAM2 character*12 name of an additional LCM object containing an auxiliary SAPHYB data structure (L_SAPHYB signature). This object is optional.

MAPFL character*12 name of the MAP object containing fuel regions description, global parameter information (burnup, fuel/coolant temperatures, coolant density, etc). Keyword TABLE is expected in (scr_data).
scr_data input data structure containing interpolation information (see Section 4.3.1).
Note: SAPHYB files generated by APOLLO2 don't have a signature. If such a SAPHYB is given as input to module SCR: a signature must be included before using it. The following instruction can do the job:

```
Saphyb := UTL: Saphyb :: CREA SIGNATURE 3 = 'L_SA' 'PHYB' , ' ;
```

4.3.1 Interpolation data input for module SCR:

Table 56: Structure (scr_data)

```
EDIT iprint ]
[ MEMORY ]
[RES ]
[ { MACRO| MICRO } ] [ { LINEAR | CUBIC } ] [ LEAK b2 ] [EQUI TEXT4 ]
[ NMIX nmixt ]
{ [[ SAPHYB SAPNAM (descints) ]]| [[ TABLE SAPNAM [ namburn ] (descints) ]] }
[ (descdepl) ]
;
```

where

| EDIT | keyword used to set iprint. |
| :---: | :---: |
| iprint | index used to control the printing in module SCR: . $=0$ for no print; $=1$ for minimum printing (default value). |
| MEMORY | keyword activating a copy of the Saphyb into memory before performing interpolation. In some cases, this operation may reduce CPU resources in SCR: . |
| RES | keyword indicating that the interpolation is done only for the microscopic cross sections and not for the isotopic densities. In this case, a RHS microlib must be defined and the number densities are recovered from it. This option is useful for micro-depletion applications. Important note: It is possible to force interpolation of some isotopic densities with RES option if these isotopes are explicitely specified with a "*" flag after MICRO keyword in descints input data structure (see Section 4.3.2). |
| MACRO | keyword indicating that MLIB is a macrolib (default option). |
| MICRO | keyword indicating that MLIB is a microlib. Object MLIB contains an embedded mACrolib, but the CPU time required to obtain it is longer. |
| LINEAR | keyword indicating that interpolation of the SAPHYB uses linear Lagrange polynomials. |
| CUBIC | keyword indicating that interpolation of the SAPHYB uses the Ceschino method with cubic Hermite polynomials, as presented in Ref. 16 (default option). |
| LEAK | keyword used to introduce leakage in the embedded macrolib. This option should only be used for non-regression tests. |
| b2 | the imposed buckling corresponding to the leakage. |
| EQUI | keyword used to select a SPH factor set in the Saphyb. By default, the cross sections and diffusion coefficients are not SPH-corrected. |
| TEXT4 | character*4 user-defined keyword of the SPH factor set selected in the Saphyb. These sets are stored as local parameter information in the Saphyb. |
| NMIX | keyword used to define the maximum number of material mixtures. This information is required only if MLIB is created. |
| nmixt | the maximum number of mixtures (a mixture is characterized by a distinct set of macroscopic cross sections) the MACROLIB may contain. The default value is nmixt $=0$ or the value recovered from MLIB if it appears on the RHS. |
| SAPHYB | keyword used to set SAPNAM and to define each global parameter. |
| TABLE | keyword used to set SAPNAM and to recover some global parameter from a mAP object named MAPFL. |
| SAPNAM | character*12 name of the LCM object containing the SAPHYB data structure where the interpolation is performed. This name must be set in the RHS of the (SCR:) data structure. |
| namburn | name of the parameter for burnup (or irradiation). This value is defined if option TABLE is set and if burnup (or irradiation) is to be considered as parameter. |
| descints | input data structure containing interpolation information relative to the SAPHYB data structure named SAPNAM (see Section 4.3.2). |

(descdepl) input structure describing the depletion chain (see Section 4.3.3). This input structure requires option MICRO. By default, the depletion chain data is not written in the output MICROLIB.

### 4.3.2 Defining global parameters

If a MAP object is defined on the RHS of structure (scr_data), and if the TABLE keyword is set, some information required to set the interpolation points is found in this object. In this case, the SCR: operator search the SAPHYB object for global parameters having an arbitrary name specified in the MAP object or set directly in this module. Note that any parameter's value set directly in this module prevails on a value stored in the MAP object.

Each instance of descints is a data structure specified as

Table 57: Structure (descints)

```
[[ MIX imix [ { FROM imixold | USE } ]
    [ { TIMAV-BURN | INST-BURN | AVG-EX-BURN ivarty } ]
    [[ { SET | DELTA | ADD } } [{ LINEAR| CUBIC } ] PARKEY { val1 | MAP } [ {val2 | MAP } ]
            [ REF [[ PARKEY { valref | SAMEASREF } ]] ENDREF ] ]]
    [ MICRO { ALL | ONLY } [[ HISO { conc|* } ]] ]
ENDMIX ]]
```

where

MIX
imix
FROM
imixold
USE
TIMAV-BURN

INST-BURN

AVG-EX-BURN keyword used to compute the derivatives of cross-section information relative to the exit burnup of a single combustion zone. The derivatives are computed using Eq. (3.3) of Ref. 15, written as

$$
\frac{\partial \bar{\Sigma}_{x}}{\partial B_{j}^{\mathrm{e}}}=\frac{1}{B_{j}^{\mathrm{e}}\left(B_{j, k}^{\mathrm{eoc}}-B_{j, k}^{\mathrm{boc}}\right)}\left[-\int_{B_{j, k}^{\mathrm{boc}}}^{B_{j, k}^{\mathrm{eoc}}} d B \Sigma_{x}(B)+B_{j, k}^{\mathrm{eoc}} \Sigma_{x}\left(B_{j, k}^{\mathrm{eoc}}\right)-B_{j, k}^{\mathrm{boc}} \Sigma_{x}\left(B_{j, k}^{\mathrm{boc}}\right)\right]
$$

where $B_{j, k}^{\mathrm{boc}}, B_{j, k}^{\mathrm{eoc}}$, and $B_{j}^{\mathrm{e}}$ are the beginning of cycle burnup of bundle $\{j, k\}$, end of cycle burnup of bundle $\{j, k\}$ and exit burnup of channel $j$. This option is available
only if a MAPFL object is set. By default, the type of calculation (TIMAV-BURN or INST-BURN) is recovered from the MAPFL object.
ivarty index of the combustion zone for differentiation of cross-section information.

SET

DELTA

ADD

LINEAR

CUBIC
val2 value of the final global parameter. By default, a simple interpolation is performed, so that val $2=$ vall . val 2 is always a real value with val $2 \geq$ vall.
keyword used to indicate that the value of parameter vall or the second value for the $\Delta \sigma$ calculation is recovered from $M A P F L$, i.e. the MAP object containing fuel regions description.

REF keyword only available together with the ADD option. It is used to set all the other variable values when a $\Delta$ contribution is performed for one variable.
valref value of the reference parameter, when it is directly given by the user. Note that there is no default value.

SAMEASREF

ENDREF

MICRO

ALL keyword to indicate that all the isotopes present in the SAPHYB object will be used in the microlib and macrolib objects. Concentrations of these isotopes will be recovered from the SAPHYB object or set using the "HISO conc" data statement.

ONLY keyword to indicate that only the isotopes set using the "HISO conc" data statement will be used in the microlib and macrolib objects.

## HISO character*8 name of an isotope.

conc user-defined value of the number density (in $10^{24}$ particles per $\mathrm{cm}^{3}$ ) of the isotope.

* the value of the number density for isotope HISO is recovered from the SAPHYB object.

ENDMIX end of specification keyword for the material mixture.

### 4.3.3 Depletion data structure

Part of the depletion data used in the isotopic depletion calculation (the fission yields and the radioactive decay constants) is recovered from the Saphyb file. Remaining depletion data is recovered from the input data structure (descdepl). This data describes the heredity of the radioactive decay and the neutron activation chain.

Table 58: Structure (descdepl)

```
CHAIN
    [[ NAMDPL [ izae ]
        [[ reaction [ energy ] ]]
        [{ STABLE | FROM [[ { DECAY | reaction } [[ yield NAMPAR ]] ]] } ] ]]
ENDCHAIN
```

with:

CHAIN keyword to specify the beginning of the depletion chain.
NAMDPL character*12 name of an isotope (or isomer) of the depletion chain that appears as a particularized isotope of the Saphyb.
izae optional six digit integer representing the isotope. The first two digits represent the atomic number of the isotope; the next three indicate its mass number and the last digit indicates the excitation level of the nucleus ( 0 for a nucleus in its ground state, 1 for an isomer in its first exited state, etc.). For example, ${ }^{238} \mathrm{U}$ in its ground state will be represented by izae $=922380$.
reaction character*6 identification of a neutron-induced reaction that takes place either for production of this isotope, its depletion, or for producing energy. Example of reactions are following:
indicates that a radiative capture reaction takes place either for production of this isotope, its depletion or for producing energy.

N2N indicates that the following reaction is taking place:

$$
n+{ }^{A} X_{Z} \rightarrow 2 n+{ }^{A-1} X_{Z}
$$

N3N
indicates that the following reaction is taking place:

$$
n+{ }^{A} X_{Z} \rightarrow 3 n+{ }^{A-2} X_{Z}
$$

N4N indicates that the following reaction is taking place:

$$
n+{ }^{A} X_{Z} \rightarrow 4 n+{ }^{A-3} X_{Z}
$$

NP indicates that the following reaction is taking place:

$$
n+{ }^{A} X_{Z} \rightarrow p+{ }^{A} Y_{Z-1}
$$

NA
indicates that the following reaction is taking place:

$$
n+{ }^{A} X_{Z} \rightarrow{ }^{4} \mathrm{He}_{2}+{ }^{A-3} X_{Z-2}
$$

NFTOT indicates that a fission is taking place.
energy energy (in MeV ) recoverable per neutron-induced reaction of type reaction. If the energy associated to radiative capture is not explicitely given, it should be added to the energy released per fission. By default, energy=0.0 MeV.

STABLE non depleting isotope. Such an isotope may produces energy by neutron-induced reactions (such as radiative capture).

FROM indicates that this isotope is produced from decay or neutron-induced reactions.
DECAY indicates that a decay reaction takes place for its production.
yield branching ratio or production yield expressed in fraction.
NAMPAR character*12 name of the a parent isotope (or isomer) that appears as a particularized isotope of the Saphyb.

ENDCHAIN keyword to specify the end of the depletion chain.

### 4.3.4 Interpolation in the parameter grid

The following example corresponds to a delta-sigma computation in mixture 1 corresponding to a perturbation. Note that in this case, the MACROLIB object may content negative cross-section.

```
MACROLIB := SCR: SAP ::
    EDIT 40 NMIX 1 SAPHYB SAP
    MIX 1 !(* delta sigma contribution *)
        SET 'CELL' '3D'
        DELTA 'PITCH' 0.0 1.0
    ENDMIX
;
```

When the number of parameters used for the interpolation is increased, all the lattice computations corresponding to all the combinations of parameters may not be done for computation time reasons. In this case, some approximations may be required. The choice for the SET, DELTA and ADD is then dependent of the structure of the database (i.e. how the database grid of possibilities is filled). When a MAP object containing fuel regions description is used, the problem become even more complex, because values have to be automatically changed for all bundles. In order to clarify all the different possibilities and limitations dependently of the database structure, we will use a 3 parameter case. The paramaters are referenced by 'A', 'B' and 'C'. But before we explain the different cases, we want to remind that the interpolation factors are computed on each axis seperatly.

The first case corresponds to a complete grid, represented by a gray paralepiped on Fig. 2 and 3. The figure 2 shows that the interpolated value in point $V$ can be obtained directly without map object. For time-average (TA) computation, lets assume that the parameter 'B' represents the burnup (and keep this convention for other database structure also). In this case the figure 3 shows also that the direct interpolation can be done to compute an average value between the points $V^{\prime}$ and $V$. Note that the TA burnups are stored in the MAP object, and are then recovered automatically.

The second case corresponds to a partial grid where all the lattice computations have been perfomed for several pairs of parameters, which are represented as the gray rectangles on Fig. 4 and 5. If we use the notations of Fig. 4 and 5 , the best estimate interpolated values, $f$, we can get are given by:
$f=f(V) \approx f\left(V_{B}\right)+\left(f\left(V_{B A}\right)-f\left(V_{B}\right)\right)+\left(f\left(V_{B C}\right)-f\left(V_{B}\right)\right)=f\left(V_{B C}\right)+\left(f\left(V_{B A}\right)-f\left(V_{B}\right)\right)=$ $f\left(V_{B A}\right)+\left(f\left(V_{B C}\right)-f\left(V_{B}\right)\right)$ for instataneous
$f=f\left(V^{\prime}, V\right) \approx f\left(V_{B}^{\prime}, V_{B}\right)+\left(f\left(V_{B A}^{\prime}, V_{B A}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)+\left(f\left(V_{B C}^{\prime}, V_{B C}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)=f\left(V_{B C}^{\prime}, V_{B C}\right)+$ $\left(f\left(V_{B A}^{\prime}, V_{B A}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)=f\left(V_{B A}^{\prime}, V_{B A}\right)+\left(f\left(V_{B C}^{\prime}, V_{B C}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)$ for TA
where $f(.,$.$) represents the average value between two points.$
The third case corresponds to a minimal grid, where the lattice computations have been perfomed only for one parameter variation at a time. In this case, the grid is represented by the thick gray lines on the axis on Fig. 6 and 7. If we use the notations of Fig. 6 and 7, the best estimate interpolated values, $f$, we can get are given by:
$f=f(V) \approx f\left(V_{0}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)+\left(f\left(V_{B}\right)-f\left(V_{0}\right)\right)+\left(f\left(V_{C}\right)-f\left(V_{0}\right)\right)=f\left(V_{B}\right)+\left(f\left(V_{A}\right)-\right.$ $\left.f\left(V_{0}\right)\right)+\left(f\left(V_{C}\right)-f\left(V_{0}\right)\right)$ for instataneous
$f=f\left(V^{\prime}, V\right) \approx f\left(V_{B}^{\prime}, V_{B}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)+\left(f\left(V_{C}\right)-f\left(V_{0}\right)\right)$ for TA
Note that the reference point ( $V_{0}$ in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 8 can also been used. In this case, we even have two choices for the $\Delta f$ computation on axis ' A '.

The last case is in fact a mix of cases 2 and 3 . The gray rectangle and the gray line on Fig. 9 and 10 reprensent where all the lattice computations have been performed. With the notations used on those figures, one can write that the best estimate interpolated values, $f$, we can get are given by:
$f=f(V) \approx f\left(V_{B}\right)+\left(f\left(V_{B C}\right)-f\left(V_{B}\right)\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)=f\left(V_{B C}\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)$ for instataneous
$f=f\left(V^{\prime}, V\right) \approx f\left(V_{B}^{\prime}, V_{B}\right)+\left(f\left(V_{B C}^{\prime}, V_{B C}\right)-f\left(V_{B}^{\prime}, V_{B}\right)\right)+\left(f\left(V_{A}\right)-f\left(V_{0}\right)\right)=f\left(V_{B C}^{\prime}, V_{B C}\right)+\left(f\left(V_{A}\right)-\right.$ $\left.f\left(V_{0}\right)\right)$ for TA

Note once again that the reference point ( $V_{0}$ in the example) does not have to be the same for all parameters. Database structures such as represented on Fig 11 can also been used.

The input files will actually reflect the previous equations. However, they are different if the parameters are stored in a MAP object, MAPFL, or provided directly by the user. For the case of one point interpolation (i.e. instantaneous), the input files will be:

| case | all parameters explicitly set | all parameters in MAP |
| :---: | :---: | :---: |
| GRID <br> (Fig. 2) | ```MACROLIB := SCR: SAP :: NMIX 1 SAPHYB SAP MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc>> ENDMIX ;``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 ENDMIX ;``` |
| PLANE <br> (Fig. 4) | ```MACROLIB := SCR: SAP :: NMIX 1 SAPHYB SAP MIX 1 SET 'A' <<va>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' <<vb>> ENDREF !or 'B' SAMEASREF ENDREF ENDMIX ;``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'C' <<vc0>> ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' SAMEASREF ENDREF !or SET 'A' <<va0>> !or ADD 'A' <<va0>> MAP !or REF 'C' <<vc0>> !or 'B' SAMEASREF ENDREF ENDMIX ;``` |
| AXE (Fig. <br> 6) | ```MACROLIB := SCR: SAP :: NMIX 1 SAPHYB SAP MIX 1 SET 'A' <<va0>> SET 'B' <<vb>> SET 'C' <<vc0>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;``` |
|  |  | continued on next page |



Table 59: SCR inputs for instantaneous cases
For the TA, the burnup variable has no other choice than to be stored in the MAP object, MAPFL. Then the input files will be:

| case | only the burnup in MAP | all parameters in MAP |
| :---: | :---: | :---: |
| GRID <br> (Fig. 3) | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vc>> ENDMIX ;``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 ENDMIX ;``` |
| PLANE <br> (Fig. 5) | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va>> SET 'C' <<vc0>> ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' SAMEASREF ENDREF ENDMIX ;``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'C' <<vc0>> ADD 'C' <<vcO>> MAP REF 'A' <<va0>> 'B' SAMEASREF ENDREF !or SET 'A' <<va0>> !or ADD 'A' <<va0>> MAP !or REF 'C' <<vc0>> !or 'B' SAMEASREF ENDREF ENDMIX ;``` |


| case | only the burnup in MAP | all param. in MAP |
| :---: | :---: | :---: |
| AXE (Fig. <br> 7) | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc0>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vc0>> <<vc>> REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vcO>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ADD 'C' <<vcO>> MAP REF 'A' <<va0>> 'B' <<vb0>> ENDREF ENDMIX ;``` |
| PLANE + AXE (Fig. 10) | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> SET 'C' <<vc>> ADD 'A' <<va0>> <<va>> REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX ;``` | ```MACROLIB := SCR: SAP FMAP :: NMIX 1 TABLE SAP 'B' MIX 1 SET 'A' <<va0>> ADD 'A' <<va0>> MAP REF 'C' <<vc0>> 'B' <<vb0>> ENDREF ENDMIX ;``` |

Table 60: SCR inputs for TA cases

### 4.4 The AFM: module

The AFM: module is used to create an extended macrolib containing set of interpolated nuclear properties from a feedback model database. ${ }^{[20]}$ The DATABASE information are obtained by previous DRAGON calculations using module CFC: . ${ }^{[17]}$

There are two possible utilizations:

- Construction of an extended macrolib for fuel properties directly from DATABASE information with respect to local parameters contained in the fuel map object or directly input.
- Construction of an extended macrolib containing only one set of cross sections derivated from the database information. Properties can be obtained for fuel or reflector.

The calling specifications are:

Table 61: Structure AFM:

```
MACRO := AFM:[ MACRO ] DBASE [MAPFL ] :: (descafm)
```

where
MACRO character*12 name of the extended mACROLIB. The mACROLIB can be in modification mode.

DBASE character*12 name of the DATABASE object containing fuel properties with respect to local parameters.

MAPFL character*12 name of the MAP object containing fuel regions description and burnup informations. This file is only required when a MACRO is created for fuel area.
(descafm) structure containing the data to module AFM:.
4.4.1 Input data to the AFM: module

Table 62: Structure (descafm)

```
{ MAP | MCR mmix } INFOR NAMDB
DNAME ntyp ( NAMTYP(i), i=1,ntyp )
REFT ( imix(i) NAMTYP(i), i=1,ntyp )
[ EDIT iprint]
[ FIXP { INIT| pow } ]
[{ PWF| NPWF } ]
[ TFUEL tfuel ]
[ TCOOL tcool]
[ TMOD tmod ]
```

Structure (descafm)

```
[ BORON nB ]
RDCL dcool ]
RDMD dmod]
PUR purity ]
BURN bval]
{ XENON nXe| XEREF }]
{ NEP nNp| NREF } ]
SAM nSm ]
IMET imet ]
BLIN ]
```

where
MAP keyword to specify that a MACROLIB for fuel properties will be computed.
MCR keyword to specify that a MACROLIB containing only one non-zero mixture will be created.
mmix maximum number of mixtures in the macrolib.
INFOR keyword to specify the data base name.

NAMDB
DNAME
ntyp number of fuel types. For MCR option, ntyp must be 1.
NAMTYP(i)
REFT
$\operatorname{imix}(i) \quad$ fuel type index as specified for the fuel map or a non-zero mixture number for the single-property sc macrolib.

EDIT keyword used to set iprint.
index used to control the printing in module AFM: . $=0$ for no print(default value); $=1$ for minimum printing; larger values produce increasing amounts of output.
keyword used to set the power used for cross-section interpolation.
a distributed beginning-of-transient bundle power in kW is used. This power distribution has to be pre-calculated in the FLPOW: module using the INIT keyword.
uniform bundle power in kW . If this data is omitted, the reference value in the data base is used or the bundle powers present in a map. The reference value is 615 kW if none were provided at the database computation time.
keyword used to activate power bundle feedback on fuel properties using powers recovered from 'BUND-PW' record in MAPFL. This is the default option if MAP is selected.

NPWF
keyword used to desactivate PWF feedback. This is the only possible option if MCR is selected.

| TFUEL | keyword used to set tfuel. |
| :---: | :---: |
| tfuel | fuel temperature in K. If this data is omitted and the bundle powers present in a MAP, fuel temperatures are computed with respect to powers. If this data is omitted and there is no bundle power, the reference value in the data base is used, where it is 941.29 K if none were provided at the database computation time. |
| TCOOL | keyword used to set tcool. |
| tcool | coolant temperature in K. If this data is omitted, the reference value in the data base is used. The reference value is 560.66 K if none were provided at the database computation time. |
| TMOD | keyword used to set tmod. |
| tmod | moderator temperature in K . If this data is omitted, the reference value in the data base is used. The reference value is 345.66 K if none were provided at the database computation time. |
| BORON | keyword used to set $n B$. |
| $n B$ | Boron concentration in ppm. If this data is omitted, the reference value in the data base is used. The reference value is 0.0 ppm . See note below for inside equations. |
| RDCL | keyword used to set dcool. |
| dcool | coolant density in $\mathrm{g} / \mathrm{cm}^{3}$. If this data is omitted, the reference value in the data base is used. The reference value is $0.81212 \mathrm{~g} / \mathrm{cm}^{3}$ if none were provided at the database computation time. |
| RDMD | keyword used to set dmod. |
| dmod | moderator density in $\mathrm{g} / \mathrm{cm}^{3}$. If this data is omitted, the reference value in the data base is used. The reference value is $1.082885 \mathrm{~g} / \mathrm{cm}^{3}$ if none were provided at the database computation time. |
| PUR | keyword used to set purity. |
| purity | moderator purity in $\mathrm{atm} \%$. If this data is omitted, the reference value in the data base is used. The reference value is $99.911 \mathrm{~atm} \%$ if none were provided at the database computation time. |
| BURN | keyword used to set bval. This option is valid only when MCR is used and can not be omitted. |
| bval | fuel burnup in MWd/t. This value must be positive. |
| XENON | keyword used to set $n X e$. |
| $n X e$ | Xenon concentration in $10^{24} \mathrm{at} / \mathrm{cm}^{3}$. This concentration will be applied to every bundle. |
| XEREF | keyword used to specify that the Xenon concentrations as computed with DRAGON will be taken. If this option is omitted and MAP contains bundle fluxes, new Xenon concentrations will be computed and used. |
| NEP | keyword used to set $n N p$. |
| $n N p$ | Neptunium concentration in $10^{24} \mathrm{at} / \mathrm{cm}^{3}$. |

XEREF keyword used to specify that the Neptunium concentrations as computed with DRAGON will be taken. If this option is omitted and map contains bundle fluxes, new Neptunium concentrations will be computed and used.

SAM keyword used to set nSm.
nSm Samarium concentration in $10^{24} \mathrm{at} / \mathrm{cm}^{3}$. If this data is omitted, bundle concentrations as computed by DRAGON is used.

IMET keyword used to set imet.
imet interpolation type for time-average calculations. imet $=1$ : using Lagrange approximations; imet $=2$ : using spline approximations; imet $=3$ : using Hermite approximations (default value).

BLIN
keyword used to linear interpolation for burnup instead of the Lagrangian interpolation method.

Note: The concentration of boron is provided in terms of $10^{24} \mathrm{at} / \mathrm{cm}^{3}$ in the database. However, the usual units are $p p m(w t)$ of Boron. Thus, the input asks for $p p m$ of Boron $\left(n_{B}\right)$, and automatically transform the units into $10^{24} \mathrm{at} / \mathrm{cm}^{3}$ using the following equations:

$$
\begin{aligned}
\rho_{B}\left(\mathrm{~g} / \mathrm{cm}^{3}\right) & =n_{B} \cdot \rho_{\text {water }}\left(\mathrm{g} / \mathrm{cm}^{3}\right) \\
\text { and } & \\
\rho_{\text {water }}\left(\mathrm{at} / \mathrm{cm}^{3}\right) & =3 \rho_{\text {water }}\left(\text { molecule } / \mathrm{cm}^{3}\right)=\frac{3 \cdot N}{M_{\text {water }}} \rho_{\text {water }}\left(\mathrm{g} / \mathrm{cm}^{3}\right) \\
\rho_{B}\left(\mathrm{at} / \mathrm{cm}^{3}\right) & =\rho_{B}\left(\text { molecule } / \mathrm{cm}^{3}\right)=\frac{N}{M_{B}} \rho\left(\mathrm{~g} / \mathrm{cm}^{3}\right) \\
\text { thus } & \\
\rho_{B}\left(10^{24} \mathrm{at} / \mathrm{cm}^{3}\right) & =n_{B} \cdot \frac{M_{\text {water }}}{3 . M_{B}} \rho_{\text {water }}\left(10^{24} \mathrm{at} / \mathrm{cm}^{3}\right)
\end{aligned}
$$

where $M$ molar mass and $N$ the Avogadro number.
They are many options on how to use the module AFM: for its different purposes. A compact summary is presented on Tab. 63.

The Rozon correlation for fuel temperature as a function of bundle power is:

$$
T_{\text {fuel }}=T_{\text {cool }}+0.476 P+2.267 P^{2} \times 10^{-4}
$$

where $P$ is in kW and temperatures are in Kelvin.

Table 63: AFM options summary

| Option | Keywords | Parameter values |
| :---: | :---: | :---: |
| MCR | ```REFT REFT + {TFUEL, TCOOL, ...}``` | Nominal values <br> Nominal values except for specified parameters |
| TAB | REFT $\begin{aligned} & \text { REFT + \{TFUEL, TCOOL, } \\ & \ldots . .\} \\ & \hline \end{aligned}$ | Nominal values except for TFUEL parameter which is computed according to the Rozon correlation using nominal power Same as above except for specified parameters which will have a constant value |
| MAP with local parameters | REFT $\begin{aligned} & \text { REFT + \{TFUEL, TCOOL, } \\ & \text {...\} } \end{aligned}$ | Nominal values except for local parameters included in MAP <br> Same as above except for specified parameters which will have a constant value |
| MAP without <br> local parame- <br> ters  | REFT $\begin{aligned} & \text { REFT + \{TFUEL, TCOOL, } \\ & \ldots . .\} \\ & \hline \end{aligned}$ | Nominal values except for TFUEL parameter which is computed according to the Rozon correlation if power distribution is available Same as above except for specified parameters which will have a constant value |

### 4.5 The T16CPO: module

The WIMS-AECL Tape16 file is a FORTRAN sequential binary file which is used to transfer the results of a WIMS-AECL calculation to other applications. ${ }^{[25]}$ The explicit contents of this file may vary from application to application since the output of most records to this file is controlled by the user who can activate specific keywords in the WIMS-AECL input file.

The standard CPO data structure used by the code DONJON is generally generated by the cell code DRAGON. This data structure can be stored on a FORTRAN direct access binary file in the form of a hierarchical data base. There is also the possibility to keep the contents of this data structure in memory (with the same hierarchical structure) for faster access. The structure of the data base is in the form of a list of material directories which contain burnup sub-directories. Inside each of these burnup subdirectories the isotopic contents of a mixture is described and the multigroup cross sections associated with a specific isotope are stored in individual sub-directories. Note that in this database the macroscopic cross sections associated with a mixture are stored in a default isotopic sub-directory.

The interface between the Tape 16 file and the CPO data structure should be written as a new module of the code DONJON in order to facilitate the access to the GANLIB utilities which manage the hierarchical data structures. This module will be called T16CPO: The transfer of information from a Tape16 format file to a CPO data structure will require the following DONJON instructions:

The T16CPO: module specifications for creating or updating a CPO data structure from a Tape16 file are:

Table 64: Structure T16CPO:

```
DONCPO := T16CPO:[ DONCPO ] WIMS16 :: (desct16cpo) ;
```

where
DONCPO name of data structure where the output CPO is stored. This can be a new data structure or an old data structure which will be updated.
(desct16cpo) input specifications for the execution of the T16CPO: module.
; end of record keyword. This keyword is used to delimit the part of the input data stream associated the current module.

In the following dataset

```
MODULE T16CPO: ;
SEQ_BINARY WIMS16 ;
LINKED_LIST DONCPO ;
DONCPO := T16CPO: WIMS16 ::
;
```

means that that the module will read the sequential binary file WIMS16 file (in readonly mode) and create the CPO data structure DONCPO while the dataset

```
MODULE T16CPO: ;
SEQ_BINARY WIMS16 ;
LINKED_LIST DONCPO ;
```

```
DONCPO := T16CPO: DONCPO WIMS16 ::
```

. .
;
means that the data structure DONCPO will be updated. The input instructions (replaced by ... here) should indicate what part of the information located on WIMS16 should be transferred to DONCPO and in what order.

### 4.5.1 Input data for the T16CPO: module

The input data structure (desct16cpo) will take the form:

Table 65: Structure (desct16cpo)

```
[ EDIT iprint]
[ NMIX nmixt ]
[ CONDG ngcond (igc(i), i=1,ngcond )]
LIST ]
[ MIX [[ MIXNAM [ { CELLAV | REGION noreg } ]
    [ RC [ nburn ] frstrec ]
    [[ NAMPER valref npert (valper(i), frstrec(i), i=1,npert ) ]]
    [ MTMD [ valreft valrefd ] npert (valpert(i), valperd(i), frstrec(i), i=1,npert )]
    ]] ]
```

where
EDIT optional keyword used to modify the print level iprint.
iprint index used to control the printing in this module. It must be set to 0 if no printing on the output file is required while values $<10$ will print general information about each record requested on Tape16 as well as other generic information pertinent to the T16CPO: module. Finally for values of iprint $\geq 10$, additional information required for debugging will be printed. The default value is iprint $=1$.

NMIX optional keyword used to define the number of mixtures created on the CPO data structure.
nmixt the maximum number of mixtures created. The default value is nmixt=1.
CONDG optional keyword used to define the group structure for condensation. In the case where the CPO is to be updated, the information following CONDG must yield an energy group structure compatible with that already available on this data structure. If it is absent, the code will first try to use the CPO group structure (if available). Then, it will try to use the editing group structure corresponding to NGREAC on the following Tape16 record:

$$
\text { REACTION}_{ப \sqcup}, \text { FLUX }_{\square ப ப ப ப ப, ~}^{\text {, NEL }}
$$

Finally, if everything else fails, it will select the main transport group structure corresponding to NGMTR on the following Tape16 record:

$$
\text { WIMS }_{\text {பபபபபப }}, \text { CONSTANT }_{\text {பப, }} \text {, NEL }
$$

ngcond the number of condensed groups required.
ilg the last group number associated with each condensed group.
LIST keyword to specify that the complete contents of Tape16 must be listed on the output file.

MIX keyword to specify that the remaining information will be associated with mixture properties definition.

MIXNAM character*6 name of the mixture to create or update on the cpo.
optional keyword to specify that cell averaged data will be taken from Tape16. This is the default option.
optional keyword to specify that regional data will be taken from Tape16. The default option is CELLAV.
noreg region number associated with this material in Tape16.
optional keyword to specify that the cross section taken from Tape16 are at reference value. This information must be defined at least once for each mixture. It must also precede the definition of perturbation parameters.
nburn number of consecutive burnup steps associated with mixture. The default value is nburn=1. We will assume that the same number of burnup steps is also available for the nuclear properties associated with the perturbed local parameters.
frstrec first Tape16 record number associated with this mixture.
NAMPER character*2 name of the perturbation. Each perturbation is associated with a single local parameter. The values permitted for NAMPER are the following:

1. FT for fuel temperature
2. MT for moderator temperature
3. MD for moderator density
4. MP for moderator purity
5. MB for moderator boron
6. CT for coolant temperature
7. CD for coolant density
8. CP for coolant purity
9. RT for reflector temperature
10. RD for reflector density
11. RP for reflector purity

Note that these keywords are identical to those used in the Proc16 program. ${ }^{[26]}$ Here the moderator, coolant and reflector can be $\mathrm{D}_{2} \mathrm{O}, \mathrm{H}_{2} \mathrm{O}$ or any other mixture since DONJON is not aware of the compositions of these mixtures. In the case where many different Tape16 files contains the reference and the individual perturbation effects, one must first define the reference case before updating the CPO using the Tape16 files containing the perturbations.
valref reference value of the associated local parameter.
npert number of local parameter perturbations.
valper
MTMD
valreft
valrefd
npert
valpert
valperd perturbed value of the moderator density.
The explicit name of the mixtures MIXDIR that will be stored on the main CPO directory will correspond to a catenation of MIXNAM and a perturbation name and an index $i$ describing the perturbation order. It is created using the following FORTRAN instructions for the reference mixture:

```
WRITE(MIXDIR,'(A6,A6)') MIXNAM, 'RC
```

while for the $i^{\text {th }}$ perturbed state associated with $\operatorname{NAMPER}(J)$ we will use:

$$
\text { WRITE(MIXDIR, '(A6, A2, A2, I2)') MIXNAM, NAMPER }(J) \text {,' பч' }, i
$$

Finally, for the $i^{\text {th }}$ perturbed state associated with the MTMD perturbation we will use:
WRITE(MIXDIR, ' (A6, A4, I2) ') MIXNAM, 'MTMD', $i$
Typically if the (desct16cpo) structure takes the form:

## EDIT 0

NMIX 2
MIX
Candu RC 151
FT 900.021100 .0161300 .046
Maple RC 70
RP 1.010 .571
Then the first 15 cases stored on the Tape16 file will correspond to a reference CANDU fuel with burnup. The reference fuel temperature is 900.0 K . The next 15 cases are for a fuel temperature of 1100.0 K . Finally cases 46 to 60 are for a fuel temperature of 1300.0 K . The Maple mixture will have no burnup. The reference Maple cross sections correspond to case 70 , while case 71 contains the effect on the Maple fuel mixture cross sections of a $50 \%$ reduction in reflector purity. As a result we will end up with a CPO data structure which contains 5 mixtures called respectively

```
Candu_RC
Candu_FT
Candu
Maple
Maple
```

The beginning of a new case on Tape 16 will be identified by the presence of the record:
CELLAV
in a Tape16 file. Accordingly, the keyword CELLAV should be used in the WIMS-AECL run creating this file. In addition, if the REGION option is used in the T16CPO: input data structure, then it should also be used in the WIMS-AECL run creating this file.

## 5 THERMAL-HYDRAULICS MODULES

### 5.1 The THM: module

The THM: module is a simplified thermal-hydraulics module where the reactor is represented as a collection of independent channels with no cross-flow between them. Each channel is represented using 1D convection equations along the channel and 1D cylindrical equations for a single pin cell. A two-fluid homogeneous model is used. The THM : module is built around freesteam, an open source implementation of IAPWS-IF97 steam tables for light water. ${ }^{[28]}$. The THM: module works both in steady-state and in transient conditions and includes a subcooled flow boiling model based on the Jens \& Lottes correlation ${ }^{[32]}$ and on Bowring's model for two-phase homogeneous flows ${ }^{[33]}$.

The 1D thermal-hydraulics equations are solved in each channel as a fonction of two fixed inlet conditions for the coolant velocity and temperature and one fixed outlet condition for the pressure.
The THM: module specification is:

Table 66: Structure THM:

```
THERMO MAPFL := THM: [ THERMO ] MAPFL ::(descthm)
```

where
THERMO character*12 name of the THERMO object that will be created or updated by the THM: module. Object thermo contains thermal-hydraulics information set or computed by THM: in transient or in permanent conditions such as the distribution of the enthalpy, the pressure, the velocity, the density and the temperatures of the coolant for all the channels in the geometry. It also contains all the values of the fuel temperatures in transient or in permanent conditions according to the discretisation chosen for the fuel rods.

MAPFL character*12 name of the MAP object containing fuel regions description and local parameter informations.
(descthm) structure describing the input data to the THM: module.
5.1.1 Input data to the THM: module

Table 67: Structure (descthm)

```
EDIT iprint ]
[ RELAX relax ]
[ TIME caltype timestep timeiter time ]
[ FPUISS fract ] [ CRITFL cflux ]
```

```
Structure (descthm)
continued from last page
\{ CWSECT sect flow \| SPEED velocity \}
ASSMB sass nbf nbg
INLET poutlet tinlet
RADIUS r1 r2 r3 r4
\{ [ POROS poros ] [PUFR pufr ] | [ CONDF ncond (kcond \((\mathrm{k}), \mathrm{k}=0\), ncond) [ INV inv ref ] unit ] \}
[ CONDC ncond ( \(k\) cond \((\mathrm{k}), \mathrm{k}=0\), ncond) unit ]
HGAP hgap ] [ HCONV hconv ] [ TEFF wteff ]
CONV maxit1 maxit2 maxit3 ermaxt ermaxc ]
RODMESH nb1 nb2]
FORCEAVE ]
\{ BOWR | SAHA \} ]
[ SET-PARAM PNAME pvalue ]]
;
```

where
EDIT keyword used to set iprint.
iprint

RELAX
relax

TIME
caltype integer value set to control the type of calculation that will be performed by the THM module: $=0$ for steady-state $;=1$ for transient. The default value is 0 .
timestep real value set to the time step in case of a transient calculation. The default value is 0.0 .
timeiter integer value of the current time step index, used for transient calculations. The default value is 0 .
time real value of time in second, used for transient calculations. The default value is 0.0 .
FPUISS keyword used to specify the fraction of the power released in fuel. The remaining fraction is assumed to be released in coolant. The default value is 0.974.
fract real value set to the fraction $(f)$. Power densities released in coolant and fuel are computed as

$$
\begin{aligned}
& Q_{\text {cool }}=(1-f) \frac{V_{\text {cool }}+V_{\text {fuel }}}{V_{\text {cool }}} \frac{P_{\text {mesh }}}{V_{\text {mesh }}} \\
& Q_{\text {fuel }}=f \frac{V_{\text {cool }}+V_{\text {fuel }}}{V_{\text {fuel }}} \frac{P_{\text {mesh }}}{V_{\text {mesh }}}
\end{aligned}
$$

where $V_{\text {cool }}$ and $V_{\text {fuel }}$ are coolant and fuel area computed from sass, nbf, nbg, r3 and r4. The mesh power $P_{\text {mesh }}$ and volume $V_{\text {mesh }}$ are recovered from MAPFL object.

CRITFL
cflux
CWSECT
sect
flow

SPEED
velocity
ASSMB
sass
$n b f$
nbg
INLET
poutlet
tinlet
RADIUS
r1
r2
r3

## r4

POROS
poros
PUFR
pufr keyword used to specify the critical heat flux. real value set to the critical heat flux in $\mathrm{W} / \mathrm{m}^{2}$. The default value is $2.0 \times 10^{6} \mathrm{~W} / \mathrm{m}^{2}$. keyword used to specify the core coolant section and the coolant inlet flow.
real value set to the core coolant section in $\mathrm{m}^{2}$.
real value set to the coolant flow in $\mathrm{m}^{3} / \mathrm{hr}$. This value doesn't include the by-pass flow. The inlet coolant velocity in $\mathrm{m} / \mathrm{s}$ is computed as

$$
V=\frac{\text { flow }}{3600 \text { cwsect }}
$$

keyword used to specify the inlet coolant velocity.
real value set to the inlet coolant velocity in $\mathrm{m} / \mathrm{s}$.
keyword used to specify the assembly characteristics.
real value set to the assembly surface in $\mathrm{m}^{2}$. This value is equal to the square of an assembly side (including the water gap).
integer value set to the number of active fuel rods in a single assembly.
integer value set to the number of active guide tubes in a single assembly.
keyword used to specify the outlet pressure and inlet absolute temperature.
real value set to the outlet coolant pressure in Pa . The pressure along each channel is assumed to be constant and equal to poutlet in permanent conditions.
real value set to the inlet coolant absolute temperature in K.
keyword used to set the pin-cell radii.
real value set to the fuel pellet radius in m .
real value set to the internal clad rod radius in m .
real value set to the external clad rod radius in $m$.
real value set to the guide tube radius in m .
keyword used to set the oxyde porosity of fuel. Porosity affects some built-in correlations used to represent the heat conduction phenomenon in fuel.
real value set to the oxyde porosity. The default value is 0.05 .
keyword used to set the plutonium mass enrichment of fuel. Plutonium enrichment affects some built-in correlations used to represent the heat conduction phenomenon in fuel.
real value set to the plutonium mass enrichment. The default value is 0.0 .
ncond integer value set to the degree of the conductivity polynomial.
kcond real value set to the coefficient of the conductivity polynomial. ncond +1 coefficients
unit string value set to the unit of temperature $T$ in the conductivity function. Can be

CONDF

INV
inv
ref
CONDC

HGAP
hgap
HCONV
hconv

TEFF
wteff
keyword used to set the fuel thermal conductivity as a function of local fuel temperature $T_{\text {fuel }}$. Fuel conductivity is computed as

$$
\lambda_{\text {fuel }}=\sum_{k=0}^{\text {ncond }} \operatorname{kcond}(k) *\left(T_{\text {fuel }}\right)^{k}+\frac{i n v}{T_{\text {fuel }}-\text { ref }}
$$

with $\lambda_{f u e l}$ in $W / m / K$ and $T_{f u e l}$ in the selected unit (Kelvin or Celsius).
By default, built-in models are used, taking into account oxyde porosity and plutonium mass enrichment. Note that oxyde porosity and plutonium mass enrichment are ignored if this keyword is used. are expected. either CELSIUS or KELVIN.
keyword used to add an inverse term in the fuel conductivity function.
real value set to the coefficient in the inverse term of fuel conductivity. The default value is 0.0 (i.e. no inverse term).
real value set to the reference in the inverse term of fuel conductivity.
keyword used to set the clad thermal conductivity as a function of local clad temperature $T_{\text {clad }}$. Clad conductivity is computed with the following polynomial

$$
\lambda_{\text {clad }}=\sum_{k=0}^{\text {ncond }} k \operatorname{cond}(k) *\left(T_{\text {clad }}\right)^{k}
$$

with $\lambda_{\text {clad }}$ in $W / m / K$ and $T_{\text {clad }}$ in the selected unit (Kelvin or Celsius).
By default, a built-in model is used.
keyword used to set the heat exchange coefficient of the gap as a constant. By default, a built-in model is used.
real value set to the constant heat exchange coefficient of the gap in $W / m^{2} / K$.
keyword used to set the heat transfer coefficient between clad and fluid as a constant. By default, this coefficient is computed using a built-in correlation.
real value set to the constant heat transfer coefficient between clad and fluid in $W / m^{2} / K$.
keyword used to set the weighting factor in the effective fuel temperature approximation. The effective fuel temperature is used for the cross sections interpolations on fuel temperature.
real value $W_{\text {teff }}$ set to the weighting factor in the effective fuel temperature. The effective fuel temperature is computed as

$$
T_{\mathrm{eff}}^{\mathrm{fuel}}=W_{\mathrm{teff}} * T_{\text {surface }}^{\mathrm{fuel}}+\left(1-W_{\text {teff }}\right) * T_{\text {center }}^{\mathrm{fuel}}
$$

where $0 \leq W_{\text {teff }} \leq 1, T_{\text {surface }}^{\text {fuel }}$ is the temperature at the surface of the fuel pellet (K), and $T_{\text {center }}^{\text {fuel }}$ is the temperature at the center of the fuel pellet $(\mathrm{K})$.
By default, the Rowlands weighting factor $W_{\text {teff }}=\frac{5}{9}$ is used ${ }^{[35]}$.

| CONv | keyword used to set the convergence criteria for solving the conduction and the conservation equation. |
| :---: | :---: |
| maxit1 | integer value set to the maximum number of iterations for computing the conduction integral. The default value is 50 . |
| maxit2 | integer value set to the maximum number of iterations for computing the center pellet temperature. The default value is 50 . |
| maxit3 | integer value set to the maximum number of iterations for computing the coolant parameters (mass flux, pressure, enthalpy and density) in case of a transient calculation. The default value is 50 . |
| ermaxt | real value set to the maximum temperature error in K . The default value is 1 K . |
| ermaxc | real value set to the maximum relative error for parameters given by the resolution of flow conservation equations (pressure, velocity and enthalpy). The default value is $10^{-3}$. |
| RODMESH | keyword used to set the radial discretization of pin-cells. |
| nb1 | integer value set to the number of discretisation points in fuel. The default value is 5 . |
| nb2 | integer value set to the number of discretisation points in the whole pin-cell (fuel+cladding). The default value is 8 . |
| Forceave | keyword used to force the use of the average approximation during the fuel conductivity evaluation. By default, a rectangle quadrature approximation is used. |
| Bowr | keyword used to set a subcooling model based on the Jens \& Lottes correlation ${ }^{[32]}$ with the Bowring model ${ }^{[33]}$ (default option). |
| SAHA | keyword used to set a subcooling model based on the Saha-Zuber correlation ${ }^{[34]}$. This option is recommended for BWR applications. |
| SET-PARAM | keyword used to indicate the input (or modification) of the actual values for a parameter specified using its PNAME. |
| PNAME | keyword used to specify PNAME. |
| PNAME | character*12 name of a parameter. |
| pvalue | single real value containing the actual parameter's values. Note that this value will not be checked for consistency by the module. It is the user responsibility to provide the valid parameter's value which should be consistent with those recorded in the multicompo or Saphyb database. |

## 6 OPTIMIZATION MODULES

This section is related to optimization capabilities available in Donjon and based on generalized perturbation theory. ${ }^{[29,30]}$ General information about the generalized perturbation theory can be found in Sect. 5.3 of Ref. 1.

### 6.1 The DLEAK: module

The DLEAK: module is used to create a delta MACROLIB (type L_MACROLIB) with respect to leakage information. Derivatives of leakage-related information (recovered from the input macrolib) are stored in the STEP heteroneneous list components present in the output MACROLIB. Derivatives can be taken with respect to a leakage parameter itself ( $D_{g, i}$ or $\Sigma_{1, g, i}$ ) or relative to factor $\mu$ in $\mu D_{g, i}$ or $\mu \Sigma_{1, g, i}$. Note that factor $\mu$ is not a SPH factor because it multiplies only leakage-related parameters. One component of the STEP heteroneneous list is created for each value of energy group $g$ and for each value of mixture $i$.

The calling specifications are:

Table 68: Structure (DLEAK:)

```
DMACRO OPTIM := DLEAK: MACRO :: (dleak_data)
```

where
DMACRO character*12 name of a LCM object (type L_MACROLIB) containing the delta MACROLIB information. DMACRO is created by the module. A STEP heteroneneous list is present in DMACRO.

OPTIM character*12 name of a second LCM object (type L_OPTIMIZE) created by the module. Leakage-related parameters are saved in the the control variable record 'VAR-VALUE' of OPTIM object. Input data defined in Sect. 6.1.1 is also saved in OPTIM object.

MACRO character*12 name of the LCM object (type L_MACROLIB) containing the input MACROLIB.
(dleak_data) structure containing the data to module DLEAK: (see Sect. 6.1.1).
6.1.1 Data input for module DLEAK:

Table 69: Structure (dleak_data)

```
[ EDIT iprint]
TYPE { DIFF| NTOT1 }
DELTA { VALUE | FACTOR }
[ MIXMIN ibm1 ] [ MIXMAX ibm2 ]
[ GRPMIN ngr1 ] [ GRPMAX ngr2 ]
;
```

where
EDIT keyword used to set iprint.
iprint index used to control the printing in module DLEAK:.
TYPE keyword used to set the leakage parameter that is differentiated.
DIFF differentiation with respect to diffusion coefficients.
NTOT1 differentiation with respect to $P_{1}$-weighted macroscopic total cross sections.
DELTA keyword used to set the type of differentiation.
VALUE differentiation with respect to the leakage parameter itself.
FACTOR differentiation with respect to the correction factor $\mu$.
MIXMIN keyword used to set the first mixture where leakage parameters are differentiated. By default, the first mixture index is used.
ibm1 minimum mixture index where leakage parameters are differentiated.
MIXMAX keyword used to set the last mixture where leakage parameters are differentiated. By default, the total number of mixtures in $M A C R O$ is used.
ibm2 maximum mixture index where leakage parameters are differentiated.
GRPMIN keyword used to set the first energy group where leakage parameters are differentiated. By default, the first energy group index is used.
ngr1 minimum energy group index where leakage parameters are differentiated.
GRPMAX keyword used to set the last energy group where leakage parameters are differentiated. By default, the total number of energy groups in MACRO is used.
ngr2 maximum energy group index where leakage parameters are differentiated.

### 6.2 The GRAD: module

The GRAD : module is designed to perform the following tasks:

- compute the gradients of the system characteristics using solutions of direct or adjoint fixed source eigenvalue problems. Here, we assume an optimization problem with nvar control variables and with ncst constraints. The total number of system characteristics is therefore equal to ncst +1 .
- define options and parameters for the different method to solve the optimization problem. The nonlinear optimization problem can be solved as a converging sequence of linear optimization problems with a quadratic constraint of the form

$$
\sum_{i=1}^{n v a r} \omega_{i}\left(\Delta x_{i}^{(n)}\right)^{2} \leq\left(S^{(n)}\right)^{2}
$$

where $\omega_{i}$ is a weight defined after keyword CST-WEIGHT and $\Delta x_{i}^{(n)}$ is a displacement for $i-$ th control variable at iteration $(n)$. The initial value of radius $S^{(1)}$ is defined after keyword OUT-STEP-LIM.

- reduces the radius $S^{(n)}$ of the quadratic constraint.

The calling specifications are:

Table 70: Structure GRAD :

OPTIM := GRAD : [ OPTIM ] DFLUX GPT : : (grad_data)
where
OPTIM character*12 name of the OPTIMIZE object (L_OPTIMIZE signature) containing the optimization informations. Object OPTIM must appear on the RHS to be able to updated the previous values.

DFLUX character*12 name of the FLUX object (L_FLUX signature) containing a set of solutions of fixed-source eigenvalue problems.

GPT character*12 name of the GPT object (L_GPT signature) containing a set of direct or adjoint sources.
(grad_data) structure containing the data to the module GRAD: (see Sect. 6.2.1).
62.1 Data input for module GRAD:

Table 71: Structure grad_data

```
[ EDIT iprint]
```

Structure grad_data
continued from last page

```
METHOD { SIMPLEX| LEMKE | MAP | AUG-LAGRANG | PENAL-METH } ]
OUT-STEP-LIM Sr ]
OUT-STEP-EPS }\mp@subsup{\epsilon}{ext}{}][\mathrm{ [INN-STEP-EPS }\mp@subsup{\epsilon}{inn}{}
CST-QUAD-EPS \epsilonquad ]
{ MAXIMIZE|MINIMIZE } ]
STEP-REDUCT { HALF| PARABOLIC }]
VAR-VALUE ( control(i), i=1,nvar )] [ VAR-WEIGHT ( weight(i), i=1,nvar )]
VAR-VAL-MIN { ( vecmin(i), i=1,nvar )| ALL varmin ]
VAR-VAL-MAX {( vecmax(i), i=1,nvar )| ALL varmax ]
FOBJ-CST-VAL ( funct(i), i=1,ncst+1 )]
CST-TYPE ( type(i), i=1,ncst ) ] [ CST-OBJ ( cstval(i), i=1,ncst )]
CST-WEIGHT ( cstw(i), i=1,ncst )]
```

where
EDIT keyword used to set iprint.
index used to control the printing in module.

LEMKE keyword used to specify that the linear LEMKE method will be used at step one and the general LEMKE method at step two.

MAP

AUG-LAGRANG keyword used to specify that the augmented Lagrangian method will be used.
PENAL-METH keyword used to specify that the penalty method will be used.
OUT-STEP-LIM keyword used to set the initial radius of the quadratic constraint (default value is sr $=1.0$ ).
$s r \quad$ initial radius of the quadratic constraint (real).

OUT-STEP-EPS
$\epsilon_{\text {ext }}$
INN-STEP-EPS
$\epsilon_{i n n}$
CST-QUAD-EPS
$\epsilon_{\text {quad }}$
MAXIMIZE
MINIMIZE
STEP-REDUCT
HALF
PARABOLIC
VAR-VALUE
control
VAR-WEIGHT
weight
funct
CST-TYPE
type

CST-OBJ

VAR-VAL-MIN keyword to specify the minimum values of the control variables. These values can also be set in a previous call to module GRAD: .
vecmin array containing nvar real values.
varmin single real value used for all control variables.
VAR-VAL-MAX keyword to specify the maximum values of the control variables. These values can also be set in a previous call to module GRAD: .
vecmax array containing nvar real values.
varmax single real value used for all control variables.
FOBJ-CST-VAL keyword to specify the value of the objective function followed by the actual values of the constraints. These values can also be set in a previous call to module GRAD : or set in another module.
keyword used to set the tolerance of outer iteration convergence inside module PLQ: . tolerance value (real). keyword used to set the tolerance used within the SIMPLEX or LEMKE method. tolerance value (real).
keyword to set the convergence parameter epsilon4 for the radius of the quadratic constraint inside module GRAD : .
tolerance for convergence of the radius of the quadratic constraint (real).
keyword used to specify that the optimization problem will be a maximization.
keyword used to specify that the optimization problem will be a minimization (default). keyword used to define the method of the reduction of the outer step.
keyword used to specify that the step will be reduced by a factor of 2 .
keyword used to specify that the step will be reduced with the parabolic method.
keyword to specify the values of the control variables. These values can also be set in a previous call to module GRAD: or set in another module.
array containing nvar real values.
keyword to specify the values of the control variable weights in the quadratic constraint. All weights are set to 1.0 by default.
array containing nvar real values.
array containing ncst +1 real values.
keyword to specify the relation types of the constraints. These values can also be set in a previous call to module GRAD: .
array containing ncst integer values. These values are: $=-1$ for $\geq,=0$ for equalily and $=1$ for $\leq$.
keyword to specify the RHS values of the constraints. These values can also be set in a previous call to module GRAD: .
cstval array containing nest real values.
CST-WEIGHT keyword to specify the weights (or penalties) of the constraints. These weights are not used with Lemke or MAP methods. These values can also be set in a previous call to module GRAD :
cstw
array containing ncst real values.

### 6.3 The PLQ: module

The PLQ: module is used to solve the linear programming problem with a quadratic constraint. The gradients of the system characteristics are calculated with module GRAD:. The options and parameters for the different method to solve the optimization problem are also defined in module GRAD:

The calling specifications are:

Table 72: Structure PLQ:

```
OPTIM := PLQ:[ OPTIM ] :: (plq_data)
```

where
OPTIM character*12 name of the OPTIMIZE object (L_OPTIMIZE signature) containing the optimization informations. Object OPTIM must appear on the RHS to be able to updated the previous values.
(plq_data) structure containing the data to the module PLQ: (see Sect. 6.3.1).
6.3.1 Data input for module PLQ:

Table 73: Structure plq_data

```
[ EDIT iprint ]
[ WARNING-ONLY]
CALCUL-DX [ NO-STORE-OLD ]
COST-EXTRAP >> ecost << ]
CONV-TEST >> l lconv << ]
```

where
EDIT keyword used to set iprint.
iprint index used to control the printing in module.
WARNING-ONLY keyword used to specify that only a warning will be used when no valid previous decision vectors can be recall in case of error of the mathematical programming.

CALCUL-DX keyword used to specify that the new step will be calculated.
NO-STORE-OLD keyword used to specify that the old value of decision variables and gradients will not be stored in the L_OPTIMIZE/'OLD-VALUE' directory.

COST-EXTRAP keyword used to calculate the extrapolated objective constant ecost.
ecost extrapolated objective constant.
CONV-TEST keyword used to calculate if the external convergence has been reached.
$l_{\text {conv }} \quad=1$ means that external convergence has been reached; $=0$ otherwise.

## 7 DONJON DATA STRUCTURES

A brief description of each DRAGON, DONJON and TRIVAC data structures, which can be used with DONJON code, is given in Section 2.2. In this section, a detailed description of the DONJON data structures is presented.

### 7.1 Contents of /fmap/ data structure

A /fmap/ data structure is used to store fuel assembly (or bundle) map and fuel information such as powers, average fluxes, control zones, burnup or refueling scheme. The fuel bundle location are given in an embedded sub-directory which contains the records as a /geometry/ data structure. This object has a signature L_MAP; it is created using the RESINI: module.

### 7.1.1 The state-vector content

The dimensioning parameters $\mathcal{S}_{i}$, which are stored in the state vector for this data structure, represent:

- The number of fuel bundles per channel $N_{b}=\mathcal{S}_{1}$
- The number of fuel channels $N_{\mathrm{ch}}=\mathcal{S}_{2}$
- The number of combustion zones $N_{\text {comb }}=\mathcal{S}_{3}$
- The number of energy groups $N_{\mathrm{gr}}=\mathcal{S}_{4}$
- The type of interpolation with respect to burnup $I_{\text {btyp }}=\mathcal{S}_{5}$

$$
I_{\mathrm{btyp}}= \begin{cases}0 & \text { interpolation type is not provided } \\ 1 & \text { according to the time-average model } \\ 2 & \text { according to the instantaneous model }\end{cases}
$$

- The number of bundle shift. $N_{\text {sht }}=\mathcal{S}_{6}$
- The number of fuel types $N_{\text {fuel }}=\mathcal{S}_{7}$
- The number of recorded parameters $N_{\text {parm }}=\mathcal{S}_{8}$
- The total number of fuel bundles $N_{\text {tot }}=\mathcal{S}_{9}$
- The number of voided reactor channels $N_{\text {void }}=\mathcal{S}_{10}$
- The option with respect to the core-voiding pattern $I_{\text {void }}=\mathcal{S}_{11}$
$I_{\text {void }}= \begin{cases}0 & \text { voiding pattern not provided } \\ 1 & \text { full-core voiding pattern } \\ 2 & \text { half-core voiding pattern } \\ 3 & \text { quarter-core voiding pattern } \\ 4 & \text { checkerboard-full voiding pattern } \\ 5 & \text { checkerboard-half voiding pattern } \\ 6 & \text { checkerboard-quarter voiding pattern } \\ 7 & \text { user-defined voiding pattern }\end{cases}$
- The type of the geometry $F_{t}=\mathcal{S}_{12}$

$$
F_{t}= \begin{cases}7 & \text { Cartesian 3-D geometry } \\ 9 & \text { Hexagonal 3-D geometry }\end{cases}
$$

- The naval-coordinate layout used by the SIM: module $I_{\text {sim }}=\mathcal{S}_{13}$.

The number of assemblies along $X$ and $Y$ axis are given using

$$
L_{\mathrm{x}}=\frac{I_{\mathrm{sim}}}{100} \quad \text { and } \quad L_{\mathrm{y}}=\bmod \left(I_{\mathrm{sim}}, 100\right)
$$

### 7.1.2 The main /fmap/ directory

The following records and sub-directories will be found on the first level of /fmap/ directory:

Table 74: Records and sub-directories in /fmap/ data structure

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| SIGNATURE建 | C*12 |  |  | Signature of the /fmap/ data structure (SIGNA =L_MAP |
| STATE-VECTOR | I(40) |  |  | Vector describing the various parameters associated with this data structure $\mathcal{S}_{i}$ |
| FLMIX $_{\text {UUUUUUU }}$ | $\mathrm{I}\left(N_{\text {ch }}, N_{b}\right)$ |  |  | Fuel mixture indices per bundle or assembly subdivisions for each reactor channel. |
| FLMIX-INİபப | $\mathrm{I}\left(N_{\text {ch }}, N_{b}\right)$ | $I_{\text {sim }} \neq 0$ |  | Fuel mixture indices per bundle or assembly subdivisions for each reactor channel, as defined by user in RESINI: module. |
|  | $\mathrm{C}\left(N_{\text {ch }}\right) * 4$ | $I_{\text {sim }} \neq 0$ |  | identification name corresponding to the basic naval-coordinate position of an assembly, as defined by user in RESINI : module.. |
| BMIX $_{\text {பபபபபUபu }}$ | $\mathrm{I}\left(N_{x}, N_{y}, N_{z}\right)$ |  |  | Renumbered mixture indices per each fuel region over the fuel-map geometry; for the nonfuel regions these indices are set to 0 . |
| XNAME பuபuபuu $^{\text {a }}$ | $\mathrm{C}\left(N_{x}\right) * 4$ |  |  | Channel identification names with respect to their horizontal position. |
| YnAME பuபபuபu $^{\text {a }}$ | $\mathrm{C}\left(N_{y}\right) * 4$ |  |  | Channel identification names with respect to their vertical position. |
| B-ZONE butuuu $^{\text {a }}$ | $\mathrm{I}\left(N_{\text {ch }}\right)$ | $N_{\text {comb }} \geq 1$ |  | Combustion-zone indices per channel. |
| BURN-AVG ¢Uபu $^{\text {a }}$ | $\mathrm{R}\left(N_{\text {comb }}\right)$ |  | MW d | ${ }^{1}$ Average exit burnups per combustion zone. |
| BURN-INST பuப $^{\text {den }}$ | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | $I_{\text {btyp }}=2$ | MW d | ${ }^{-1}$ Instantaneous burnups per bundle or assembly subdivisions for each channel. |
| BURN-BEG_பபபu | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | $I_{\text {btyp }}=1$ | MW d | ${ }^{1}$ Low burnup integration limits according to the time-average model. |
| BURN-END $\$ Uபu & $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | $I_{\text {btyp }}=1$ | MW d | ${ }^{-1}$ Upper burnup integration limits according to the time-average model. |  |


| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| BUND-PWUUUபu | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | * | kW | Bundle-powers set in RESINI: module or recovered from L_POWER object. |
| BUND-PW-INI ${ }_{\text {U }}$ | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | * | kW | Beginning-of-transient bundle-powers recovered from L_POWER object. |
| FLUX-AV bபபபu $^{\text {den }}$ | $\mathrm{R}\left(N_{\text {ch }}, N_{b}, N_{\mathrm{gr}}\right)$ | * | $\mathrm{cm}^{-2} \mathrm{~s}^{-1}$ | The normalized average fluxes recorded per each fuel bundle and for each energy group, recovered from L_POWER object. |
| B-EXIT பuபuபu | R(1) |  | MW d t ${ }^{-1}$ | ${ }^{1}$ Core-average discharge burnup. |
| REF-SHIFT பபu | $\mathrm{I}\left(N_{\text {comb }}\right)$ |  |  | Bundle-shifts per combustion zone. A bundleshift corresponds to the number of displaced fuel bundles during the refueling operation. |
| REF-VECTORபu | $\mathrm{I}\left(N_{\text {comb }}, N_{b}\right)$ |  |  | Refueling pattern vector per combustion zone. |
| REF-SCHEME $\cup \cup$ | $\mathrm{I}\left(N_{\text {ch }}\right)$ |  |  | Refueling scheme of each channel; it corresponds to the positive or negative bundle-shift number according to the flow direction. |
| REF-RATE Uபபu $^{\text {den }}$ | $\mathrm{R}\left(N_{\text {ch }}\right)$ |  | kg d ${ }^{-1}$ | Channel refueling rates. |
| REF-CHANUபuப | $\mathrm{R}\left(N_{\text {ch }}\right)$ |  | d | Time values at which channels are refueled inside a refueling time period. |
| DEPL-TIME ¢பu $^{\text {del }}$ | R(1) |  | d | Refueling time period in days. |
| \{pshift\} | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | $N_{\text {sht }} \geq 1$ | $k W$ | The power of the bundles shifted the $i$-th time. |
| \{bshift\} | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | $N_{\text {sht }} \geq 1$ | $M W d T^{-1}$ | The burnup of the bundles shifted the $i$-th time. |
| \{ishift\} | $\mathrm{I}\left(N_{\text {ch }}, N_{b}\right)$ | $N_{\text {sht }} \geq 1$ |  | The number of shifts per bundle during refueling. |
| AX-SHAPE buıu $^{\text {a }}$ | $\mathrm{R}\left(N_{\text {ch }}, N_{b}\right)$ | $I_{\text {btyp }}=1$ |  | Normalized axial power-shape values over the fuel bundles. Equal to fuel-bundle powers divided by channel powers. |
|  | R(1) | $I_{\text {btyp }}=1$ |  | Convergence factor for the axial power-shape calculation; it is defined as a relative error between the two successives calculations. |
| GEOMAP | Dir |  |  | Sub-directory containing the embedded $3 D$ Cartesian / geometry/ of the fuel lattice. |
|  | $\operatorname{Dir}\left(N_{\text {fuel }}\right)$ |  |  | List of fuel-type sub-directories. Each component of the list is a directory containing the information relative to a single fuel type. |
| \{hcycle\} | $\operatorname{Dir}\left(N_{\text {burn }}\right)$ | $I_{\text {sim }} \neq 0$ |  | Sub-directory containing information related to a fuel cycle in a PWR. $N_{\text {burn }}$ is the number of burnup steps used during the simulation of the cycle. These burnup steps may not be of increasing values. |
| PARAM ¢Uபபuபu $^{\text {a }}$ | $\operatorname{Dir}\left(N_{\text {parm }}\right)$ | $N_{\text {parm }}>0$ |  | List of parameter-type sub-directories. Each component of the list is a directory containing the information relative to a single parameter. The total number of sub-directories corresponds to the total number of recorded parameters $N_{\text {parm }}$ (excluding burnups). |

The contents of the GEOMAP sub-directory correspond to the typical contents of the /geometry/ data structure. The dimensioning parameters $N_{x}, N_{y}$, and $N_{z}$ represent the number of volumes along the corresponding axis in the fuel-map geometry.

The shifting information records $\{$ pshift $\},\{$ bshift $\}$ and $\{$ ishift $\}$ will be composed using the following FORTRAN instructions, respectively, as

$$
\begin{aligned}
& \text { WRITE(pshift,' (A6, I2)') 'PSHIFT', ell } \\
& \text { WRITE(bshift,' (A6, I2)') 'BSHIFT', ell } \\
& \text { WRITE(ishift,' (A6, I2)') 'ISHIFT', ell }
\end{aligned}
$$

for $1 \leq e l l \leq N_{\text {sht }}$.
Each time a bundle is shifted and stay in the reactor, its burnup and power will be saved in the records \{bshift $\}$ and $\{$ pshift $\}$. For example, $\{$ bshift i $\}$ and $\{$ pshift i\} will contain all the burnups and powers of bundles that have been shifted $i$-th time.

### 7.1.3 The FUEL sub-directories

Each FUEL sub-directory contains the information corresponding to a single fuel type. Inside each sub-directory, the following records will be found:

Table 75: Records in FUEL sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| MIX பபபபபபபபப $^{\text {a }}$ | I(1) |  |  | Fuel-type mixture number. |
| TOT | I(1) |  |  | Total number of fuel bundles for this fuel type. |
| MIX-VOID | I(1) |  |  | Voided-cell mixture number for this fuel type. |
| WEIGHT $_{\text {பபபபபப }}$ | $\mathrm{R}(1)$ |  | kg | Fuel weight in a bundle for this fuel type. |
| ENRICH $ப ப ப ப ப \sqcup$ | $\mathrm{R}(1)$ |  | wt\% | Fuel enrichment for this fuel type. |
| POISON $-ப \sqcup \sqcup \sqcup \sqcup ~$ | R(1) |  |  | Poison load for this fuel type. |

### 7.1.4 The \{hcycle\} sub-directories

Each $\{$ hcycle $\}$ sub-directory contains the information corresponding to a single PWR fuel cycle. Inside each sub-directory, the following records will be found:

Table 76: Records in \{hcycle\} sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| TIME பபபபபபபப | $\mathrm{R}(1)$ |  | d | Depletion time corresponding to instantaneous burnup values. |
| BURNAVG பபபபப | R (1) |  | MW d t ${ }^{-1}$ | Average burnup of the assembly. |
| NAME | $\mathrm{C}\left(N_{\mathrm{ch}}\right) * 12$ |  |  | Names of each assembly or of each quart-of assembly during a refuelling cycle. All quart-of-assembly belonging to the same assembly have the same name. |
| FLMIX $_{\text {பபபபபபப }}$ | $\mathrm{I}\left(N_{\text {ch }}, N_{b}\right)$ |  |  | Fuel mixture indices per assembly subdivisions for each reactor channel. |
| BURN-INST bபப | $\mathrm{R}\left(N_{\mathrm{ch}}, N_{b}\right)$ |  | $\text { MW d t t }{ }^{-1}$ | Instantaneous burnups per assembly subdivisions for each channel. |
| POWER-BUND பப | $\mathrm{R}\left(N_{\mathrm{ch}}, N_{b}\right)$ |  | $\mathrm{kW}$ | Powers per assembly subdivisions for each channel. |

### 7.1.5 The PARAM sub-directories

Each PARAM sub-directory contains the information corresponding to a single local or global parameter (excluding burnups). Inside a such sub-directory, the following records will be found:

Table 77: Records in PARAM sub-directories

| Name | Type | Condition | Units | Comment |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| P-NAME | $\mathrm{C} * 12$ |  |  | Unique identification name of this parameter. This name is user-defined; however, it is recommended to use the following pre-defined values: |  |
|  |  |  |  | C-BORE <br> T-FUEL <br> T-SURF <br> T-COOL <br> D-COOL | Boron concentration <br> Averaged fuel temperature <br> Surfacic fuel temperature <br> Averaged coolant temperature <br> Averaged coolant density |
|  |  |  |  | CANDU-only parameters: |  |
|  |  |  |  | $\begin{aligned} & \text { T-MODE } \\ & \text { D-MODE } \end{aligned}$ | Averaged moderator temperature Averaged moderator density |
| PARKEY $_{\text {பபபபபப }}$ | $\mathrm{C} * 12$ |  |  | Correspon recorded i | ling name of this parameter as a multi-parameter Compo file. |

Records in PARAM sub-directories
continued from last page

| Name | Type | Condition Units | Comment |
| :--- | :--- | :--- | :--- |
| P-TYPE |  |  |  |
| P-VUபபபப | $\mathrm{I}(1)$ | Number associated to the type of recorded <br> parameter: ptype $=1$ for global parameter; <br> ptype $=2$ for local parameter. |  |
|  | $\mathrm{R}(1)$ | ptype $=1$ <br> $\mathrm{R}\left(N_{\mathrm{ch}}, N_{b}\right)$ <br> ptype $=2$ | Recorded single value for global parameter. <br> fuel bundle for every channel. |
|  |  |  |  |

### 7.2 Contents of /matex/ data structure

A /matex/ data structure is used to store several information related to the reactor extended material index and geometry. This object has a signature L_MATEX; it is created using the USPLIT: module. The information contained in this data structure can be used and updated in other DONJON modules.

### 7.2.1 The state-vector content

The dimensioning parameters $\mathcal{S}_{i}$, which are stored in the state vector for this data structure, represent:

- The number of energy groups $N_{g r}=\mathcal{S}_{1}$
- The maximum number of material mixtures $N_{m}=\mathcal{S}_{2}$ ( $N_{m}$ equals to the total number of material regions plus the number of device mixtures)
- The number of reflector types $N_{r}=\mathcal{S}_{3}$
- The number of fuel types $N_{f}=\mathcal{S}_{4}$
- The total number of mixtures indices $N_{t o t}=\mathcal{S}_{5}$ ( $N_{t o t}$ equals to the total number of mesh-splitted volumes plus the number of device mixtures)
- The type of reactor geometry $I_{g}=\mathcal{S}_{6}$ (only $I_{g}=7$ for $3 D$-Cartesian geometry or $I_{g}=9$ for 3D-Hexagonal geometry are allowed)
- The total number of mesh-splitted volumes $N_{e l}=\mathcal{S}_{7}$
- The number of mesh-splitted volumes along x-axis $L_{x}=\mathcal{S}_{8}$
- The number of mesh-splitted volumes along y-axis $L_{y}=\mathcal{S}_{9}$
- The number of mesh-splitted volumes along z-axis $L_{z}=\mathcal{S}_{10}$


### 7.2.2 The /matex/ directory

The following records will be found on the /matex/ directory:

Table 78: Records in /matex/ data structure

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| SIGNATURE | $\mathrm{C} * 12$ |  |  | Signature of the /matex/ data structure (SIGNA =L_MATEX |
| STATE-VECTOR | $\mathrm{I}(40)$ |  |  | Vector describing the various parameters associated with this data structure $\mathcal{S}_{i}$ |
| $\mathrm{RMIX}_{\text {பபபபபபபப }}$ | $\mathrm{I}\left(N_{r}\right)$ |  |  | The reflector-type mixture indices, as defined in the reactor geometry. |
| RTOT பபபபபபபப | $\mathrm{I}\left(N_{r}\right)$ |  |  | The total number of reflector regions per each reflector type. |
| $\mathrm{FMIX}_{\text {பபபபபபபப }}$ | $\mathrm{I}\left(N_{f}\right)$ |  |  | The fuel-type mixture indices, as defined in the reactor geometry. |
| $\mathrm{FTOT}_{\text {பபபபபபபப }}$ | $\mathrm{I}\left(N_{f}\right)$ |  |  | The total number of fuel regions per each fuel type. |
| MAT $\mathrm{Cuபபபபபபபப}$ | $\mathrm{I}\left(N_{t o t}\right)$ |  |  | The material mixture indices per each region and including the device mixtures. The fueltype indices are set negative; the device indices are appended at the end of vector; the virtual-region indices are set to 0 . |
| INDEX $_{\text {பபபபபபப }}$ | $\mathrm{I}\left(N_{e l}\right)$ |  |  | The renumbered mixture indices. A unique number is associated with each mesh-splitted volume. The device indices are not included; the virtual-region indices are set to 0 . |
| MESHX | $\mathrm{R}\left(L_{x}+1\right)$ |  |  | The mesh-splitted coordinates along x-axis of the reactor geometry. |
| MESHY | $\mathrm{R}\left(L_{y}+1\right)$ |  |  | The mesh-splitted coordinates along y-axis of the reactor geometry. |
| MESHZ ¢பபபபபப | $\mathrm{R}\left(L_{z}+1\right)$ |  |  | The mesh-splitted coordinates along z-axis of the reactor geometry. |
| H-FACTOR | $\mathrm{R}\left(N_{m}, N_{g r}\right)$ |  |  | The h-factors per each mixture and per each energy group, as recovered from the extended /macrolib/ data structure. |

### 7.3 Contents of /device/ data structure

A / device/ data structure is used to store several information related to the reactor devices. This object has a signature L_DEVICE; it is created using the DEVINI: module. The information contained in this data structure can be used and updated in other DONJON modules which are related to the devices, namely: LZC:, DSET: , MOVDEV: and NEWMAC: modules.

### 7.3.1 The state-vector content

The dimensioning parameters $\mathcal{S}_{i}$, which are stored in the state vector for this data structure, represent:

- The type of reactor geometry $I_{g}=\mathcal{S}_{1}$ (only $I_{g}=7$ for $3 D$-Cartesian geometry allowed)
- The total number of rod-type devices $N_{\text {rod }}=\mathcal{S}_{2}$
- The total number of the rod-type groups $N_{\text {rgrp }}=\mathcal{S}_{3}$
- The total number of lzc-type devices $N_{l z c}=\mathcal{S}_{4}$
- The total number of the lzc-type groups $N_{\text {lgrp }}=\mathcal{S}_{5}$
- Type of control rod movement $I_{\text {mov }}=\mathcal{S}_{6}$ where

$$
I_{\text {mov }}= \begin{cases}1 & \text { Fading. A fraction of the fully inserted rod vanishes } \\ 2 & \text { Moving. The complete rod is moving (DONJON3-type movement). }\end{cases}
$$

### 7.3.2 The main /device/ directory

The following records and sub-directories will be found on the first level of / device/ directory:

Table 79: Records and sub-directories in /device/ data structure

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| SIGNATURE பபப | $\mathrm{C} * 12$ |  |  | Signature of the /device/ data structure (SIGNA =L_DEVICEபபUப). |
| STATE-VECTOR | I(40) |  |  | Vector describing the various parameters associated with this data structure $\mathcal{S}_{i}$ |
| DEV_ROD பபபபப | $\operatorname{Dir}\left(N_{\text {rod }}\right)$ |  |  | Sub-directories for each controller rod. A subdirectory is created for each controller rod according to the rod identification number. |
| ROD_GROUP பபப | $\operatorname{Dir}\left(N_{\text {rgrp }}\right)$ |  |  | Sub-directories for each group of rod-type devices. A sub-directory is created for each group of rod-type devices according to the rod-group identification number. |

continued on next page

Records and sub-directories in /device/ data structure
continued from last page

| Name | Type | Condition Units | Comment |
| :--- | :--- | :--- | :--- |
| DEV_LZC |  |  |  |
|  | Dir $\left(N_{l z c}\right)$ |  | Sub-directories for each liquid zone controller. <br> A sub-directory is created for each liquid con- <br> troller according to the liquid controller iden- <br> tification number. |
| LZC_GROUP |  |  |  |
|  | $\operatorname{Dir}\left(N_{l g r p}\right)$ | Sub-directories for each group of lzc-type de- <br> vices. A sub-directory is created for each <br> group of lzc-type devices according to the lzc- <br> group identification number. |  |
|  |  |  |  |

### 7.3.3 The DEV-ROD sub-directories

Inside each DEV-ROD sub-directory, the following records will be found:

Table 80: Records in DEV-ROD sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| ROD-ID பபபபபப $^{\text {I }}$ | $\mathrm{I}(1)$ |  |  | The identification number of the rod. |
| ROD-NAME | $\mathrm{C} * 12$ |  |  | The identification name of the rod. |
| ROD-PARTS பபப | I(1) |  |  | The number of parts in the rod ( $\left.N_{\text {part }} \geq 1\right)$. |
| AXIS ¢பபபபபபப $^{\text {a }}$ | $\mathrm{I}(1)$ |  |  | The number used to identify the rod mouvement direction: $=1$ along x -axis; $=2$ along y -axis; $=3$ along z -axis. |
| FROM பபபபபபபப | $\mathrm{I}(1)$ |  |  | The number used to identify the side of geometry, from which the controller rod is inserted into the reactor core along its direction of mouvement: = 1 if a rod is inserted from the highest position (e.g. from the top); $=-1$ if a rod is inserted from the lowest position (e.g. from the bottom). |
| LENGTH | $\mathrm{R}(2)$ |  | cm | The initial and final position coordinates of the full-inserted rod along its direction of movement. The rod length is the distance between these two coordinates. |
| $\mathrm{CORE}^{\text {-LIMITS }}$ | $\mathrm{R}(6)$ |  | cm | The initial and final position coordinates of the full core along each Cartesian direction. |
| MAX-POS | $\mathrm{R}\left(6 \times N_{\text {part }}\right)$ |  | cm | The limiting 3D-Cartesian coordinates of the full-inserted rod. This data is given for each part of the rod. |

Records in DEV-ROD sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| ROD-MIX பபபபப | $\mathrm{I}\left(2 \times N_{\text {part }}\right)$ |  |  | The rod-type mixture indices. The first number corresponds to the inserted rod position and the second to the withdrawn rod position. This data is given for each part of the rod. |
| LEVEL | R(1) | * |  | The actual insertion level of the controller rod. This value must be between 0.0 for the fullwithdrawn rod and 1.0 for the full-inserted rod. |
| SPEEDபபபபபபப | $\mathrm{R}(1)$ | * | $\mathrm{cm} \mathrm{s}^{-1}$ | The speed of rod movement (insertion or extraction). |
| TIME | $\mathrm{R}(1)$ | * | S | The time for the full rod insertion or extraction. |
| ROD-POS பபபபப | $\mathrm{R}\left(6 \times N_{\text {part }}\right)$ | * | cm | The actual 3D-Cartesian coordinates of the rod. This data is given for each part of the rod. |

### 7.3.4 The ROD-GROUP sub-directories

Inside each ROD-GROUP sub-directory, the following records will be found:

Table 81: Records in ROD-GROUP sub-directories

| Name | Type | Condition Units | Comment |
| :--- | :--- | :--- | :--- |
| GROUP-ID <br> NUM-ROD <br> RUபபபப | $\mathrm{I}(1)$ | $\mathrm{I}(1)$ | The identification number of the rod-group. <br> The total number $N_{r d}$ of rod-devices in the <br> group. |
| An array of identification numbers of rods |  |  |  |
| which belong to the same group. |  |  |  |

### 7.3.5 The DEV-LZC sub-directories

Inside each DEV-LZC sub-directory, the following records will be found:

Table 82: Records in DEV-LZC sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| LZC-ID பபபபபப | I(1) |  |  | The identification number of the liquid zone controller. |
| MAX-POS பபபபப | R(6) |  | cm | The limiting 3D-Cartesian coordinates of the whole liquid controller, including its empty and full parts. |
| AXIS ¢பபபபபபப $^{\text {a }}$ | I(1) |  |  | The number used to identify the water filling direction: $=1$ along x -axis; $=2$ along y -axis; $=3$ along z -axis. |
| HEIGHT $_{\text {பபபபபப }}$ | $\mathrm{R}(1)$ |  | cm | The water height of the full-filled controller along its direction of filling. |
| LEVEL | $\mathrm{R}(1)$ |  |  | The actual water level of the liquid controller device. This value must be between 0.0 for the empty state and 1.0 for the full-filled state. |
| EMPTY-POS பபப | R (6) |  | cm | The actual 3D-Cartesian coordinates of the empty-part of liquid contoller. |
| FULL-POS பபபப | R(6) |  | cm | The actual 3D-Cartesian coordinates of the full-part of liquid contoller. |
| EMPTY-MIX பபப | $\mathrm{I}(2)$ |  |  | The empty-part mixture number and the reference mixture number. |
| FULL-MIX பபபப | $\mathrm{I}(2)$ |  |  | The full-part mixture number and the reference mixture number. |
| RATE | $\mathrm{R}(1)$ |  | $m^{3} s^{-1}$ | The water filling rate. |
| TIME | R(1) |  | S | The water filling time. |

### 7.3.6 The LZC-GROUP sub-directories

Inside each LZC-GROUP sub-directory, the following records will be found:

Table 83: Records in LZC-GROUP sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| GROUP-ID பபபப | I(1) |  |  | The identification number of the lzc-group. |
| NUM-LZCபபபபப | I(1) |  |  | The total number $N_{l d}$ of lzc-devices in the group. |
| LZC-ID பபபபபப | $\mathrm{I}\left(N_{l d}\right)$ |  |  | An array of identification numbers of liquid controllers which belong to the same group. |

### 7.4 Contents of a / detect/ data structure

The /detect/ data structure is used to store detector positions and responses. This object has a signature L_DETECT; it is created using the DETINI: module. The information contained in this data structure can be used and updated in other DONJON modules which are related to the detectors, namely: DETECT: and DETINI: modules.

### 7.4.1 The state-vector content

The dimensioning parameters $\mathcal{S}_{i}$, which are stored in the state vector for this data structure, represent:

- The number of energy groups. $N_{g}=\mathcal{S}_{1}$
- The total number of detectors $\sum \mathcal{I}_{1}=\mathcal{S}_{2}$.
- Flag for hexagonal detector definition $\mathcal{S}_{3}=1$ for hexagonal detector definition, $=0$ otherwise.

The dimensioning parameters for a specific detector type, which are stored in the vector $\mathcal{I}_{i}$, represents:

- The number of detectors of type $\{$ name_type $\} \mathcal{I}_{1}$.
- The number of delayed responses $+2, \mathcal{I}_{2}$.


### 7.4.2 The main /detect/ directory

The following records and sub-directories will be found on the first level of / detect/ directory:

Table 84: Records and sub-directories in /detect/ data structure

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| SIGNATURE பபப | $\mathrm{C} * 12$ |  |  | Signature of the /detect/ data structure (SIGNA = L_DETECT |
| STATE-VECTOR | $\mathrm{I}(40)$ |  |  | Vector describing the various parameters associated with this data structure $\mathcal{S}_{i}$ |
| \{/name_type/\} |  |  |  | Detector type sub-directory contains informations for each detector of this type. |

7.4.3 The /name_type/ sub-directories

Inside each / name_type/ sub-directory, the following records will be found:

Table 85: Records in /name_type/ sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| INFORMATIONS | $\mathrm{I}(2)$ |  | $s^{-1}$ | Record containing describing the various parameters associated with a detector type $\mathcal{I}_{i}$. The inverse time constant of the delayed detector responses. <br> The delayed and prompt fractions of the detector responses. <br> The energy spectrum of the detector. Detector information sub-directory |
| INV-CONST பபப | $\mathrm{R}\left(\mathcal{I}_{2}-2\right)$ |  |  |  |
| FRACTION $_{\text {பபப }}$ | $\mathrm{R}\left(\mathcal{I}_{2}-1\right)$ |  |  |  |
| SPECTRAL ${ }_{\text {பபபப }}$ | $\mathrm{R}\left(\mathcal{I}_{2}-1\right)$ |  |  |  |
| \{/name_detect/\} | Dir |  |  |  |

### 7.4.4 The /name_detect/ sub-directories

Inside each / name_detect/ sub-directory, the following records will be found:

Table 86: Records in /name_detect/ sub-directories

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| NHEX பபபபபபபப | $\mathrm{I}($ nhex $)$ | $h e x=1$ |  | The numbers of affected hexagons in the first X-Y plane. |
| POSITION | $\mathrm{R}(6)$ |  | cm | The coordinates of the detector. |
| RESPON | $\mathrm{R}\left(\mathcal{I}_{2}\right)$ |  |  | The responses of the detector. |

### 7.5 Contents of /power/ data structure

A / power/ data structure is used to store the information related to the powers and fluxes over the reactor core. This object has a signature L_POWER; it is created using the FLPOW: module. The reactor fluxes and powers are recorded using several data formats.

### 7.5.1 The state-vector content

The dimensioning parameters $\mathcal{S}_{i}$, which are stored in the state vector for this data structure, represent:

- The number of energy groups $N_{g r}=\mathcal{S}_{1}$
- The total number of mesh-splitted volumes $N_{e l}=\mathcal{S}_{2}$
- The number of mesh-splitted volumes along x-axis $L_{x}=\mathcal{S}_{3}$
- The number of mesh-splitted volumes along y-axis $L_{y}=\mathcal{S}_{4}$
- The number of mesh-splitted volumes along z-axis $L_{z}=\mathcal{S}_{5}$
- The number of reactor channels $N_{c h}=\mathcal{S}_{6}$
- The number of bundles per channel $N_{b}=\mathcal{S}_{7}$


### 7.5.2 The /power/ directory

The following records will be found on the /power/ directory:

Table 87: Records in /power/ data structure

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| SIGNATURE பபப $^{\text {a }}$ | $\mathrm{C} * 12$ |  |  | Signature of the /power/ data structure (SIGNA =L_POWER |
| STATE-VECTOR | $\mathrm{I}(40)$ |  |  | Vector describing the various parameters associated with this data structure $\mathcal{S}_{i}$ |
| PTOT | D (1) |  | MW | The total reactor power. |
| VTOT | D (1) |  | $\mathrm{cm}^{3}$ | The total reactor volume. |
| NORM Uபபபபபபப $^{\text {l }}$ | D (1) |  |  | The flux normalization factor. |
| FLMIX பபபபபபப | $\mathrm{I}\left(N_{c h}, N_{b}\right)$ |  |  | Fuel mixture indices per fuel bundle. |
| $\mathrm{FLUX}_{\text {பபபபபபபப }}$ | $\mathrm{R}\left(N_{e l}, N_{g r}\right)$ |  | $\mathrm{cm}^{-2}$ | ${ }^{1}$ The normalized fluxes over the whole reactor geometry, recorded per each mesh-splitted volume and per each energy group. The flux values over the virtual regions are set to 0 . |
| VOLU-BUND பபப | $\mathrm{R}\left(N_{c h}, N_{b}\right)$ |  | $\mathrm{cm}^{2}$ | The volume of each fuel bundle. |
| FLUX-BUND பபப $^{\text {b }}$ | $\mathrm{R}\left(N_{c h}, N_{b}, N_{g r}\right)$ |  | $\mathrm{cm}^{-2}$ | ${ }^{1}$ The normalized average fluxes recorded per each fuel bundle and per each energy group. |
| FLUX-DISTR bu | $\mathrm{R}\left(L_{x}, L_{y}, L_{z}, N_{g r}\right)$ |  | $\mathrm{cm}^{-2}$ | ${ }^{1}$ The normalized flux distribution over the whole reactor geometry, recorded per each X-Y-Z planes and per each energy group. |
| FLUX-RATIO ப | $\mathrm{R}\left(L_{x}, L_{y}, L_{z}, N_{g r}-1\right)$ |  |  | The fluxes ratios with respect to the thermal energy-group fluxes. |
| POWER-BUND பப | $\mathrm{R}\left(N_{c h}, N_{b}\right)$ |  | $k W$ | The bundle powers. |
| POWER-CHAN - | $\mathrm{R}\left(N_{c h}\right)$ |  | $k W$ | The channel powers. |
| POWER-DISTR ${ }_{\sqcup}$ | $\mathrm{R}\left(L_{x}, L_{y}, L_{z}\right)$ |  | W | The power distribution over the reactor core, recorded per each X-Y-Z planes. The power values over the non-fuel regions are set to 0 . |
| PMAX-CHAN ${ }_{\text {Uபப }}$ | R (1) |  | $k W$ | The maximum channel power. |
| PMAX-BUND $ப \sqcup \sqcup$ | $\mathrm{R}(1)$ |  | $k W$ | The maximum bundle power. |
| FORM-CHAN | $\mathrm{R}(1)$ |  |  | The radial power-form factor, defined as maximum-to-average channel power in core. |


| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| FORM-BUND பபப | $\mathrm{R}(1)$ |  |  | The over maximum |
| K-EFFECTIVE ${ }_{\sqcup}$ | R(1) |  |  | The effec from the |

All stored fluxes are normalized either to the given total reactor power or using the previously recorded normalization factor. The recorded values of the maximum channel and bundle powers, the channel and bundle power-form factors, and the effective multiplication factor, can be used as power and criticity constraints for the optimization and fuel management purposes.

### 7.6 Contents of /history/ data structure

This data structure contains the information required to ensure a smooth coupling of DRAGON with DONJON when a history based full reactor calculation is to be performed.

### 7.6.1 The main directory

The following records and sub-directories will be found in the first level of a /history/ directory:

Table 88: Main records and sub-directories in /history/

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| SIGNATURE | $\mathrm{C} * 12$ |  |  | parameter SIGNA containing the signature of the data structure |
| STATE-VECTOR | $\mathrm{I}(40)$ |  |  | array $\mathcal{S}_{i}^{h}$ containing various parameters that are required to describe this data structure |
| BUNDLELENGTH | $\mathrm{R}(1)$ |  | cm | parameter $L_{z}$ containing the fuel bundle length |
| NAMEGLOBAL | $\mathrm{C}\left(\mathcal{S}_{1}^{h}\right) * 12$ |  |  | array $\mathcal{G}_{j}$ containing the names of the global parameters |
| PARAMGLOBAL ${ }_{\sqcup}$ | $\mathrm{R}\left(\mathcal{S}_{1}^{h}\right)$ |  |  | array $G_{j}$ containing the value of the global parameters |
| NAMELOCAL | $\mathrm{C}\left(\mathcal{S}_{2}^{h}\right) * 12$ |  |  | array $\mathcal{L}_{j}$ containing the names of the local parameters |
| CELLID $-ப \sqcup ப \sqcup \sqcup ~$ | $\mathrm{I}\left(\mathcal{S}_{3}^{h}, \mathcal{S}_{4}^{h}\right)$ |  |  | array $C_{i, j}$ containing an identification number associated with bundle $i$ and channel $j$ |
| FUELID பபபபபப | $\mathrm{I}\left(\mathcal{S}_{3}^{h}, \mathcal{S}_{4}^{h}\right)$ |  |  | array $F_{i, j}$ containing the fuel type associated with bundle $i$ and channel $j$ |

continued on next page

Main records and sub-directories in /history/

| Name | Type | Condition | Units Comment |
| :--- | :--- | :--- | :--- |
| $\{/ F U E L D I R /\}$ | Dir | list of sub-directories $\mathrm{FUEL}_{i, j}$ that contain the prop- <br> erties associated with the fuel type $F_{i, j}$ <br> list of sub-directories $\mathrm{CELL}_{i, j}$ that contain the prop- <br> erties associated with the cell $C_{i, j}$ |  |
| $\{/ C E L L D I R /\}$ | Dir | lat |  |

The signature for this data structure is SIGNA=L_HISTORY பபப. . The array $\mathcal{S}_{i}^{h}$ contains the following information:

- $\mathcal{S}_{1}^{h}=N_{g}$ contains the number of global parameters.
- $\mathcal{S}_{2}^{h}=N_{l}$ contains the number of local parameters.
- $\mathcal{S}_{3}^{h}=N_{b}$ contains the number of bundles per channel.
- $\mathcal{S}_{4}^{h}=N_{c}$ contains the number of channels in the core.
- $\mathcal{S}_{5}^{h}=N_{s}$ contains the number of bundle shift.
- $\mathcal{S}_{6}^{h}=T_{s}$ contains the type of depletion solution used.
- $\mathcal{S}_{7}^{h}=T_{b}$ contains the type of burnup considered.
- $\mathcal{S}_{8}^{h}=N_{I}$ contains the number of isotopes.
- $\mathcal{S}_{9}^{h}=G$ contains the number of transport groups.
- $\mathcal{S}_{10}^{h}=N_{r}$ contains the number of regions.
- $\mathcal{S}_{11}^{h}=N_{F}$ contains the number of fuel types.

The fuel directory name $\mathrm{FUEL}_{i, j}$ associated with fuel type $F_{i, j}$ is composed using the following FORTRAN instruction:

```
WRITE(FUEL,'(A4,I8.8)') 'FUEL', F
```

This directory will contain the initial isotopic content of this fuel type. The cell directory name $\mathrm{CELL}_{i, j}$ associated with $C_{i, j}$ is composed using the following FORTRAN instruction:

```
WRITE(CELL,'(A4,I8.8)') 'CELL', \(C_{i, j}\)
```

This directory will contain the value of the local parameters associated with cell $C_{i, j}$ as well as the current isotopic content of this cell.

The identification number $C_{i, j}$ associated with channel $j$ and bundle $i$ can be seen as the serial number of the bundle located at a position in space identified by $(i, j)$. It is automatically managed by the HST : module. ${ }^{[?]}$ For a fresh core $C_{i, j}=n$ where $n$ represents the cell order definition in the input file. Upon refueling, some bundles in channel $k$ of the core are displaced from region $(l, k)$ to ( $m, k$ ), new bundles are introduced at location $(l, k)$ and old bundles removed from location $(m, k)$. If one assumes that $C^{\text {NEW }}$ and $C^{\text {OLD }}$ represents the value of $C$ after and before refueling then we will have:

$$
\begin{aligned}
C_{m . k}^{\mathrm{NEW}} & =C_{l, k}^{\mathrm{OLD}} \\
C_{l, k}^{\mathrm{NEW}} & =C_{m, k}^{\mathrm{FRESH}}
\end{aligned}
$$

where $C_{m, k}^{\mathrm{FRESH}}$ represent a fresh fuel cell. The local parameters and burnup power density of the fuel cell previously located at $(m, k)$ are preserved and the fresh fuel isotopic densities is that provided in $F_{m, k}$, the fuel type associated with $C_{m, k}^{\mathrm{FRESH}}$.

### 7.6.2 The fuel type sub-directory

Each fuel sub-directory $\mathrm{FUEL}_{i, j}$ contains the following information

Table 89: Fuel type sub-directory

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| FUELDEN-INIT | $\mathrm{R}(2)$ |  |  | array containing the initial density of heavy element in the fuel $\rho_{f}$ in $\mathrm{g} / \mathrm{cm}^{3}$ and the initial linear density of heavy element in the fuel $m_{f}$ in $\mathrm{g} / \mathrm{cm}$. |
| ISOTOPESUSED | $\mathrm{C}\left(N_{I}\right) * 12$ |  |  | array containing the name of isotopes used in this fuel type |
| ISOTOPESMIX $_{\sqcup}$ | $\mathrm{I}\left(N_{I}\right)$ |  |  | array containing the mixture associated with each isotopes in this fuel type |
| ISOTOPESDENS | $\mathrm{R}\left(N_{I}\right)$ |  | $(\mathrm{cm} \mathrm{b})^{-1}$ | array $\rho_{i}$ containing the density of each isotopes |

7.6.3 The cell type sub-directory

Each cell isotopic sub-directory $\mathrm{CELL}_{i, j}$ contains the following information

Table 90: Cell sub-directory

| Name | Type Condition Units | Comment |  |
| :--- | :--- | :--- | :--- |
| FUELDEN-INIT | $\mathrm{R}(2)$ | array containing the initial density of heavy <br> element in the fuel $\rho_{f}$ in $\mathrm{g} / \mathrm{cm}^{3}$ and the initial <br> linear density of heavy element in the fuel $m_{f}$ <br> in $\mathrm{g} / \mathrm{cm}$. <br> array $V_{l}^{B}$ containing the value of the local pa- <br> rameters before refueling <br> array $V_{l}^{A}$ containing the value of the local pa- <br> rameters after refueling |  |
| PARAMLOCALAR | $\mathrm{R}\left(N_{l}\right)$ | $\mathrm{R}\left(N_{l}\right)$ |  |

Cell sub-directory
continued from last page

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| PARAMBURNTBR | $\mathrm{R}(2)$ |  |  | array containing the depletion time $T^{B}$ in days and the burnup power rate $P^{B}$ in $\mathrm{kW} / \mathrm{kg}$ before refueling |
| PARAMBURNTAR | $\mathrm{R}(2)$ |  |  | array containing the depletion time $T^{A}$ in days and the burnup power rate $P^{A}$ in $\mathrm{kW} / \mathrm{kg}$ after refueling |
| DEPL-PARAM பப | R(3) |  |  | array containing the time step $T$ in days, the burnup $B$ in $\mathrm{kWd} / \mathrm{kg}$ and the irradiation $w$ in $\mathrm{n} / \mathrm{kb}$ currently reached by the fuel in this cell |
| ISOTOPESDENS | $\mathrm{R}\left(N_{I}\right)$ |  | $(\mathrm{cm} \mathrm{b})^{-1}$ | array $\rho_{i}$ containing the density of each isotopes |

### 7.7 Contents of /thm/ data structure

This data structure contains the thermal-hydraulics information required in a multi-physics calculation

### 7.7.1 The main /thm/ directory

The following records and sub-directories will be found in the first level of a / thm/ directory:

Table 91: Main records and sub-directories in /thm/

| Name | Type | Condition | Units Comment |
| :---: | :---: | :---: | :---: |
| SIGNATURE | $\mathrm{C} * 12$ |  | parameter SIGNA containing the signature of the data structure |
| STATE-VECTOR | $\mathrm{I}(40)$ |  | array $\mathcal{S}_{i}^{\text {th }}$ containing various integer parameters that are required to describe this data structure |
| REAL-PARAM $_{\text {பப }}$ | R (40) |  | array $\mathcal{R}_{i}^{t h}$ containing various floating-point parameters that are required to describe this data structure |
| KCONDF | $\mathrm{R}\left(\mathcal{S}_{16}^{\text {th }}+3\right)$ | $\mathcal{S}_{12}^{\text {th }} \neq 0$ | coefficients of the user-defined correlation for the fuel thermal conductivity |
| UCONDF ${ }_{\text {பபபபபப }}$ | C12 | $\mathcal{S}_{12}^{\text {th }} \neq 0$ | string variable set to KELVIN or to CELSIUS |
| KCONDC | $\mathrm{R}\left(\mathcal{S}_{17}^{\text {th }}+3\right)$ | $\mathcal{S}_{13}^{\text {th }} \neq 0$ | coefficients of the user-defined correlation for the clad thermal conductivity |
| UCONDC பபபபபப | C12 | $\mathcal{S}_{13}^{\text {th }} \neq 0$ | string variable set to KELVIN or to CELSIUS |
| ERROR-T-FUEL | $\mathrm{R}(1)$ |  | K absolute error in fuel temperature |
| ERROR-D-COOL | R (1) |  | $\mathrm{g} / \mathrm{cc}$ absolute error in coolant density |

continued on next page

Main records and sub-directories in /thm/

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| ERROR-T-COOL | $\mathrm{R}(1)$ |  | K | absolute error in coolant temperature |
| MIN-T-FUEL பப $^{\text {L }}$ | $\mathrm{R}(1)$ |  | K | minimum fuel temperature |
| MIN-D-COOL | R(1) |  | $\mathrm{g} / \mathrm{cc}$ | minimum coolant density |
| MIN-T-COOL | R(1) |  | K | minimum coolant temperature |
| MAX-T-FUEL பப $^{\text {L }}$ | R(1) |  | K | maximum fuel temperature |
| MAX-D-COOL | R(1) |  | g/cc | maximum coolant density |
| MAX-T-COOL $-{ }_{\text {- }}$ | R(1) |  | K | maximum coolant temperature |
| HISTORY-DATA | Dir |  |  | sub-directory containing the historical values taken by the thermal-hydraulics parameters (mass flux, density, pressure, enthalpy, temperature) in the coolant and in the fuel rod for the whole geometry |

The signature for this data structure is SIGNA=L_THM. The array $\mathcal{S}_{i}^{h}$ contains the following information:

- $\mathcal{S}_{1}^{t h}$ contains the number of active fuel rods.
- $\mathcal{S}_{2}^{t h}$ contains the number of guide tubes.
- $\mathcal{S}_{3}^{t h}$ contains the maximum number of iterations for computing the conduction integral.
- $\mathcal{S}_{4}^{t h}$ contains the maximum number of iterations for computing the center pellet temperature.
- $\mathcal{S}_{5}^{t h}$ contains the maximum number of iterations for computing the coolant parameters (velocity, pressure, enthapy, density) in case of a transient calculation.
- $\mathcal{S}_{6}^{t h}$ contains the number of discretisation points in fuel.
- $\mathcal{S}_{7}^{\text {th }}$ contains the number of total discretisation points in the whole fuel rod (fuel+cladding).
- $\mathcal{S}_{8}^{t h}$ contains the integer setting the type of calculation (steady-state or transient) performed by the THM: module.
- $\mathcal{S}_{9}^{t h}$ contains the current time index.
- $\mathcal{S}_{10}^{t h}$ flag to set the gap correlation:

$$
\mathcal{S}_{10}^{t h}= \begin{cases}0 & \text { built-in correlation is used } \\ 1 & \text { set the heat exchange coefficient of the gap as a user-defined constant. }\end{cases}
$$

- $\mathcal{S}_{11}^{t h}$ flag to set the heat transfer coefficient between the clad and fluid:

$$
\mathcal{S}_{11}^{t h}= \begin{cases}0 & \text { built-in correlation is used } \\ 1 & \text { set the heat exchange coefficient between the clad and fluid as a user-defined constant. }\end{cases}
$$

- $\mathcal{S}_{12}^{\text {th }}$ flag to set the fuel thermal conductivity:

$$
\mathcal{S}_{12}^{t h}= \begin{cases}0 & \text { built-in correlation is used } \\ 1 & \text { set the fuel thermal conductivity as a function of a simple user-defined correlation. }\end{cases}
$$

- $\mathcal{S}_{13}^{\text {th }}$ flag to set the clad thermal conductivity:

$$
\mathcal{S}_{13}^{t h}= \begin{cases}0 & \text { built-in correlation is used } \\ 1 & \text { set the clad thermal conductivity as a function of a simple user-defined correlation. }\end{cases}
$$

- $\mathcal{S}_{14}^{t h}$ type of approximation used during the fuel conductivity evaluation:

$$
\mathcal{S}_{14}^{t h}= \begin{cases}0 & \text { use a rectangle quadrature approximation } \\ 1 & \text { use an average approximation }\end{cases}
$$

- $\mathcal{S}_{15}^{t h}$ type of subcooling model:

$$
\mathcal{S}_{15}^{t h}= \begin{cases}0 & \text { use the Jens-Lottes correlation and Bowring's model } \\ 1 & \text { use the Saha-Zuber subcooling model. }\end{cases}
$$

- $\mathcal{S}_{16}^{t h}$ contains the number of terms in the user-defined correlation for the fuel thermal confuctivity (if $\mathcal{S}_{12}^{\text {th }}=1$ ).
- $\mathcal{S}_{17}^{t h}$ contains the number of terms in the user-defined correlation for the clad thermal confuctivity (if $\mathcal{S}_{13}^{\text {th }}=1$ ).

The array $\mathcal{R}_{i}^{t h}$ contains the following information:

- $\mathcal{R}_{1}^{\text {th }}$ contains the current time step in s .
- $\mathcal{R}_{2}^{t h}$ contains the fraction of reactor power released in fuel.
- $\mathcal{R}_{3}^{t h}$ contains the critical heat flux in $\mathrm{W} / \mathrm{m}^{2}$.
- $\mathcal{R}_{4}^{\text {th }}$ contains the inlet coolant velocity in $\mathrm{m} / \mathrm{s}$.
- $\mathcal{R}_{5}^{t h}$ contains the outlet coolant pressure in Pa .
- $\mathcal{R}_{6}^{\text {th }}$ contains the inlet coolant temperature in K .
- $\mathcal{R}_{7}^{t h}$ contains the Plutonium mass fraction in fuel.
- $\mathcal{R}_{8}^{t h}$ contains the fuel porosity.
- $\mathcal{R}_{9}^{\text {th }}$ contains the fuel pellet radius
- $\mathcal{R}_{10}^{t h}$ contains the internal clad rod radius in m .
- $\mathcal{R}_{11}^{t h}$ contains the external clad rod radius in $m$.
- $\mathcal{R}_{12}^{t h}$ contains the guide tube radius in m .
- $\mathcal{R}_{13}^{t h}$ contains the assembly surface in $\mathrm{m}^{2}$.
- $\mathcal{R}_{14}^{t h}$ contains the temperature maximum absolute error (in K ) allowed in the solution of the conduction equations.
- $\mathcal{R}_{15}^{t h}$ contains the maximum relative error allowed in the matrix resolution of the conservation equations of the coolant.
- $\mathcal{R}_{16}^{t h}$ contains the relaxation parameter for the multiphysics parameters (temperature of fuel and coolant and density of coolant).
- $\mathcal{R}_{17}^{t h}$ contains the time in s.
- $\mathcal{R}_{18}^{t h}$ contains the heat transfer coefficient of the gap (if $\mathcal{S}_{10}^{t h}=1$ ).
- $\mathcal{R}_{19}^{\text {th }}$ contains the heat transfer coefficient between the clad and fluid (if $\mathcal{S}_{11}^{\text {th }}=1$ ).
- $\mathcal{R}_{20}^{t h}$ contains the surface temperature weighting factor of effective fuel temperature for the Rowlands approximation.


### 7.7.2 The HISTORY-DATA sub-directory

In the HISTORY-DATA directory, the following sub-directories will be found:
Table 92: Sub-directories in HISTORY-DATA directory

| Name | Type Condition Units | Comment |
| :--- | :--- | :--- | :--- |
| STATIC-PARAM | $\operatorname{Dir}\left(N_{\text {ch }}\right)$ | sub-directory containing all the values of the <br> thermal-hydraulics parameters computed by <br> the THM: module in steady-state conditions <br> and sorted channel by channel. Each chan- <br> nel is identified by an integer numc that can <br> take values between 1 and 9999. For exam- <br> ple, the first channel is identified by the string <br> character "CHANNEL 0001". |
|  |  | sub-directories containing all the values of the <br> thermal-hydraulics parameters computed by <br> the THM: module in transient conditions at a |
|  | $\operatorname{Dir}\left(N_{\text {ch }}\right)$ | given time index numt and sorted channel by <br> channel. numt can take values between 1 and <br> 9999. |
|  |  |  |

In each of the $N_{\mathrm{ch}}$ CHANNEL numc sub-directories, the following records will be found:
Table 93: Records in each CHANNEL directory

| Name | Type | Condition | Units | Comment |
| :---: | :---: | :---: | :---: | :---: |
| VINLET பபபபபப $^{\text {a }}$ | $\mathrm{R}(1)$ |  | $m . s^{-1}$ | inlet velocity |
| TINLET | $\mathrm{R}(1)$ |  | K | inlet temperature |
| PINLET ¢பபபபப | $\mathrm{R}(1)$ |  | $P a$ | inlet pressure |
| VELOCITIESபப | $\mathrm{R}\left(N_{b}\right)$ |  | $m . s^{-1}$ | velocity in each of the $N_{b}$ bundles of the channel numbered numc |
| PRESSURE பபபப | $\mathrm{R}\left(N_{b}\right)$ |  | $P a$ | pressure in each bundle of the channel |
| ENTHALPY | $\mathrm{R}\left(N_{b}\right)$ |  | J. $\mathrm{kg}^{-1}$ | enthalpy in each bundle of the channel |
| DENSITY | $\mathrm{R}\left(N_{b}\right)$ |  | kg.m ${ }^{-3}$ | density in each bundle of the channel |
| LIQUID-DENS ${ }_{\sqcup}$ | $\mathrm{R}\left(N_{b}\right)$ |  | $\mathrm{kg} \cdot \mathrm{m}^{-3}$ | density of liquid phase in each bundle of the channel |
| TEMPERATURES | $\mathrm{R}\left(N_{b}, N_{\text {dtot }}\right)$ |  | K | distribution of the temperature in the fuel-pin for each bundle of the channel |
| CENTER-TEMPS | $\mathrm{R}\left(N_{b}\right)$ |  | K | center fuel pellet temperature in each bundle of the channel |

### 7.8 Contents of a /optimize/ data structure

The /optimize/ specification is used to store the optimization variables and functions values and definitions, limits and options.

In any case, the signature variable for this data structure must be SIGNA= L_OPTIMIZE $\quad$. The dimensioning parameters for this data structure, which are stored in the state vector $\mathcal{S}_{i}^{o}$, represents:

- The number of decision variables $N_{v a r}=\mathcal{S}_{1}^{o}$.
- The number of constraints $N_{c s t}=\mathcal{S}_{2}^{o}$.
- The type of optimization $\mathcal{S}_{3}^{o}$, where

$$
\mathcal{S}_{3}^{o}=\left\{\begin{aligned}
1 & \text { minimization } \\
-1 & \text { maximization }
\end{aligned}\right.
$$

- The result of a test for external convergence of the quadratic constraint $\mathcal{S}_{4}^{o}$, where

$$
\mathcal{S}_{4}^{o}= \begin{cases}0 & \text { not converged } \\ 1 & \text { converged }\end{cases}
$$

- The number of iterations relative to the quadratic constraint $\left(S_{5}^{o}\right)$.
- The type of reduction for the radius if the quadratic constraint $\left(\mathcal{S}_{6}^{o}\right)$, where

$$
\mathcal{S}_{6}^{o}= \begin{cases}1 & \text { half } \\ 2 & \text { parabolic }\end{cases}
$$

- The number of inner iterations $S_{7}^{o}$.
- The number of outer iterations $S_{8}^{o}$.
- The resolution's method for the linear problem with quadratic constraint $\left(\mathcal{S}_{9}^{o}\right)$, where

$$
\mathcal{S}_{9}^{o}= \begin{cases}1 & \text { SIMPLEX/LEMKE } \\ 2 & \text { LEMKE/LEMKE } \\ 3 & \text { MAP } \\ 4 & \text { Augmented Lagragian } \\ 5 & \text { Penalty Method }\end{cases}
$$

- The number of outer iterations without step-back $S_{10}^{o}$.
- $S_{11}^{o}$ (not used).
- $S_{12}^{o}$ (not used).
- A flag for unsuccessful resolution in module PLQ: $S_{13}^{o}$, where

$$
\mathcal{S}_{13}^{o}=\left\{\begin{aligned}
0 & \text { successful at last iteration } \\
\geq 1 & \text { number of iteration with unsuccessful resolution. }
\end{aligned}\right.
$$

Table 94: Main records and sub-directories in /optimize/

| Name | Type | Condition | UnitsComment |
| :---: | :---: | :---: | :---: |
| SIGNATURE | $\mathrm{C} * 12$ |  | Signature of the data structure (SIGNA) |
| STATE-VECTOR | $\mathrm{I}(40)$ |  | Vector describing the various parameters associated with data structure $\mathcal{S}_{i}^{o}$. |
| DLEAK-STATE ${ }_{\cup}$ | $\mathrm{I}(40)$ | * | Vector describing the various parameters associated with data structure $\mathcal{S}_{i}^{g}$. This array is available if the optimize object has been created using module DLEAK: . |
| VAR-VALUE பபப | $\mathrm{R}\left(N_{v a r}\right)$ |  | The values of the decision variables |
| VAR-MAX-VAL ${ }_{\sqcup}$ | $\mathrm{R}\left(N_{v a r}\right)$ |  | The maximum values of the decision variables can be. |
| VAR-MIN-VAL ${ }_{\sqcup}$ | $\mathrm{R}\left(N_{v a r}\right)$ |  | The minimum values of the decision variables can be. |
| VAR-WEIGHT ${ }_{\text {ப }}$ | $\mathrm{R}\left(N_{\text {var }}\right)$ |  | The weight of the decision variables $w_{i}$ in the quadratic constraint. |
| CST-OBJ பபபபப | $\mathrm{R}\left(N_{c s t}\right)$ |  | The limit value of the contraints. The units depends with the type of the constraint type. |
| CST-TYPE | $\mathrm{I}\left(N_{c s t}\right)$ |  | The type of the contraints: $=-1$ for $\geq ;=0$ for $=;=1$ for $\leq$. |
| CST-WEIGHT ${ }_{\text {ப }}$ | $\mathrm{R}\left(N_{c s t}\right)$ |  | The weight of the constraint $\eta_{j}$ and $\gamma_{j}$ for the duals and meta-heuristic methods. |
| FOBJ-CST-VAL | $\mathrm{R}\left(N_{c s t}+1\right)$ |  | The actual values of the objective function (first value) and the contraints (the following values). The number of the constraints are assigned in the order they have been defined. |
| OPT-PARAM- $\mathrm{R}_{\sqcup}$ | $\mathrm{R}(40)$ |  | The different limits and values for the iterative calculations of the optimization problem. |
| GRADIENT பபபப | $\mathrm{R}\left(N_{v a r}, N_{c s t}+1\right)$ |  | The gradients of the objective function and the constraints. The gradients of the objective for all the decision variables are in first position, then follow the gradients of the constraints. |
| OLD-VALUE $\sqcup \sqcup \sqcup$ | Dir |  | Directory containing differents informations of the previous iterations. the values of the decision variables, the objective function, the constraints and the gradients of these functions for the previous external iteration. This repertory will be created by the module QLP : unless it is specified to not do. |

The array OPT-PARAM-R contains real values related with the different limits and values for the iterative calculations of the optimization problem:

| 1st | $S$ | initial radius of the quadratic constraint (default: 1.0). |
| :--- | :--- | :--- |
| 2nd | $\delta$ | initial size of the hypercube for MAP method. (default: 0.1 ). |
| 3 rd | $\varepsilon_{\text {ext }}$ | limit for external convergence (default: $10^{-4}$ ). |
| 4 th | $\varepsilon_{\text {int }}$ | limit for internal convergence (default: $10^{-4}$ ). |
| 5 th | $\varepsilon_{\text {quad }}$ | limit for convergence of the quadratic constraint (default: $10^{-4}$ ). |
| The other value of the record are not used and set to 0.0. |  |  |

The optional array DLEAK-STATE contains integer values related to the definition of mixture and group indices in module DLEAK: .

- The number of energy groups in macrolib $\mathcal{S}_{1}^{g}$.
- The number of mixtures in macrolib $\mathcal{S}_{2}^{g}$.
- The type of leakage parameters $\mathcal{S}_{3}^{g}$, where

$$
\mathcal{S}_{3}^{g}= \begin{cases}1 & \text { use diffusion coefficients } \\ 2 & \text { use } P_{1} \text {-weighted macroscopic total cross sections. }\end{cases}
$$

- The type of control variables $\mathcal{S}_{4}^{g}$, where

$$
\mathcal{S}_{4}^{g}= \begin{cases}1 & \text { use leakage parameter itself } \\ 2 & \text { use a correction factor. }\end{cases}
$$

- The minimum group index $\mathcal{S}_{5}^{g}$, with $1 \leq \mathcal{S}_{5}^{g} \leq \mathcal{S}_{1}^{g}$.
- The maximum group index $\mathcal{S}_{6}^{g}$, with $\mathcal{S}_{5}^{g} \leq \mathcal{S}_{6}^{g} \leq \mathcal{S}_{2}^{g}$.
- The minimum mixture index $\mathcal{S}_{7}^{g}$, with $1 \leq \mathcal{S}_{7}^{g} \leq \mathcal{S}_{2}^{g}$.
- The maximum mixture index $\mathcal{S}_{8}^{g}$, with $\mathcal{S}_{7}^{g} \leq \mathcal{S}_{8}^{g} \leq \mathcal{S}_{2}^{g}$.
7.8.1 The sub-directory /OLD-VALUE/ in /optimize/

Table 95: Main records and sub-directories in //OLD-VALUE//

| Name | Type | Condition | UnitsComment |
| :---: | :---: | :---: | :---: |
| VAR-VALUE பபப | $\mathrm{R}\left(N_{v a r}\right)$ |  | The values of the decision variables of the last valid iteration. |
| FOBJ-CST-VAL | $\mathrm{R}\left(N_{c s t}+1\right)$ |  | The values of the objective function and the contraints of the last valid iteration. |
| GRADIENT பபபப | $\mathrm{R}\left(N_{v a r}, N_{c s t}+1\right)$ |  | The gradients of the objective function and the constraints of the last valid iteration. |
| VAR-VALUE2பப | $\mathrm{R}\left(N_{v a r}\right)$ |  | The values of the decision variables of the second-last valid iteration. |
| BEST-VAR | $\mathrm{R}\left(N_{v a r}\right)$ |  | The values of the decision variables corresponding to the best valid solution ever found. |
| BEST-FCT பபபப | R(1) |  | The value of the objective function corresponding to the best valid solution ever found. |

## 8 EXAMPLES

The following examples of input files represent a typical core modeling using DONJON. The main characteristics of a simplified design for the ACR-700 benchmark core model are given below.


Figure 12: Face View of ACR Benchmark Core Model (292 Channels)

- Number of reactor channels 292
- Number of fuel bundles per channel 12
- Core radius 260 cm
- Core length 594.36 cm
- Lattice pitch 22 cm
- Reactor thermal power 1800 MW(th)


## 8.1 (Example1) - Compo related example

Input data for test case: Example1.x2m

```
**************************************************************
*
* Input file : Example1.x2m *
* Purpose : Test for non-regression using DONJON-4 *
* Author(s) : D. Sekki (2007/11) *
*
***************************************************************
PROCEDURE assertS Pgeom Pfmap Pburn Pdevc ;
MODULE DELETE: GREP: END: CRE: MACINI: FLUD: USPLIT:
    DSET: TAVG: FLPOW: TRIVAT: TRIVAA: NEWMAC: ;
LINKED_LIST GEOM TRACK MATEX FMAP FLUX POWER MACFL
    DEVICE MACRO1 MACRO2 MACRO SYSTEM ;
LINKED_LIST LREFL1 LREFL2 LFUEL1 LFUEL2
    LZCRin LZCRot LSORin LSORot ;
*--
* variables:
*--
INTEGER nbMix := 8 ;
INTEGER nbRefl nbFuel := 2 2 ;
INTEGER mFuel1 mFuel2 := 1 2 ;
INTEGER mRefl1 mRefl2 := 3 4 ;
INTEGER mZCRin mZCRot := 5 6 ;
INTEGER mSORin mSORot := 7 8 ;
INTEGER MaxReg := 100000 ;
STRING Method := "MCFD" ;
INTEGER degree quadr := 1 1 ;
INTEGER iter iEdit := 0 5 ;
REAL Power := 1800. ;
REAL epsil := 1.E-5 ;
REAL Precf := 1.E-5 ;
REAL Eps Keff Bexit ;
*--
* compo files:
*--
SEQ_ASCII SFUEL1 :: FILE 'CpoFuel1' ;
SEQ_ASCII SFUEL2 :: FILE 'CpoFuel2' ;
SEQ_ASCII SREFL1 :: FILE 'CpoMode1' ;
SEQ_ASCII SREFL2 :: FILE 'CpoMode2' ;
SEQ_ASCII SZCRin :: FILE 'CpoZCRin' ;
SEQ_ASCII SZCRot :: FILE 'CpoZCRot' ;
SEQ_ASCII SSORin :: FILE 'CpoSORin' ;
SEQ_ASCII SSORot :: FILE 'CpoSORot' ;
*--
* compo directories:
*--
STRING NamFuel1 := "FUEL1 1" ;
STRING NamFuel2 := "FUEL2 1" ;
STRING NamRefl1 := "MODE1 1" ;
STRING NamRefl2 := "MODE2 1" ;
```

```
STRING 
*-------------------------------------------------------------
*
* FULL-CORE CALCULATION
* ========================
*--
* geometry construction:
*--
GEOM := Pgeom ;
*--
* reactor material index:
*--
GEOM MATEX := USPLIT: GEOM :: EDIT O NGRP 2 MAXR <<MaxReg>>
    NREFL <<nbRefl>> RMIX <<mRefl1>> <<mRefl2>>
    NFUEL <<nbFuel>> FMIX <<mFuel1>> <<mFuel2>> ;
*--
* numerical discretization:
*--
IF Method "MCFD" = THEN
    TRACK := TRIVAT: GEOM :: EDIT 1
                MAXR <<MaxReg>> MCFD <<degree>> ;
ELSEIF Method "PRIM" = THEN
    TRACK := TRIVAT: GEOM :: EDIT 1
        MAXR <<MaxReg>> PRIM <<degree>> ;
ELSEIF Method "DUAL" = THEN
    TRACK := TRIVAT: GEOM :: EDIT 1
                MAXR <<MaxReg>> DUAL <<degree>> <<quadr>> ;
ENDIF ;
*--
* macrolib for reflector:
*--
LREFL1 := SREFL1 ;
LREFL2 := SREFL2 ;
MACRO1 := CRE: LREFL1 LREFL2 :: EDIT 1 NMIX <<nbMix>> READ
                        COMPO LREFL1 MIX <<mRefl1>> <<NamRefl1>> ENDMIX
                        COMPO LREFL2 MIX <<mRefl2>> <<NamRefl2>> ENDMIX ;
*--
* device specification:
*--
DEVICE MATEX := Pdevc MATEX ::
    <<mZCRin>> <<mZCRot>> <<mSORin>> <<mSORot>> ;
*--
* full insertion of ZCR-devices:
*--
DEVICE := DSET: DEVICE :: EDIT 1
                        ROD-GROUP 1 LEVEL 1.0 END
                        ROD-GROUP 2 LEVEL 1.0 END
                        ROD-GROUP 3 LEVEL 1.0 END ;
*--
* update macrolib for devices:
```

```
*--
LZCRin := SZCRin ;
LZCRot := SZCRot ;
LSORin := SSORin ;
LSORot := SSORot ;
MACRO1 := CRE: MACRO1 LZCRin LZCRot LSORin LSORot :: EDIT 1
    READ
    COMPO LZCRin MIX <<mZCRin>> <<NamZCRin>> ENDMIX
    COMPO LZCRot MIX <<mZCRot>> <<NamZCRot>> ENDMIX
    COMPO LSORin MIX <<mSORin>> <<NamSORin>> ENDMIX
    COMPO LSORot MIX <<mSORot>> <<NamSORot>> ENDMIX ;
*--
* fuel-map specification:
*--
FMAP MATEX := Pfmap MATEX ;
*--
* average exit burnups:
*--
FMAP := Pburn FMAP ;
*--
* initialization:
*--
LFUEL1 := SFUEL1 ;
LFUEL2 := SFUEL2 ;
EVALUATE Eps := epsil 1. + ;
*----------------------------------------------------------------
* TIME-AVERAGE CALCULATION
WHILE Eps epsil > iter 20< * DO
    EVALUATE iter := iter 1 + ;
*--
* fuel-map macrolib:
*--
    MACFL := CRE: LFUEL1 LFUEL2 FMAP :: EDIT O READ
                        TABLE LFUEL1
                        MIX <<mFuel1>> <<NamFuel1>> ENDMIX
            TABLE LFUEL2
                MIX <<mFuel2>> <<NamFuel2>> ENDMIX ;
*--
* extended macrolib:
*--
    MACRO2 MATEX := MACINI: MATEX MACRO1 MACFL :: EDIT O ;
    MACFL := DELETE: MACFL ;
*--
* complete macrolib:
*--
    MACRO MATEX := NEWMAC: MATEX MACRO2 DEVICE :: EDIT O ;
    MACRO2 := DELETE: MACRO2 ;
*--
* numerical solution:
*--
    SYSTEM := TRIVAA: MACRO TRACK :: EDIT 0 ;
```

```
    MACRO := DELETE: MACRO ;
    IF iter 1 = THEN
        FLUX := FLUD: SYSTEM TRACK :: EDIT 0
                ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
                THER 1000 ;
    ELSE
        FLUX := FLUD: FLUX SYSTEM TRACK :: EDIT 0
                        ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
                THER 1000 ;
    ENDIF ;
    SYSTEM := DELETE: SYSTEM ;
*--
* flux and power:
*--
    POWER := FLPOW: FMAP FLUX TRACK MATEX ::
        EDIT 0 PTOT <<Power>> ;
* burnups integration limits:
*--
    FMAP := TAVG: FMAP POWER :: EDIT 0
            AX-SHAPE RELAX 0.5 B-EXIT ;
    POWER := DELETE: POWER ;
*--
* current parameters:
*--
    GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;
    GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
    ECHO "Iteration No. " iter ;
    ECHO "AXIAL-SHAPE ERROR : " Eps ;
    ECHO "RESULTING K-EFF : " Keff ;
ENDWHILE ;
*---------------------------------------------------------------------
*--
* edit resulting fluxes and powers:
*--
POWER := FLPOW: FMAP FLUX TRACK MATEX ::
        EDIT <<iEdit>> PTOT <<Power>> ;
*--
* last parameters:
*--
GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;
GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
GREP: FMAP :: GETVAL B-EXIT 1 >>Bexit<< ;
ECHO "Number of Iterations " iter ;
ECHO "AXIAL-SHAPE ERROR : " Eps ;
ECHO "CORE-AVERAGE EXIT BURNUP : " Bexit ;
ECHO "RESULTING K-EFFECTIVE : " Keff ;
assertS FLUX :: 'K-EFFECTIVE' 1 1.050128 ;
END: ;
QUIT .
```


## 8.2 (Example2) - Multicompo related example

Input data for test case: Example2.x2m

```
***************************************************************
* *
* Input file : Example2.x2m *
* Purpose : Test for non-regression using DONJON-4 *
* Author(s) : D. Sekki (2007/11) *
*
**************************************************************
PROCEDURE assertS Pgeom Pfmap Pburn Pdevc ;
MODULE DELETE: GREP: END: NCR: MACINI: FLUD: USPLIT:
    DSET: TAVG: FLPOW: TRIVAT: TRIVAA: NEWMAC: ;
LINKED_LIST GEOM TRACK MATEX FMAP FLUX POWER MACFL
    DEVICE MACRO1 MACRO2 MACRO SYSTEM LCPO ;
*--
* variables:
*--
INTEGER nbMix := 8 ;
INTEGER nbRefl nbFuel := 2 2 ;
INTEGER mFuel1 mFuel2 := 1 2 ;
INTEGER mRefl1 mRefl2 := 3 4 ;
INTEGER mZCRin mZCRot := 5 6 ;
INTEGER mSORin mSORot := 7 8 ;
INTEGER MaxReg := 100000 ;
STRING Method := "MCFD" ;
INTEGER degree quadr := 1 1 ;
INTEGER iter iEdit := 0 5 ;
REAL Power := 1800. ;
REAL epsil := 1.E-5 ;
REAL Precf := 1.E-5 ;
REAL Eps Keff Bexit ;
*--
* multi-compo file:
*--
SEQ_ASCII SCPO :: FILE 'MultiCompo' ;
*---------------------------------------------------------------
*
* FULL-CORE CALCULATION
* =======================
*--
* geometry construction:
*--
GEOM := Pgeom ;
*--
* reactor material index:
*--
GEOM MATEX := USPLIT: GEOM :: EDIT 1 NGRP 2 MAXR <<MaxReg>>
                        NREFL <<nbRefl>> RMIX <<mRefl1>> <<mRefl2>>
    NFUEL <<nbFuel>> FMIX <<mFuel1>> <<mFuel2>> ;
*--
* numerical discretization:
```

```
*--
IF Method "MCFD" = THEN
    TRACK := TRIVAT: GEOM :: EDIT 1
                MAXR <<MaxReg>> MCFD <<degree>> ;
ELSEIF Method "PRIM" = THEN
    TRACK := TRIVAT: GEOM :: EDIT 1
                MAXR <<MaxReg>> PRIM <<degree>> ;
ELSEIF Method "DUAL" = THEN
    TRACK := TRIVAT: GEOM :: EDIT 1
        MAXR <<MaxReg>> DUAL <<degree>> <<quadr>> ;
ENDIF ;
*--
* macrolib for reflector and devices:
*--
LCPO := SCPO ;
*
MACRO1 := NCR: LCPO :: EDIT 1 MACRO NMIX <<nbMix>>
    COMPO LCPO MODE
    MIX <<mRefl1>> SET MTYPE CELL20 ENDMIX
    MIX <<mRefl2>> SET MTYPE CELL18 ENDMIX
    COMPO LCPO FUEL
    MIX <<mZCRin>>
            SET FTYPE ZCU SET RDTPOS 1. SET RDDPOS 1.
        ENDMIX
        MIX <<mZCRot>>
            SET FTYPE ZCU SET RDTPOS 1. SET RDDPOS 0.
            ENDMIX
            MIX <<mSORin>>
                SET FTYPE SOR SET RDTPOS 1. SET RDDPOS 1.
            ENDMIX
            MIX <<mSORot>>
                SET FTYPE SOR SET RDTPOS 1. SET RDDPOS 0.
            ENDMIX ;
*--
* device specification:
*--
DEVICE MATEX := Pdevc MATEX ::
    <<mZCRin>> <<mZCRot>> <<mSORin>> <<mSORot>> ;
*--
* full insertion of ZCR-devices:
*--
DEVICE := DSET: DEVICE :: EDIT 1
    ROD-GROUP 1 LEVEL 1.0 END
    ROD-GROUP 2 LEVEL 1.0 END
    ROD-GROUP 3 LEVEL 1.0 END ;
*--
* fuel-map specification:
*--
FMAP MATEX := Pfmap MATEX ;
*--
* average exit burnups:
*--
FMAP := Pburn FMAP ;
```

```
EVALUATE Eps := epsil 1. + ;
```



```
* TIME-AVERAGE CALCULATION
*-------------------------------------------------------------
WHILE Eps epsil > iter 10 < * DO
    EVALUATE iter := iter 1 + ;
*--
* fuel-map macrolib:
*--
    MACFL := NCR: LCPO FMAP :: EDIT O MACRO
                        TABLE LCPO FUEL BURN
                        MIX <<mFuel1>> SET FTYPE CELL20 ENDMIX
                        TABLE LCPO FUEL BURN
                        MIX <<mFuel2>> SET FTYPE CELL18 ENDMIX ;
*--
* extended macrolib:
*--
    MACRO2 MATEX := MACINI: MATEX MACRO1 MACFL :: EDIT O ;
    MACFL := DELETE: MACFL ;
*--
* complete macrolib:
*--
    MACRO MATEX := NEWMAC: MATEX MACRO2 DEVICE :: EDIT O ;
    MACRO2 := DELETE: MACRO2 ;
*--
* numerical solution:
*--
    SYSTEM := TRIVAA: MACRO TRACK :: EDIT 0 ;
    MACRO := DELETE: MACRO ;
    IF iter 1 = THEN
        FLUX := FLUD: SYSTEM TRACK :: EDIT 0
                        ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
                        THER 1000;
    ELSE
        FLUX := FLUD: FLUX SYSTEM TRACK :: EDIT 0
                        ACCE 3 3 ADI 4 EXTE 1000 <<Precf>>
                        THER 1000;
    ENDIF ;
    SYSTEM := DELETE: SYSTEM ;
* flux and power:
*--
    POWER := FLPOW: FMAP FLUX TRACK MATEX ::
                        EDIT O PTOT <<Power>> ;
*--
* burnups integration limits:
*--
    FMAP := TAVG: FMAP POWER :: EDIT 0
        AX-SHAPE RELAX 0.5 B-EXIT ;
    POWER := DELETE: POWER ;
*--
* current parameters:
```

```
*--
    GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;
    GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
    ECHO "Iteration No. " iter ;
    ECHO "AXIAL-SHAPE ERROR : " Eps ;
    ECHO "RESULTING K-EFF : " Keff ;
ENDWHILE ;
*------------------------------------------------------------------------
*--
* edit resulting fluxes and powers:
*--
POWER := FLPOW: FMAP FLUX TRACK MATEX ::
    EDIT <<iEdit>> PTOT <<Power>> ;
*--
* last parameters:
*--
GREP: FLUX :: GETVAL 'K-EFFECTIVE' 1 >>Keff<< ;
GREP: FMAP :: GETVAL EPS-AX 1 >>Eps<< ;
GREP: FMAP :: GETVAL B-EXIT 1 >>Bexit<< ;
ECHO "Number of Iterations " iter ;
ECHO "AXIAL-SHAPE ERROR : " Eps ;
ECHO "CORE-AVERAGE EXIT BURNUP : " Bexit ;
ECHO "RESULTING K-EFFECTIVE : " Keff ;
assertS FLUX :: 'K-EFFECTIVE' 1 1.050102 ;
END: ;
QUIT .
```


### 8.3 Procedures

8.3.1 Input file for geometry

Input data for test case: Pgeom.c2m

```
***********************************************************
* *
* Procedure : Pgeom.c2m *
* Purpose : Reactor geometry definition *
* Author(s) : D. Sekki (2007/06) *
*
* CALI - GEOM := Pgeom
: GEOM := Pgeom ; *
***********************************************************
```

PARAMETER GEOM :: :: : LINKED_LIST GEOM ; ;
MODULE END: GEO: ;
GEOM := GEO: : : CAR3D 242412


Figure 13: Geometry definition (plane-1)

EDIT 1

| $\mathrm{X}-\mathrm{VOID}$ | $\mathrm{X}+$ VOID |
| :--- | :--- |
| $\mathrm{Y}-\mathrm{VOID}$ | $\mathrm{Y}+$ VOID |
| $\mathrm{Z}-\mathrm{VOID}$ | $\mathrm{Z}+$ VOID |

MIX
PLANE 1
$000000003333133330030000001-$
$000000333333133333300000001-$
000003333333333333300000 ! -





$\begin{array}{llllllllllllllllllllllllll}3 & 3 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 3 & 3 & 3 & & F\end{array}$

$\begin{array}{llllllllllllllllllllllllll} & 3 & 3 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 3 & 3 & 3 & & \text { ! }\end{array}$


PLANE 2 SAME 1
PLANE 3 SAME 1
PLANE 4 SAME 1

PLANE 5

```
* - - - 1 2 3456789 0 1 2 34567 8 - - -
    0}0000000000444444444000 0 0 0 0 0 0 ! -
    0 0 0 0 0 0 4 4 4 4 4 4 4 4 4 4 4 4 0 0 0 0 0 0 ! -
    0 0 0 0 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 0 0 0 0 0 ! -
    0 0 0 4 4 4 4 2 2 2 2 2 2 2 2 2 244444 0 0 0 ! A
    0 0 0 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 0 0 0 ! B
    0 0 4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 0 0 ! C
    044422222222 2 2 2 2 2 2 2 24444 0 ! D
    04422222222 2 2 2 2 2 2 2 2 2 24440, ! E
    44422222222 2 2 2 2 2 2 2 2 2 24444 ! F
    444222222222 2 2 2 2 2 2 2 2 24444 ! G
    4442 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 4 ! H
    44422222 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 4 ! J
    4442222 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 4 ! K
    4442 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 4 ! L
    4442 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 4 ! M
    4442 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 4 ! N
    04422 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 0 ! 0
    04442222 2 2 2 2 2 2 2 2 2 2 2 2 2 4 4 400 ! P
    0 044222222 2 2 2 2 2 2 2 2 2 2 4 4 0 0 ! Q
    0 00442222 2 2 2 2 2 2 2 2 2 24440000 ! R
    0004444422222 22 2 2 44440000, S
    0 0 0 0 0 4 444444444444444 0 0 0 0 0 ! -
    0 0 0 0 0 0 4 4 4 4 4 4 4 4 4 4 4 4 0 0 0 0 0 0 ! -
    0 000000000444444444000000000, -
```

    PLANE 6 SAME 5
    PLANE 7 SAME 5
    PLANE 8 SAME 5
    ```
    PLANE 9 SAME 1
    PLANE 10 SAME 1
    PLANE 11 SAME 1
    PLANE 12 SAME 1
    MESHX 0.0 20. 40. 62. 84. 106. 128. 150. 172.
        194. 216. 238. 260. 282. 304. 326. 348. 370.
        392. 414. 436. 458. 480. 500. 520.
    MESHY 0.0 20. 40. 62. 84. 106. 128. 150. 172.
        194. 216. 238. 260. 282. 304. 326. 348. 370.
        392. 414. 436. 458. 480. 500. 520.
MESHZ 0.0 49.53 99.06 148.59 198.12 247.65 297.18
        346.71 396.24 445.77 495.30 544.83 594.36
    SPLITX 2 2 2 2 2 2 2 2 2 2 2 2
        22222 2 2 2 2 2 2 2
SPLITY 2 2 2 2 2 2 2 2 2 2 2 2
        222222222 2 2 2
SPLITZ 2 2 2 2 2 2 2 2 2 2 2 2 ;
END: ;
QUIT .
```

8.3.2 Input file for devices

Input data for test case: Pdevc.c2m

```
*************************************************************
*
* Procedure : Pdevc.c2m *
* Purpose : Reactor rod-devices specification *
* Author(s) : D. Sekki (2007/06) *
* *
* CALL : DEVICE MATEX := Pdevc MATEX :: *
* <<mZCRin>> <<mZCRout>> <<mSORin>> <<mSORout>> ; *
*
***************************************************************
```

PARAMETER DEVICE MATEX : :
::: LINKED_LIST DEVICE MATEX ; ;
MODULE END: DEVINI: ;
INTEGER mZCRin mZCRout mSORin mSORout ;
*--

* Read arguments:
*--
:: >>mZCRin<< >>mZCRout<< >>mSORin<< >>mSORout<< ;


Figure 14: Top View of ACR Benchmark Core Model

```
DEVICE MATEX := DEVINI: MATEX :: EDIT 1 NUM-ROD 56 FADE
```

* ZCR:
*--
ROD 1
ROD-NAME ZCR01A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS $161.0183 .0 \quad 0.0 \quad 260.0 \quad 123.825173 .355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
* ROD 2

ROD-NAME ZCR01B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 161.0 183.0 $260.0520 .0 \quad 123.825173 .355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 3
ROD-NAME ZCR02A
LEVEL 0.0 AXIS Y FROM HMAXPOS 205.0 $227.0 \quad 0.0 \quad 260.0 \quad 123.825 \quad 173.355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 4
ROD-NAME ZCR02B
LEVEL 0.0 AXIS Y FROM H +
MAXPOS 205.0 $227.0 \quad 260.0 \quad 520.0 \quad 123.825173 .355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 5
ROD-NAME ZCR03A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS $249.0271 .0 \quad 0.0 \quad 260.0 \quad 123.825 \quad 173.355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 6
ROD-NAME ZCR03B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 249.0 $271.0 \quad 260.0 \quad 520.0 \quad 123.825 \quad 173.355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 7
ROD-NAME ZCR04A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS 293.0 $315.0 \quad 0.0 \quad 260.0 \quad 123.825 \quad 173.355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 8
ROD-NAME ZCRO4B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 293.0 $315.0 \quad 260.0 \quad 520.0 \quad 123.825173 .355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 9
ROD-NAME ZCR05A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS $337.0359 .0 \quad 0.0 \quad 260.0 \quad 123.825 \quad 173.355$
DMIX <<mZCRin>> <<mZCRout>>

ENDROD
*
ROD 10
ROD-NAME ZCR05B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 337.0 $359.0 \quad 260.0 \quad 520.0 \quad 123.825173 .355$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 11
ROD-NAME ZCR06A
LEVEL 0.0 AXIS Y FROM HMAXPOS 161.0 183.0 $0.0 \quad 260.0 \quad 272.415321 .945$ DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 12
ROD-NAME ZCR06B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 161.0 183.0 $260.0 \quad 520.0 \quad 272.415 \quad 321.945$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 13
ROD-NAME ZCR07A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS 205.0 $227.0 \quad 0.0 \quad 260.0 \quad 272.415 \quad 321.945$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 14
ROD-NAME ZCRO7B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 205.0 227.0 $260.0520 .0 \quad 272.415321 .945$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 15
ROD-NAME ZCR08A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS 249.0 $271.0 \quad 0.0 \quad 260.0 \quad 272.415 \quad 321.945$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 16
ROD-NAME ZCR08B
LEVEL 0.0 AXIS Y FROM H + MAXPOS 249.0 $271.0 \quad 260.0 \quad 520.0 \quad 272.415 \quad 321.945$ DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 17
ROD-NAME ZCR09A

```
    LEVEL 0.0 AXIS Y FROM H-
    MAXPOS 293.0 315.0 0.0 260.0 272.415 321.945
    DMIX <<mZCRin>> <<mZCRout>>
    ENDROD
*
    ROD 18
    ROD-NAME ZCR09B
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 293.0 315.0 260.0 520.0 272.415 321.945
    DMIX <<mZCRin>> <<mZCRout>>
    ENDROD
*
    ROD 19
    ROD-NAME ZCR10A
    LEVEL 0.0 AXIS Y FROM H-
    MAXPOS 337.0 359.0 0.0 260.0 272.415 321.945
    DMIX <<mZCRin>> <<mZCRout>>
    ENDROD
*
    ROD 20
    ROD-NAME ZCR10B
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 337.0 359.0 260.0 520.0 272.415 321.945
    DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
    ROD 21
    ROD-NAME ZCR11A
    LEVEL 0.0 AXIS Y FROM H-
    MAXPOS 161.0 183.0 0.0 260.0 421.005 470.535
    DMIX <<mZCRin>> <<mZCRout>>
    ENDROD
*
    ROD 22
    ROD-NAME ZCR11B
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 161.0 183.0 260.0 520.0 421.005 470.535
    DMIX <<mZCRin>> <<mZCRout>>
    ENDROD
*
    ROD 23
    ROD-NAME ZCR12A
    LEVEL 0.0 AXIS Y FROM H-
    MAXPOS 205.0 227.0 0.0 260.0 421.005 470.535
    DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 24
    ROD-NAME ZCR12B
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 205.0 227.0 260.0 520.0 421.005 470.535
    DMIX <<mZCRin>> <<mZCRout>>
ENDROD
```

* 

ROD 25
ROD-NAME ZCR13A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS $249.0271 .0 \quad 0.0 \quad 260.0 \quad 421.005470 .535$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 26
ROD-NAME ZCR13B
LEVEL 0.0 AXIS Y FROM H+ MAXPOS $249.0271 .0 \quad 260.0520 .0 \quad 421.005470 .535$ DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 27
ROD-NAME ZCR14A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS 293.0 $315.0 \quad 0.0 \quad 260.0 \quad 421.005470 .535$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 28
ROD-NAME ZCR14B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $293.0315 .0 \quad 260.0520 .0 \quad 421.005470 .535$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 29
ROD-NAME ZCR15A
LEVEL 0.0 AXIS Y FROM H-
MAXPOS $337.0359 .0 \quad 0.0 \quad 260.0 \quad 421.005470 .535$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*
ROD 30
ROD-NAME ZCR15B
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $337.0359 .0 \quad 260.0520 .0 \quad 421.005470 .535$
DMIX <<mZCRin>> <<mZCRout>>
ENDROD
*--

* SOR:
*--
ROD 31
ROD-NAME SORO1
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 117.0 139.0 $53.75 \quad 466.25 \quad 49.5399 .06$
DMIX <<mSORin>> <<mSORout>>
ENDROD
* 

```
    ROD 32
    ROD-NAME SORO2
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 183.0 205.0 24.5 495.5 49.53 99.06
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 33
    ROD-NAME SORO3
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 227.0 249.0 24.5 495.5 49.53 99.06
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 34
    ROD-NAME SORO4
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 271.0 293.0 24.5 495.5 49.53 99.06
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 35
    ROD-NAME SORO5
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 315.0 337.0 24.5 495.5 49.53 99.06
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 36
    ROD-NAME SOR06
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 381.0 403.0 53.75 466.25 49.53 99.06
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 37
    ROD-NAME SOR07
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 117.0 139.0 53.75 466.25 123.825 173.355
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 38
    ROD-NAME SOR08
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 381.0 403.0 53.75 466.25 123.825 173.355
    DMIX <<mSORin>> <<mSORout>>
    ENDROD
*
    ROD 39
    ROD-NAME SOR09
    LEVEL 0.0 AXIS Y FROM H+
    MAXPOS 117.0 139.0 53.75 466.25 222.885 272.415
```

DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 40
ROD-NAME SOR10
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 227.0 $249.0 \quad 24.5495 .5 \quad 198.12247 .65$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 41
ROD-NAME SOR11
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 271.0 $293.0 \quad 24.5495 .5 \quad 198.12247 .65$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 42
ROD-NAME SOR12
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $381.0403 .0 \quad 53.75 \quad 466.25 \quad 222.885 \quad 272.415$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 43
ROD-NAME SOR13
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 117.0 139.0 $53.75466 .25 \quad 272.415 \quad 321.945$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 44
ROD-NAME SOR14
LEVEL 0.0 AXIS Y FROM H +
MAXPOS $381.0403 .0 \quad 53.75 \quad 466.25 \quad 272.415 \quad 321.945$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 45
ROD-NAME SOR15
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 117.0 139.0 $53.75 \quad 466.25 \quad 321.945 \quad 371.475$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 46
ROD-NAME SOR16
LEVEL 0.0 AXIS Y FROM H +
MAXPOS 227.0 $249.0 \quad 24.5495 .5 \quad 346.71 \quad 396.24$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 47

ROD-NAME SOR17
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 271.0 $293.0 \quad 24.5495 .5 \quad 346.71 \quad 396.24$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 48
ROD-NAME SOR18
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $381.0403 .0 \quad 53.75 \quad 466.25 \quad 321.945 \quad 371.475$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 49
ROD-NAME SOR19
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $117.0139 .0 \quad 53.75466 .25 \quad 421.005470 .535$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 50
ROD-NAME SOR20
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $381.0403 .0 \quad 53.75466 .25 \quad 421.005470 .535$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 51
ROD-NAME SOR21
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 117.0 $139.0 \quad 53.75466 .25 \quad 495.3544 .83$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 52
ROD-NAME SOR22
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 183.0 $205.0 \quad 24.5495 .5 \quad 495.3544 .83$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 53
ROD-NAME SOR23
LEVEL 0.0 AXIS Y FROM H+
MAXPOS 227.0 $249.0 \quad 24.5495 .5 \quad 495.3544 .83$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 54
ROD-NAME SOR24
LEVEL 0.0 AXIS Y FROM H +
MAXPOS 271.0 $293.0 \quad 24.5495 .5 \quad 495.3544 .83$
DMIX <<mSORin>> <<mSORout>>

ENDROD
*
ROD 55
ROD-NAME SOR25
LEVEL 0.0 AXIS Y FROM H+
MAXPOS $315.0337 .0 \quad 24.5495 .5495 .3544 .83$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*
ROD 56
ROD-NAME SOR26
LEVEL 0.0 AXIS Y FROM H+ MAXPOS $381.0403 .0 \quad 53.75466 .25 \quad 495.3544 .83$
DMIX <<mSORin>> <<mSORout>>
ENDROD
*--

* create rod-devices groups:
*--
CREATE ROD-GR 5

GROUP-ID 1
ROD-ID 1221516192023242728

GROUP-ID 2
ROD-ID 34789101314

GROUP-ID 3
ROD-ID $56 \begin{array}{lllllllll} & 11 & 12 & 17 & 18 & 21 & 22 & 25 & 26 \\ 29 & 30\end{array}$

GROUP-ID 4
ROD-ID $31 \begin{array}{llllllllllllll}36 & 37 & 38 & 39 & 42 & 43 & 44 & 45 & 48 & 49 & 50 & 51 & 52 & 53 \\ 54 & 55\end{array}$

GROUP-ID 5
ROD-ID 32333435404146475356 ;

END: ;
QUIT .
8.3.3 Input file for fuel map

Input data for test case: Pfmap.c2m

```
*************************************************************
*
* Procedure : Pfmap.c2m *
* Purpose : Reactor fuel-map specification *
* Author(s) : D. Sekki (2007/11) *
* *
* CALL : FMAP MATEX := Pfmap MATEX ; *
* *
```

```
::: GEO: CAR3D 20 20 12
```


## EDIT 0

| $\mathrm{X}-\mathrm{VOID}$ | $\mathrm{X}+\mathrm{VOID}$ |
| :--- | :--- |
| $\mathrm{Y}-\mathrm{VOID}$ | $\mathrm{Y}+\mathrm{VOID}$ |
| $\mathrm{Z}-\mathrm{VOID}$ | $\mathrm{Z}+$ VOID |

```
MIX
```

PLANE 1

```
* - 123456789 0 1 2 3 4 5 6 7 8-
```

0000000000000



$0 \begin{array}{lllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & 0 & & \text { ! }\end{array}$
$\begin{array}{lllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & \text { ! } \\ \mathrm{E}\end{array}$
$\begin{array}{llllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & & \text { ! }\end{array}$

$\begin{array}{llllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & & \text { ! }\end{array}$
$\begin{array}{llllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & \text { ! J }\end{array}$
$\begin{array}{llllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & & \text { ! }\end{array}$




$0 \begin{array}{lllllllllllllllllllll}0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & 0 & & \mathrm{P}\end{array}$
$\begin{array}{lllllllllllllllllllll}0 & 0 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 0 & 0 & \\ !\end{array}$

0 |  | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


0000000000000000000000010
PLANE 2 SAME 1
PLANE 3 SAME 1
PLANE 4 SAME 1

PLANE 5

*     - 123456789012345678 -

0000000000000
00000222222222200000 ! A 00022222222222222000 ! B 00222222222222222200 ! C

```
    002 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 0 ! D
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 ! E
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 ! F
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 ! G
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 ! H
    022222222 2 2 2 2 2 2 2 2 2 2 0 ! J
    0222222222 2 2 2 2 2 2 2 2 2 0 ! K
    022222222 2 2 2 2 2 2 2 2 2 2 0 ! L
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 ! M
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 ! N
    0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0, 0
    0 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 0 ! P
    0 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 0 0 ! Q
    00022 2 2 2 2 2 2 2 2 2 2 2 2 0 0 0 ! R
    0 0000022 2 2 2 2 2 2 2 2 0 0 0 0 0 ! S
    0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 ! -
    PLANE 6 SAME 5
    PLANE }7\mathrm{ SAME 5
    PLANE }8\mathrm{ SAME 5
    PLANE 9 SAME 1
    PLANE 10 SAME 1
    PLANE 11 SAME 1
    PLANE 12 SAME 1
    MESHX 0.0 62. 84. 106. 128. 150. 172.
        194. 216. 238. 260. 282. 304. 326.
        348. 370. 392. 414. 436. 458. 520.
    MESHY 0.0 62. 84. 106. 128. 150. 172.
        194. 216. 238. 260. 282. 304. 326.
        348. 370. 392. 414. 436. 458. 520.
    MESHZ 0.0 49.53 99.06 148.59 198.12 247.65
    297.18 346.71 396.24 445.77 495.30 544.83 594.36
;
NXNAME '_, '1' '2, '3' '4' '5' '6' '7' '8' '9' '10'
    '11' '12', '13', '14', '15', '16', '17' '18',',
NYNAME ,_, 'A' 'B' 'C' 'D' 'E' 'F' 'G' 'H' 'J,
    'K' 'L' 'M' 'N' 'O' 'P' 'Q' 'R' 'S' '_,
```

NCOMB 73 B-ZONE

| 1 | 2 | 3 | 4 | 5 | 5 | 4 | 3 | 2 | 1 | 6 | 7 | 8 | 9 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 11 | 12 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 13 | 14 | 15 | 16 |
| 17 | 18 | 19 | 20 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 21 | 22 |
| 23 | 24 | 25 | 26 | 27 | 28 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 |
| 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 37 | 36 | 35 | 34 | 33 |
| 32 | 31 | 30 | 29 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 46 |


| 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 | 47 | 48 | 49 | 50 | 51 | 52 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 53 | 54 | 55 | 55 | 54 | 53 | 52 | 51 | 50 | 49 | 48 | 47 | 56 | 57 |
| 58 | 59 | 60 | 61 | 62 | 63 | 64 | 64 | 63 | 62 | 61 | 60 | 59 | 58 |
| 57 | 56 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 73 | 72 | 71 |
| 70 | 69 | 68 | 67 | 66 | 65 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 |
| 73 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 | 56 | 57 | 58 | 59 |
| 60 | 61 | 62 | 63 | 64 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 |
| 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 55 | 54 | 53 | 52 | 51 |
| 50 | 49 | 48 | 47 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 46 |
| 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 | 29 | 30 | 31 | 32 | 33 | 34 |
| 35 | 36 | 37 | 37 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 29 | 21 | 22 |
| 23 | 24 | 25 | 26 | 27 | 28 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 |
| 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 20 | 19 | 18 | 17 | 16 | 15 |
| 14 | 13 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 12 | 11 | 10 | 9 | 8 |
| 7 | 6 | 1 | 2 | 3 | 4 | 5 | 5 | 4 | 3 | 2 | 1 |  |  |

END: ;
QUIT .
8.3.4 Input file for exit burnups

|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 5 | 4 | 3 | 2 | 1 |  |  |  |  |
| B |  |  | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 12 | 11 | 10 | 9 | 8 | 7 | 6 |  |  |
| C |  | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 |  |
| D |  | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 |  |
| E | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 37 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 29 |
| F | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 46 | 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 |
| G | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 55 | 54 | 53 | 52 | 51 | 50 | 49 | 48 | 47 |
| H | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 |
| J | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 |
| K | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 73 | 72 | 71 | 70 | 69 | 68 | 67 | 66 | 65 |
| L | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 64 | 63 | 62 | 61 | 60 | 59 | 58 | 57 | 56 |
| M | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 55 | 54 | 53 | 52 | 51 | 50 | 49 | 48 | 47 |
| N | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 46 | 45 | 44 | 43 | 42 | 41 | 40 | 39 | 38 |
| O | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 37 | 36 | 35 | 34 | 33 | 32 | 31 | 30 | 29 |
| P |  | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 |  |
| Q |  | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 |  |
| R |  |  | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 12 | 11 | 10 | 9 | 8 | 7 | 6 |  |  |
| S |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 5 | 4 | 3 | 2 | 1 |  |  |  |  |

Figure 15: Combustion zones definition

Input data for test case: Pburn.c2m

```
**************************************************************
*
* Procedure : Pburn.c2m *
* Purpose : Provide average exit burnups *
* Author(s) : D. Sekki (2007/11) *
* *
* CALL : FMAP := Pburn FMAP ; *
* *
**************************************************************
PARAMETER FMAP :: ::: LINKED_LIST FMAP ; ;
MODULE END: RESINI: ;
    FMAP := RESINI: FMAP :: EDIT 2 REF-SHIFT 8
    BTYPE TIMAV-BURN
    TIMAV-BVAL
*A
    1008.98 1057.69 1071.61 1095.41 1137.92
*B
    1365.60 1586.43 1643.79 1656.34 1756.62
    2014.25 2364.85
*C
    1806.72 2019.33 2425.27 2556.62 2822.28
    3250.93 3391.85 3761.47
*D
    2279.49 2267.03 2563.72 2898.28 3261.49
    3409.15 3715.98 4136.73
*E
    2258.14 2345.30}303173.47 3111.80 3212.21
    3456.56 3705.48 3801.69 3953.67
*F
    2678.92 3263.24 3614.41 3764.97}303813.93
    3857.62 3925.74 4046.12 4119.31
*G
    2792.21 3087.13 3705.48}303960.65 4030.43
    4025.20 3978.10 3990.31 4037.40
*H
    1693.96 2811.67 3666.96 4115.83 4241.15
    4134.99 4025.20 3910.02 3915.26
*J
    2268.81 3065.97 3826.17 4232.46 4380.19
    4121.05 3995.54 3889.07 3890.81
;
```

END: ; QUIT

## References

[1] A. Hébert, Applied Reactor Physics, Presses Internationales Polytechnique, ISBN 978-2-553-01436-9, 424 p., Montréal, 2009.
[2] A. Hébert, "Development Procedures for Version4 of Reactor Physics Codes," Report IGE-287, École Polytechnique de Montréal, Institut de Génie Nucléaire (2006).
[3] A. Hébert and R. Roy, "The GAN Generalized Driver," École Polytechnique de Montréal, Institut de Génie Nucléaire (2000).
[4] G. Marleau, A. Hébert and R. Roy, "A User Guide for DRAGON Version4," Report IGE-294, École Polytechnique de Montréal, Institut de Génie Nucléaire (2007).
[5] A. Hébert, "A User Guide for TRIVAC Version4," Report IGE-293, École Polytechnique de Montréal, Institut de Génie Nucléaire (2007).
[6] A. Hébert, "TRIVAC, A Modular Diffusion Code for Fuel Management and Design Applications," Nucl. J. of Canada, Vol. 1, No. 4, 325 (1987).
[7] A. Hébert, "Application of the Hermite Method for Finite Element Reactor Calculations," Nucl. Sci. Eng., 91, 34 (1985).
[8] A. Hébert, "Variational Principles and Convergence Acceleration Strategies for the Neutron Diffusion Equation," Nucl. Sci. Eng., 91, 414 (1985).
[9] A. Hébert, "Preconditioning the Power Method for Reactor Calculations," Nucl. Sci. Eng., 94, 1 (1986).
[10] A. Hébert, "Development of the Nodal Collocation Method for Solving the Neutron Diffusion Equation," Ann. Nucl. Energy, 14, 527 (1987).
[11] A. Hébert, "Application of a Dual Variational Formulation to Finite Element Reactor Calculations," Ann. nucl. Energy, 20, 823 (1993).
[12] E. Varin, A. Hébert, J. Koclas and R. Roy, "A User Guide for DONJON," Report IGE-208, , École Polytechnique de Montréal, Institut de Génie Nucléaire (2005).
[13] E. Varin, A. Hébert, "Data Structures for DONJON," Report IGE-226, École Polytechnique de Montréal, Institut de Génie Nucléaire (2003).
[14] D. Rozon, "Gestion du combustible nucléaire. Notes de cours Ene6109," Report IGE-298, École Polytechnique de Montréal, Institut de Génie Nucléaire (2007).
[15] R. Chambon, Optimisation de la gestion du combustible dans les réacteurs CANDU refroidis à l'eau légère, Ph. D. Thesis, École Polytechnique de Montréal (2006).
[16] A. Hébert, Revisiting the Ceschino Interpolation Method, in MATLAB - A Ubiquitous Tool for the Practical Engineer, Clara M. Ionescu (Ed.), InTech Open Access Publisher, ISBN 978-953-307-907-3, Croatia, 2011.
[17] A. Hébert, G. Marleau and R. Roy, "A description of the DRAGON Data Structures," Report IGE-295, École Polytechnique de Montréal, Institut de Génie Nucléaire (2007).
[18] E. Varin and G. Marleau, "CANDU reactor core simulations using fully coupled DRAGON and DONJON calculations," Ann. Nucl. Energy, 33, 682 (2006).
[19] J. Tajmouati, "Optimisation de la gestion du combustible enrichi d'un réacteur CANDU avec prise en compte des paramètres locaux," Ph. D. thesis, École Polytechnique de Montréal (1993).
[20] M. T. Sissaoui, G. Marleau and D. Rozon, "CANDU Reactor Simulations Using the Feedback Model with Actinide Burnup History," Nucl. Technology, 125, 197 (1999).
[21] R. Roy, "The CLE-2000 Tool-box," Report IGE-163, École Polytechnique de Montréal, Institut de Génie Nucléaire (1999).
[22] A. Hébert and R. Roy, "A Programmer's Guide for the GAN Generalized Driver - FORTRAN-77 version," Report IGE-158, École Polytechnique de Montréal, Institut de Génie Nucléaire (1994).
[23] "Argonne Code Center: Benchmark Problem Book," ANL-7416, Supp. 2, ID11-A2, Argonne National Laboratory (1977).
[24] S. Loubière, R. Sanchez, M. Coste, A. Hébert, Z. Stankovski, C. Van Der Gucht and I. Zmijarevic, "APOLLO2, Twelve Years Later," paper presented at the Int. Conf. on Mathematics and Computation, Reactor Physics and Environmental Analysis in Nuclear Applications, Madrid, Spain, September 27-30, 1999.
[25] J. Griffiths, WIMS-AECL Users Manual, Report RC-1176, Atomic Energy of Canada Limited, Chalk River, Ontario (1994).
[26] J.V. Donnelly, Post-Processing WIMS-AECL Results with Proc16, Report FCC-RCP-001, Atomic Energy of Canada Limited, Chalk River, Ontario (1997).
[27] J.V. Donnelly, Wrfsp: Post-Processing Data from WIMS-AECL to RFSP, Report FCC-RCP-006, Atomic Energy of Canada Limited, Chalk River, Ontario (1997).
[28] See the home page at http://freesteam.sourceforge.net/.
[29] D. Rozon, A. Hébert and D. McNabb, "The application of generalized perturbation theory and mathematical programming to equilibrium refueling studies of a CANDU reactor," Nucl.Sci. Eng., 78, 211 (1981).
[30] R. Chambon, E. Varin and D. Rozon, "CANDU fuel management optimization using alternative gradient methods," Ann. Nucl. Energy, 34, 1002 (2007).
[31] J. A. Ferland, "A linear programming problem with an additional quadratic constraint solved by parametric linear complementarity," Publication number 497, Département d'informatique et de recherche opérationnelle, Université de Montréal, January 1984.
[32] W. H. Jens, P. A. Lottes, "Analysis of heat transfer, burnout, pressure drop and density data for high-pressure water," ANL-4627 Argonne National Laboratory (1951).
[33] R. W. Bowring, "Physical model, based on bubble detachment, and calculation of steam voidage in the subcooled region of a heated channel," Norway Institutt for Atomenergi. OECD Halden Reaktor Prosjekt (1962).
[34] R. T. Lahey and F. J. Moody, The Thermal-Hydraulics of a Boiling Water Nuclear Reactor, American Nuclear Society Publications, U.S.A. (1977).
[35] G. Rowlands, "Resonance Absorption and Non-Uniform Temperature Distributions," Journal of Nuclear Energy Parts A/B, 16, pp 235-236 (1962).

## Index

$\epsilon_{e x t}, 102,103$
$\epsilon_{\text {inn }}, 102,103$
$\epsilon_{\text {quad }}, 102,103$
$l_{\text {conv }}, 105,106$
'BUND-PW', 34
'FLUX-AV', 34
(, 133, 137
*, 62, 63, 65, 66, 68, 76, 77, 79
-, 43
.res, 35
//OLD-VALUE//, 131
: : , 8, 14, 16, 17, 21, 24, 28, 30, 32, 33, 36, 39, $42,46,48,50,53,60,64,75,85,90,94$, 99, 101, 105
: : : , 9
$:=, 8,14,16,17,21,24,28,30,32,33,36,39$, $42,46,48,50,53,60,64,75,85,90,94$, 99, 101, 105
; , 6, 7, 48, 90
BURNUP, 53, 54
HISTORY, 53, 54
MAP, 53, 54
$3-D, 1,3,4,8-12,14,15,17,18,24,108$
$3 D, 109,112,114-117$
0001, 128
DETECT: , 48
INIDET: , 21
ADD, 66-68, 77, 78, 80
ADD-PARAM, 11, 12
AFM: , 4, 10, 11, 16, 35, 37, 40, 85
ALL, $9,10,20,27,34,35,40,41,62,63,66,67$, $77,78,102$
ALLX, 64, 65
and/or, 33
AREFL, 53, 54, 59
asmb1, 43, 44
asmb2, 43, 44
ASSMB, 95, 96
AT, 43, 44
AUG-LAGRANG, 102
avburn, 43, 44
AVG-EX-BURN, 62, 66, 77
AVGB, 43, 44
AX-SHAPE, 36, 37, 56
AXIS, 19, 25, 26
axn, 43, 44
B-EXIT, 36, 37
B-ZONE, 9,10
b2, 64, 65, 75, 76
BLIN, 86,88
BORON, 86, 87
BOWR, 95, 98
BREFL, 53, 54, 59
(brnpar), 54
BTYPE, 11
BUNBLES, 55
BUND, 11, 12, 34, 35
BUNDLE-POW, 11
BUNDLES, 54
bunl, 54, 55
BURN, 42, 43, 55, 86, 87
burn, 62, 63
BURN-STEP, 40, 43, 44
burn0, 62, 63
burn1, 62, 63
burncycle, 42, 43
burncycle1, 43
burncycle2, 43
BURNUP, 53, 54, 56-58
BURNUP-BEG, 56
bval, 86, 87
bvalue, 11
CALCUL-DX, 105
caltype, 94, 95
CD, 92
CELL, 11, 13
CELLAV, 91-93
\{/CELLDIR/\}, 122
/celldir/, 58
CELLID, 56
CELLID, 53, 54, 58
CELSIUS, 97
CFC: , 85
cflux, 94, 96
CHAIN, 79
CHAN, 11, 12, 40, 41
CHAN-VOID, 50, 52
CHANNEL, 128
CHANNELS, 54, 55
CHECKER, 50, 51
CHECKER-1/2,50, 51
CHECKER-1/4, 50, 51
COMB, 11, 12
COMPARE, 43, 44
COMPO, 61, 64, 65
COMPO, 5, 21, 60, 61, 63
COMPO:, 5, 65
conc, 62, 63, 66, 67, 77-79

CONDC, 95, 97
CONDF, 95, 97
CONDG, 91
control, 102, 103
CONV, 95, 98
CONV-TEST, 105, 106
COST-EXTRAP, 105
CP, 92
CPO, 60-62
CPO, 90-93
CPO:, 5
CPONAM, 64, 65
CPONAM1, 64
CPONAM2, 64
CRE: , 4, 5, 10, 11, 16, 37, 40, 60, 61
CREATE, 17, 18, 25
CRITFL, 94, 96
CST-OBJ, 102, 103
CST-QUAD-EPS, 102, 103
CST-TYPE, 102, 103
CST-WEIGHT, 101, 102, 104
cstval, 102, 104
cstw, 102, 104
CT, 92
CUBIC, 64-67, 75-78
CVR: , 4, 50, 51
CWSECT, 95, 96
CYCLE, 42, 43
DATABASE, 85
DAY, 40, 43, 44
DBASE, 85
dcool, 86, 87
dcoolV, 50, 51
DECAY, 79, 80
DEFAULT, 21, 22
DELETE:, 3
DELH, 30, 31
delh, 30, 31
DELT, 30, 31
delt, 30, 31
DELTA, 66-68, 77, 78, 80, 99, 100
DENS-COOL, 50, 51
DERIV, 62
(descafm), 85, 86
(desccre1), 16, 60, 61
(desccre2), 16, 60, 61
(descdata1), 61, 62
(descdata2), 61, 62
(descdepl), 75, 77, 79
(descdet), 21, 22
(descdetect), 48
(descdev), 17, 21
(descdset), 28
(descflpow), 33, 34
(descgeo), 9
(descinidet), 21
(descintf), 64, 66
descintf, 65, 66
(descints), 75, 77
descints, 76, 77
(desclink), 14
(desclzc), 24, 25
(descmove), 30
(descrevr), 50
(descresini1), 8, 9
(descresini2), 8, 9, 11
(descsim), 42, 43
(desct16cpo), 90, 91, 93
(desctavg), 36
(descthm), 94, 95
(desctinst), 39, 40
(descxenon), 46, 47
DETEC, 48
DETECT, 21
/detect/, 118
DETECT, 5, 21, 48, 49
DETECT: , 4, 5, 33, 35, 48, 49, 118
DETINI: , 4, 5, 21, 118
DEV-LZC, 116, 117
(dev-lzc), 25
DEV-ROD, 115, 116
(dev-rod), 17-19
DEVICE, 17, 24, 28, 30, 32
/device/, 114, 115
DEVICE, 5, 17, 24, 28, 30, 32
DEVINI: , 4, 5, 17, 24, 29, 31, 114
DFLUX, 101
DIFF, 99, 100
DIMENSIONS, 54
DIST-AX, 43, 44
DIST-BURN, 43, 45
DIST-POWR, 43, 45
DISTR, 34, 35
(DLEAK:), 99
DLEAK:, 99
(dleak_data), 99
DMACRO, 99
DMIX, 19, 20
dmod, 86,87
DNAME, 85, 86
DONCPO, 90, 91
(DONJON), 6
DSET: , 4, 17, 20, 24, 28, 114
dt, 48, 49
ecost, 105, 106
EDI:, 65
EDIT, 9, 11, 14-18, 21, 25, 28, 30, 32, 34, 36, 37, $40,42,43,46-48,50,54,61,64,75,76$, 85, 86, 91, 94, 95, 99-102, 105
EMPTY-MIX, 25, 26
END, 28, 29
END: , 3, 6, 7
ENDCHAIN, 79, 80
ENDCYCLE , 43, 44
ENDMIX, 62, 63, 66, 68, 77, 79
ENDN, 22, 23
ENDREF, 66, 67, 77, 78
ENDROD, 19, 20
energy, 79, 80
ENRICH, 11, 13
epsburn, 43, 45
epsilon4, 103
epspowr, 43, 45
EQUI, 75, 76
ermaxc, 95, 98
ermaxt, 95, 98
EVO: , 39, 55
EXTR, 30, 31
FACTOR, 99, 100
FADE, 17, 18
FIXP, 85, 86
FLMAP, 8, 9
flow, 95, 96
FLPOW: , 4, 5, 33, 34, 36, 37, 39, 42, 46, 48, 86, 119
FLUD: , 3, 5, 33, 34, 37, 48
FLUX, 33, 34, 48
FLUX, 34, 35
/flux/, 121
FLUX, 5, 33, 34, 48, 101
FMAP, 33-36, 39, 42, 50, 51, 60, 62
FMAP, 8,12
/fmap/, 107-109
FMAP, $5,33,36,39,42,50,60,61$
FMAPV, 50, 51
fmax, 25, 26
FMIX, 14, 15
FOBJ-CST-VAL, 102, 103
FORCEAVE, 95, 98
FPUISS, 94, 95
frac, 22
fract, 21, 94, 95
FRACTION, 21, 22
FROM, 19, 42-44, 66, 77, 79, 80
frstrec, 91, 92
FSTH, 34, 35
fsth, 34, 35
FT, 92
FUEL, 11, 13, 43, 44, 110
fuel, 44
\{/FUELDIR/\}, 122
FULL, 50, 51
FULL-MIX, 25, 26
funct, 102, 103
fvalue, 11, 13
GEO: , 3, 5, 9, 14, 48
GEOM, 14, 15, 48
GEOMAP, 110
/geometry/, 107, 109, 110
GEOMETRY, $5,14,15,48$
GEOMOLD, 14, 15
GET, 53, 54, 56
GLOBAL, 11, 12, 54, 55
GPT, 101
GPT, 101
GRAD:, 101
(grad_data), 101
grad_data, 101, 102
GREP:, 3
GROUP, 30, 31
GROUP-ID, 20, 27
GRPMAX, 99, 100
GRPMIN, 99, 100
H+, 19
H-, 19
HALF, 50, 51, 102, 103
hc1, 43, 44
hc2, 43, 44
hcase, 42, 43
hcnew, 42, 43
hcold, 42-44
hcold2, 43, 44
HCONV, 95, 97
hconv, 95, 97
height, 9
HEX, 22, 23
HEXZ, 21
HGAP, 95, 97
hgap, 95, 97
HISO, 62, 63, 66-68, 77-79
History, 57
/history/, 121, 122
HISTORY, 5, 53-58
HISTORY-DATA, 128
HistXSM, 58
HOUR, 40, 43, 44
HST : , 4, 5, 53, 56, 122
(hstbrn), 53-55
(hstdim), 53, 54
(hstpar), 53-56
hx, 42, 43
hy, 42, 43
I-BURNUP, 62,63
ialch, 11, 13
ialch(i), 13
ibm1, 99, 100
ibm2, 99, 100
ibun, 53, 54
ibun, 58
icha, 53, 54
icha, 58
icz, 9, 10
id, 19, 20, 25-27, 30, 31
idfuel, 53, 54
idfuel, 58
ifuel, 43
igc, 91
igrp, 20, 27, 30, 31
ihex, 22, 23
ilg, 92
ilgrp, 28, 29
ilzc, 28, 29
IMET, 86, 88
imet, 86,88
imix, 40, 41, 66, 77, 85, 86
imixold, 66, 77
in, 17
indcycle, 42, 43
indcycle1, 43
indcycle2, 43
INFO, 21, 22
INFOR, 85,86
INIT, 34, 35, 47, 85, 86
INLET, 95, 96
INN-STEP-EPS, 102, 103
INSR, 30, 31
INST-BURN, 11, 62, 66, 77, 78
INST-BVAL, 11
INV, 95,97
inv, 95, 97
INVCONST, 21, 22
iprint, $9,11,14-18,25,28,30,32,34,36,37,40$, $42,43,46,47,50,51,54,61,64,65,75$, $76,85,86,91,94,95,99-102,105$
iprt, 21, 48
irgrp, 28, 29
irod, 28, 29
ishift, 11, 12
ivarty, $62,63,66,77,78$
izae, 79
kc, 48, 49
kcond, 95, 97
KELVIN, 97
kg, 13
KINET, 33, 34
Kinet, 33, 34
KINSOL:, 33, 34
L_POWER, 109
LEAK, 64, 65, 75, 76
LEMKE, 102
length, 9
LEVEL, 19, 25, 26, 28-31
LIBRARY, 39
Library, 39, 46
LINEAR, 64-67, 75-78
LINKED_LIST, 6,7
LIST, 91,92
LOCAL, 11, 12, 54, 55
lx, 9, 10, 42, 43
ly, 9, 10, 42, 43
LZC, 25, 26, 28, 29
LZC-GR, 25
LZC-GROUP, 28, 29, 117
(lzc-group), 25, 27
LZC-ID, 27
LZC: , 4, 17, 24, 29, 114
MAC: $, 3,5,16$
MACD : , 21
MACFL, 16, 60
MACINI: , $4,5,16,32,37$
MACRO, 85
MACRO, 16, 33, 34, 60, 61, 85, 99, 100
MACRO, $64,65,75,76$
MACRO2, 16, 32
MACRO3, 32
MACROLIB, 68,80
/macrolib/, 113
macrolib, $1,3-5,10,16,32,34,37,60-63,85$, 86
MAP, $34,35,42,43,66,67,77,78,85,86,102$
MAP, 53-58, 85-88, 94
MAPO, 57
MAPFL, 64-67, 70, 71, 75-78, 82, 83, 85, 86, 94, 96
MATEX, 8, 14, 16, 17, 24, 32-34
MATEX, 14
/matex/, 112, 113
matex, $5,8,13,14,16,17,24,32,34,51$
MAX-FULL, 25, 26
MAXIMIZE, 102, 103
maxit1, 95, 98
maxit2, 95, 98
maxit3, 95, 98
MAXPOS, 19, 20, 25, 26
MAXR, 14, 15
maxreg, 14, 15
MB, 92
MCR, 85-87
MD, 92, 93
MEMORY, 75, 76
METHOD, 102
MICLIB, 39
MICLIB2, 39
MICLIB3, 39
MICRO, 40, 62-67, 75-78
MICROLIB, 39
MICROLIB, 46
MICROLIB, 4
MINIMIZE, 102, 103
MINUTE, 40, 43, 44
MIX, 9, 62, 66, 77, 91, 92
mix, 62, 63
MIX-FUEL, 50, 51
MIX-VOID, 50, 51
mix1, 19, 20
mix2, 19, 20
mixE, 25, 26
mixF, 25, 26, 50, 51
mixf, 14, 15
MIXMAX, 99, 100
MIXMIN, 99, 100
MIXNAM, 91-93
mixr, 14, 15
$\operatorname{mix} V, 50,51$
MLIB, 64, 65, 75, 76
MLIB2, 64, 75
mmix, 85, 86
MODNAME, 6
MODULE, 6
(module), 6, 7
MOVDEV: , 4, 20, 30, 114
MOVE, 17, 18
MP, 92
MT, 92, 93
MTMD, 91, 93
MTS, 93
MULTICOMPO, 5
$M W \cdot$ day per tonne, 11

N2N, 79
N3N, 79
N4N, 80
NA, 80
namburn, 64, 65, 75, 76
NAMCHA, 40, 41

NAMDB, 85, 86
NAMDET, 22, 23
NAMDIR, 62, 64, 65
NAMDPL, 79
NAME, 19
NAME, 22, 23
/name_detect/, 119
\{/name_detect/\}, 119
/name_type/, 118, 119
\{/name_type/\}, 118
NAMPAR, 56, 79, 80
NAMPER, 91-93
NAMTYP, 21, 22, 49, 85, 86
naval, 9, 10
nB, 86, 87
nb, 10, 11, 43
nb1, 95, 98
nb2, 95, 98
nbf, 95, 96
nbfuel, 64, 65
nbg, 95, 96
nbun, 54, 55
nburn, 91, 92
Nc, 56
nch, 9-11
ncha, 54, 55
NCOMB, 9, 10
ncomb, 9-11
ncond, 95, 97
(NCR:), 64, 65
NCR: $, 4,5,10,11,16,37,39,40,50,51,60,64$
(ncr_data), 64, 66
ncr_data, 64
ncst, 101-104
ndetect, 21, 22
NEP, 86, 87
NEW, 43
NEWFUEL, 40
NEWMAC : , 4, 5, 16, 20, 26, 32, 37, 114
NFTOT, 80
NFUEL, 14, 15
nfuel, 11, 13-15, 50
NG, 79
ngcond, 91, 92
nglo, 54, 55
nglob, 55
NGMTR, 91
ngr1, 99, 100
ngr2, 99, 100
NGREAC, 91
NGRP, $14,15,21$
ngrp, 14, 15, 17, 18, 20, 21, 25, 27, 29, 31
NHEX, 22, 23
nhex, 22, 23
nk, 40
nloc, 54, 55
nlzc, 25-27, 29
NMCHA1, 40, 41
NMCHA2, 40, 41
NMIX, 14, 15, 61, 64, 65, 75, 76, 91
nmix, 61, 62
nmixt, 14, 15, 64, 65, 75, 76, 91
nNp, 86, 87
NO-STORE-OLD, 105
noreg, 91, 92
NORM, 34, 35, 48, 49
NP, 80
npert, 91, 93
NPWF, 85, 86
NREF, 86
NREFL, 14, 15
nrefl, 14, 15
nrep, 21, 22
NRMFLUX, 33
nrod, 17-20, 29, 31
nsh, 40, 41
nSm, 86, 88
NTOT1, 99, 100
ntyp, 85, 86
NUM-LZC, 25
NUM-ROD, 17, 18
nvar, 101-103
nvoid, 50, 52
nx, 9, 10
nXe, 86, 87
NXNAME, 40, 41
NXNAME, 9
ny, 9, 10
NYNAME, 40, 41
NYNAME, 9,10
ONLY, 66, 67, 77, 78
OPTIM, 99, 101, 105
/optimize/, 129, 130
OPTIMIZE, 101, 105
or, 29, 30, 50
out, 17
OUT-STEP-EPS, 102, 103
OUT-STEP-LIM, 101, 102
P-NEW, 34, 35
PARAB, 49
PARABOLIC, 102, 103
PARAM, 111, 112
PARAMBURNTAR, 57, 58
PARKEY, 11, 12, 66, 67, 77, 78
PARKEY, 11, 12

PENAL-METH, 102
period, 55
PLQ:, 105
(plq_data), 105
plq_data, 105
PNAME, 11, 12, 43, 45, 50, 51, 95, 98
PNAME, 11, 12, 45, 98
PNAMEREF, 11-13
POISON, 11, 13
POOL, 40, 41
POROS, 95, 96
poros, 95, 96
pos, 19, 20, 22, 23, 25, 26
POSITION, 22, 23
poutlet, 95, 96
pow, 85, 86
POWER, 33, 34, 36, 39, 40, 42, 44, 46
POWER, 33-35
/power/, 119-121
POWER, 5, 33, 36, 39, 42, 46
power, 34, 35, 55
POWOLD, 33, 35
PRINT, 34, 35
PTOT, 34, 35
PUFR, 95, 96
pufr, 95, 96
PUR, 86, 87
purity, 86, 87
PUT, 53, 54, 56
pvalue, 11, 13, 43, 45, 95, 98
PWF, 85, 86
pwvalue, 11
QLP:, 130
QMAP, 42-44
QUARTER, 50, 51
r1, 95, 96
r2, 95, 96
r3, 95, 96
r4, 95, 96
RADIUS, 95, 96
RATE, 25, 26
rate, 25, 26
RATIO, 34, 35
rburn, 40, 43, 44
RC, 91, 92
RD, 92
RDCL, 86, 87
RDMD, 86, 87
reaction, 79, 80
READ, 61
REF, 48, 49, 66, 67, 77, 78
ref, 95, 97

REF-SHIFT, 11, 12
REFT, 85, 86
REFUEL, 40
REGION, 91-93
RELAX, 36, 37, 94, 95
relax, 94, 95
relval, 36, 37
rep, 22, 23
RES, 64, 65, 75, 76
RESINI, 8
RESINI: , 4, 5, 8, 9, 36, 37, 39, 42, 50, 107, 109
RESP, 22, 23
RMIX, 14, 15
ROD, 19, 28, 30, 31
ROD-GR, 17, 18
ROD-GROUP, 28, 29, 116
(rod-group), 17, 18, 20
ROD-ID, 20
ROD-NAME, 19
RODMESH, 95, 98
RP, 92
RT, 92
rtime, 40, 43, 44

SAHA, 95, 98
SAM, 86, 88
SAME, 11, 12
SAMEASREF, 66, 67, 77, 78
SAP:, 5
SAPHYB, 75,76
SAPHYB, 5
SAPNAM, 75, 76
SAPNAM1, 75
SAPNAM2, 75
sass, 95, 96
(SCR:), 75, 76
SCR:, 75
(scr_data), 75, 77
scr_data, 75
SECOND, 40, 43, 44
sect, 95, 96
SEQ_ASCII, 6, 7
SEQ_BINARY, 6, 7
SET, 43, 44, 50, 51, 66-68, 77, 78, 80
SET-PARAM, 11, 12, 43, 45, 95, 98
SHUFF, 40, 41
side, 9
SIM, 9, 10
SIM: , 4, 42
SIMEX, 49
SIMPLEX, 102
SMOOTH, 11
SOME, 40

SPC, 44
SPEC, 43, 44
spec, 21, 22
SPECTRAL, 21, 22
SPEED, 19, 28-31, 95, 96
speed, 19, 28-31
SPLINE, 49
sr, 102
STABLE, 79, 80
STEP-REDUCT, 102, 103
STRNAME, 6, 7
SYSTEM, 5, 37
T-BURNUP, 62, 63
T16CPO: , 90, 91, 93
TABLE, 61, 62, 64-66, 75-77
Tape16, 90-93
TAVG:, 4, 36, 37
TCalo, 57
TComb, 57
TCOOL, 85, 87
tcool, 85, 87
TEFF, 95, 97
TEXT4, 75, 76
TFUEL, 85, 87
tfuel, 85, 87
THERMO, 94
THERMO, 94
/thm/, 124, 125
THM : , 94, 95, 125, 128
TIMAV-BURN, 11, 62, 66, 77, 78
TIMAV-BVAL, 11
TIME, 19, 20, 25, 26, 28, 29, 40, 43, 44, 48, 49, 94, 95
time, 19, 20, 25, 26, 28, 29, 94, 95
timeiter, 94, 95
TIMES, 11, 12
times, 9
timestep, 94, 95
tinlet, 95, 96
TINST: , 4, 39, 40
tinv, 21, 22
TMOD, 85, 87
TMod, 57
tmod, 85, 87
TO, 40, 41
TRACK, 33, 34, 48
TRACK, $5,34,48$
TRIVAA: , 3, 5, 37
TRIVAT: , 3, 5, 34
TYPE, 21, 22, 99, 100
type, 102, 103
unit, 95, 97

UPS, 62
USE, 66,77
USPLIT: , 4, 5, 13, 14, 48, 112
UTL:, 3
vall, $66,67,77,78$
val2, 66, 67, 77, 78
valpar, 56
valper, 91, 93
valperd, 91, 93
valpert, 91, 93
valref, 66, 67, 77, 78, 91, 92
valrefd, 91, 93
valreft, 91, 93
VALUE, 99, 100
value, 19, 25, 26, 28-31
VAR-VAL-MAX, 102, 103
VAR-VAL-MIN, 102, 103
VAR-VALUE, 102, 103
VAR-WEIGHT, 102, 103
varmax, 102, 103
varmin, 102, 103
vecmax, 102, 103
vecmin, 102, 103
velocity, 95, 96
vnorm, 48, 49
VOID-PATTERN, 50, 51
WARNING-ONLY, 105
WEIGHT, 11, 13
weight, 102, 103
width, 9
WIMS16, 90, 91
wt, 13
wteff, 95,97
X, 19, 25, 26
XENON, 86, 87
XENON:, 46, 47
XEREF, 86-88
XFAC, 32
xfac, 32
XNAME, 9, 50, 52
XSM, 63
XSM_FILE, 6, 7
Y, 19, 25, 26
yield, 79, 80
YNAME, 9, 10, 50, 52
Z, 19, 25, 26

